

## InAs-based distributed feedback interband cascade lasers

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## InAs-based distributed feedback interband cascade lasers

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Single mode emission of InAs-based interband cascade lasers using lateral metal gratings that provide distributed feedback is presented. A double ridge configuration was developed, where the grating is placed above the active region while a second, slightly wider ridge ensures current confinement in the active region. Side mode suppression ratios above 30 dB have been obtained, and single mode emission was observed at wavelengths around 6  $\mu\text{m}$  in continuous-wave operation up to a temperature of  $-10^\circ\text{C}$ . Current- and temperature-tuning rates of 0.011 nm/mA and 0.50 nm/ $^\circ\text{C}$ , respectively, have been found, and a total tuning range of 6.5 nm has been covered by one device. As a reference, ridge waveguide devices without a grating made from the same material were able to emit in pulsed mode up to  $49^\circ\text{C}$  and in continuous-wave operation at temperatures up to  $0^\circ\text{C}$  around 6  $\mu\text{m}$ . © 2015 AIP Publishing LLC. [<http://dx.doi.org/10.1063/1.4935076>]

Single mode devices in the mid-infrared spectral region are of great interest for applications like tunable diode laser absorption spectroscopy.<sup>1</sup> The requirements for such applications include low power consumption and continuous-wave (cw) operation, which makes interband cascade lasers (ICLs)<sup>2–4</sup> the ideal candidates for these tasks. On GaSb-based ICLs, room-temperature cw operation has already been demonstrated in the wavelength range between 2.8  $\mu\text{m}$  and 5.6  $\mu\text{m}$ .<sup>5–8</sup> At longer wavelengths, the low thermal conductivity and the complex growth of the superlattice claddings become increasingly difficult, as the thickness of the claddings has to be increased to avoid mode leakage into the substrate. By using highly doped InAs plasmon claddings in ICLs grown on InAs substrates, a higher thermal conductivity and a simplified growth can be achieved,<sup>9</sup> allowing such devices to extend the wavelength range covered by ICLs. Recent progress made on InAs-based ICL devices resulted in pulsed operation at room temperature up to wavelengths of 7.1  $\mu\text{m}$  (Ref. 10) and cw operation at room temperature around 4.8  $\mu\text{m}$ .<sup>11</sup> Quantum cascade lasers (QCLs), on the other hand, have also proven to be capable of high power cw operation at room temperature around 6  $\mu\text{m}$ .<sup>12</sup> While they generally outperform ICLs in terms of output power, they tend to suffer from relatively high power consumptions due to their need for high cascade numbers following the short upper state lifetimes. The lowest threshold power density reported for QCLs in this wavelength region is just below 6 kW/cm<sup>2</sup> at 300 K for an injectorless QCL emitting at 6.8  $\mu\text{m}$ .<sup>13</sup>

Several approaches have already been realized to achieve a single mode emission on GaSb-based ICL devices in the wavelength range between 2.8  $\mu\text{m}$  and 5.2  $\mu\text{m}$ .<sup>5,14–18</sup> While early single mode devices were based on corrugated sidewall gratings or top gratings, more recently distributed feedback (DFB) lasers using lateral metal gratings were demonstrated on the GaSb-based ICL material.<sup>18</sup> In these devices, a metal grating is placed on both sides of the ridges

in the GaSb-separate confinement layer (SCL) directly beneath the active region.

In this work, we present single mode DFB devices using metal gratings based on ICLs grown on InAs substrates. While investigating a configuration similar to Ref. 18 with the metal grating placed in the waveguide layer below the active region, the coupling of the mode to the grating turned out to be challenging, and no single mode operation could be achieved. This might be due to the different waveguide configuration in InAs-based ICLs. It shifts the peak of the transverse mode roughly into the middle of the active region - as opposed to GaSb-based ICLs, in which a high light field intensity is located in the SCLs surrounding the active region. Along with a higher cascade number in InAs-based ICLs, this results in a lower grating confinement factor. As the grating confinement factor decreases with the etch depth, we also examined a modified configuration with a shallowly etched ridge where the grating was placed above the active region. While sufficient coupling for single mode operation could be achieved with this structure, the severe current spreading in the active region made it impossible to achieve cw operation. Therefore, to enable cw operation while still maintaining sufficient coupling to the grating, we realized a double ridge approach, which is similar to the one presented in Ref. 19. In this work, however, we used a metal grating instead of an index grating, which is placed on the waveguide layers above the active region, as sufficient coupling can be achieved here. For further maintaining proper current confinement, a second, slightly wider ridge is defined, which is etched through the active region and thereby inhibits current spreading. A simulated mode profile for this configuration is shown in the inset of Figure 1. An estimate of the coupling coefficient based on the confinement factor of the grating and the absorption coefficient of the chromium yields values in the range of 10–20 cm<sup>-1</sup>.

The presented 11-stage device was grown on an n-InAs (100) substrate in an EIKO EV-100 molecular beam epitaxy

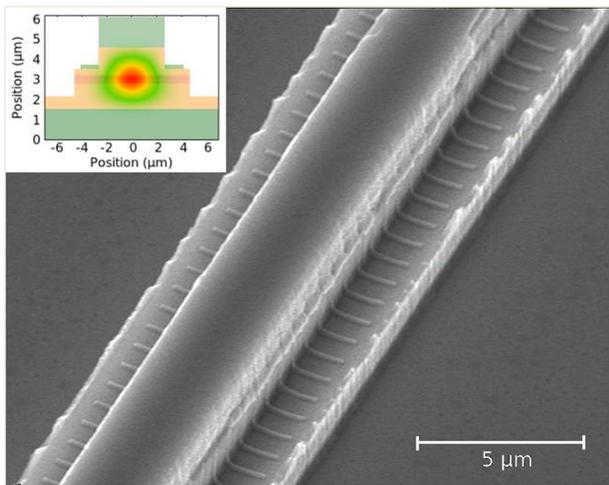


FIG. 1. Scanning electron microscope image of the double ridge structure after patterning of the chromium grating. The inset shows an overlay of the simulated mode profile and a cross-section of the waveguide.

system. Both group V elements, As and Sb, were supplied by cracker cells, while normal effusion cells were used for the group III elements. The active region was designed for an emission wavelength of  $6\ \mu\text{m}$ . Three InAs-quantum wells were used in the electron injector, two of which were Si-doped at a concentration of  $1.0 \times 10^{18}\ \text{cm}^{-3}$  for carrier rebalancing.<sup>20</sup> The total layer sequence of the active region, starting with the first InAs layer in the electron injector, is 4.2 nm InAs/1.2 nm AlSb/3.6 nm InAs/1.2 nm AlSb/3.1 nm InAs/2.5 nm AlSb/2.9 nm InAs/3.0 nm Ga<sub>0.24</sub>In<sub>0.76</sub>Sb/2.5 nm InAs/1.0 nm AlSb/3.0 nm GaSb/1.0 nm AlSb/4.5 nm GaSb/2.5 nm AlSb. To compensate for the compressive strain introduced by the AlSb, GaSb, and Ga<sub>0.24</sub>In<sub>0.76</sub>Sb layers, As soak-times were inserted in the shutter sequence at the AlSb/InAs layer transitions in the electron injector to enforce highly tensile strained AlAs interfaces. All other layer transitions were grown without any further growth interruptions.

Mode guiding is provided by a “plasmon enhanced waveguide,”<sup>9</sup> consisting of highly Si-doped InAs cladding layers and undoped InAs waveguide layers. The high doping in the cladding layers reduces the refractive index and hence introduces the refractive index in contrast to the waveguide layer required for the sufficient mode confinement. To avoid high absorption losses by free carriers in the highly doped cladding regions, a thickness of  $1.35\ \mu\text{m}$  was chosen for both waveguide layers, thus reducing the modal overlap with the cladding regions. For an initial evaluation of the grown structure, deeply etched,  $45\ \mu\text{m}$  wide ridge waveguide (RWG) structures were processed. After the dry etch step to a depth of around  $4.0\ \mu\text{m}$  using a BaF<sub>2</sub>/Cr-mask, 200 nm Si<sub>3</sub>N<sub>4</sub> and 200 nm SiO<sub>2</sub> were sputtered onto the sidewalls as passivation layers. Following the removal of the passivation on top of the ridge and the evaporation of top and bottom contacts, the sample was cleaved to 2 mm long laser bars and electro-optically characterized in pulsed operation. A short pulse width of 100 ns and a repetition rate of 1 kHz were used to avoid heating of the sample. The spectral characterization of the sample was performed using a Fourier transform infrared spectrometer.

To further evaluate the potential of the structure with regard to cw operation, narrow ridge Fabry-Pérot devices were subsequently fabricated based on the same processing procedure. For improved heat dissipation, a  $5\ \mu\text{m}$  gold layer was additionally electroplated on top of the ridge. The cleaved laser bars were mounted epi side up on copper heat-sinks using In solder. No coating was applied to the laser facets.

The processing of the DFB structure started with the definition of a  $9.3\ \mu\text{m}$  wide outer ridge using e-beam lithography in Polymethyl-methacrylate (PMMA) resist and a BaF<sub>2</sub>/Cr-mask. This ridge was then dry etched using an electron cyclotron resonance plasma process to a depth of around  $1\ \mu\text{m}$ . Subsequently, the inner ridge was defined in the middle of the wide ridge using a Ti/Pt/BaF<sub>2</sub>/Cr-mask and otherwise the same method as before. A width of  $5.3\ \mu\text{m}$  was used for this ridge, hence leaving a shoulder of  $2\ \mu\text{m}$  width on both sides of the inner ridge. A second etch was then performed to a depth of around  $2.6\ \mu\text{m}$ . As a result, the inner ridge was etched to a few hundred nanometers above the active region, while the outer ridge was etched through the active region. Afterwards, 10 nm Si<sub>3</sub>N<sub>4</sub> was sputtered onto the sidewalls to prevent shorting of the cascades by metal grating stripes accidentally overlapping the shoulder edges. The 1st order grating with a duty cycle of 23% was then defined in PMMA resist on the shoulders of the lower ridge using e-beam lithography, followed by evaporation of Cr with a thickness of 110 nm. The period of the grating was varied between 864 nm and 912 nm. A scanning electron microscope image of the ridge after this step is shown in Figure 1. Afterwards, 200 nm Si<sub>3</sub>N<sub>4</sub> and 200 nm SiO<sub>2</sub> passivation layers were sputtered onto the sidewalls. Following the removal of the passivation on top of the inner ridge, a Ti/Pt/Au top contact was evaporated, and an additional  $5\ \mu\text{m}$  of gold was electroplated on top for improved heat dissipation. After thinning the substrate to around  $150\ \mu\text{m}$ , an AuGe/Ni/Au bottom contact was evaporated. Subsequently, laser bars were cleaved from the sample and mounted epi-side up on copper heatsinks using In solder. The facets were left uncoated.

The measurements on the  $45\ \mu\text{m}$  wide and 2 mm long RWG devices revealed a pulsed threshold current density of  $950\ \text{A}/\text{cm}^2$  at a temperature of  $20\ ^\circ\text{C}$ . This is lower than our results published previously on 11 cascade ICLs grown on InAs substrates in this wavelength region,<sup>21</sup> which is mainly attributed to better carrier rebalancing in the electron injector due to the higher doping. The spectral characterization yielded emission around a central wavelength of  $6.12\ \mu\text{m}$  at  $20\ ^\circ\text{C}$ . Laser emission could be measured up to a temperature of  $49\ ^\circ\text{C}$ .

In Figure 2, the light-current-voltage (L-I-V) characteristics of a narrow ridge Fabry-Pérot device with a ridge width of  $6\ \mu\text{m}$  and a resonator length of 2.4 mm in cw operation in the temperature range between  $-16\ ^\circ\text{C}$  and  $0\ ^\circ\text{C}$  are presented. With a maximum operation temperature of  $0\ ^\circ\text{C}$ , this marks the highest operation temperature of an InAs-based ICL in this wavelength range. Higher operation temperatures, even above room temperature, have only been reported below  $5\ \mu\text{m}$  so far.<sup>11</sup> An emission spectrum of this

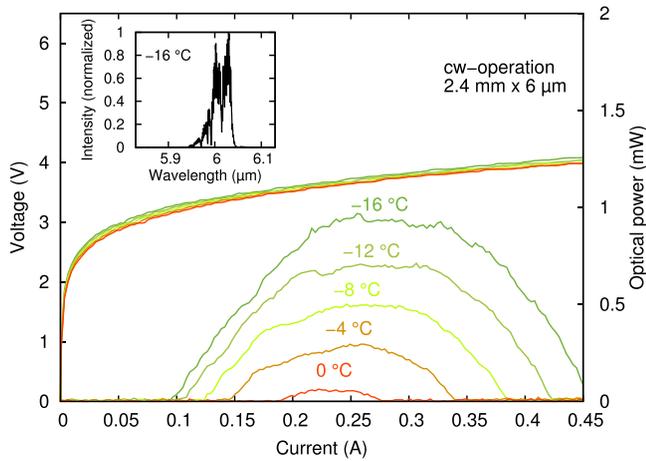


FIG. 2. Light-current-voltage characteristics of a narrow ridge Fabry-Pérot device with a ridge width of  $6\ \mu\text{m}$  and a length of  $2.4\ \text{mm}$  in cw operation at several temperatures. The device operates in the cw regime up to a temperature of  $0\ ^\circ\text{C}$ . The inset shows an emission spectrum of this device at a temperature of  $-16\ ^\circ\text{C}$ .

device recorded at a temperature of  $-16\ ^\circ\text{C}$  is depicted in the inset.

Figure 3 shows emission spectra recorded from a DFB device at a driving current of  $260\ \text{mA}$  at temperatures of  $-20\ ^\circ\text{C}$ ,  $-15\ ^\circ\text{C}$ , and  $-10\ ^\circ\text{C}$ . The dimensions of the device are  $2.4\ \text{mm}$  in length and  $5.3\ \mu\text{m}$  and  $9.3\ \mu\text{m}$  in width for the upper and lower ridge, respectively. The grating has a period of  $875\ \text{nm}$ . For the two lower temperatures, side mode suppression ratios (SMSR) of more than  $30\ \text{dB}$  can be observed, while for the spectrum recorded at  $-10\ ^\circ\text{C}$ , the side modes are buried under the noise originating from the FTIR measurement. No single mode emission could be measured above this temperature. Using the Bragg condition  $\lambda_{DFB} = 2n_{eff}\Lambda$  with the grating period  $\Lambda$  and the emission wavelength of the device, an effective refractive index of  $3.37$  can be evaluated at  $-20\ ^\circ\text{C}$ . This value compares well to our simulations of the waveguide structure.

The current dependent tuning behavior of the spectral mode of this device is depicted in Figure 4 for temperatures of  $-20\ ^\circ\text{C}$ ,  $-15\ ^\circ\text{C}$ , and  $-10\ ^\circ\text{C}$ . Tuning coefficients of  $0.011\ \text{nm}/\text{mA}$  with current and  $0.50\ \text{nm}/^\circ\text{C}$  with temperature

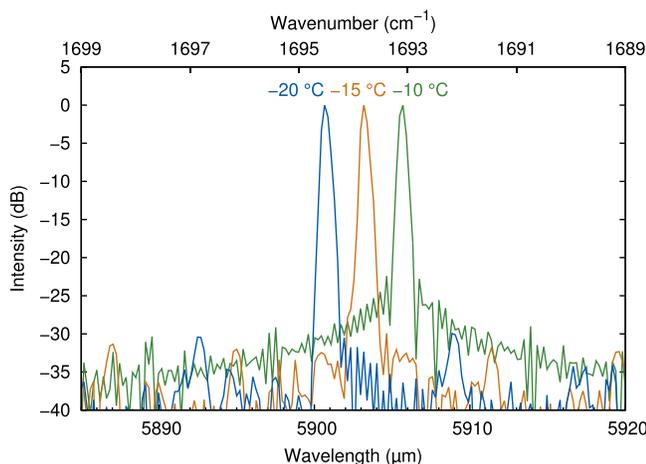


FIG. 3. Emission spectra of a DFB device at temperatures of  $-20\ ^\circ\text{C}$ ,  $-15\ ^\circ\text{C}$ , and  $-10\ ^\circ\text{C}$ . The spectra were recorded at a driving current of  $260\ \text{mA}$  (device dimensions:  $2.4\ \text{mm} \times 5.3\ \mu\text{m}/9.3\ \mu\text{m}$ ).

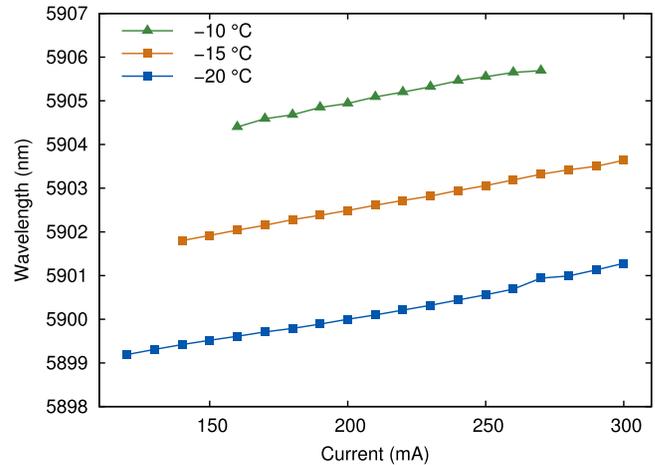


FIG. 4. Current dependent tuning characteristics for a  $2.4\ \text{mm}$  long and  $5.3\ \mu\text{m}/9.3\ \mu\text{m}$  wide ridge with a grating period of  $875\ \text{nm}$  at temperatures of  $-20\ ^\circ\text{C}$ ,  $-15\ ^\circ\text{C}$ , and  $-10\ ^\circ\text{C}$ .

were extracted for this ridge. These values are slightly lower than those reported for a GaSb-based ICL-DFB emitting at  $5.2\ \mu\text{m}$ .<sup>17</sup> A total tuning bandwidth of  $6.5\ \text{nm}$ , corresponding to  $1.9\ \text{cm}^{-1}$ , can be covered by this ridge in the temperature range from  $-20\ ^\circ\text{C}$  to  $-10\ ^\circ\text{C}$ .

Figure 5 shows the tuning behavior of another ridge with a grating period of  $895\ \text{nm}$  and a single mode emission around  $6021\ \text{nm}$ . The dimensions of this device are  $3\ \text{mm} \times 5.3\ \mu\text{m}/9.3\ \mu\text{m}$ . Due to a low signal level at a temperature of  $-10\ ^\circ\text{C}$ , the signal to noise ratios were below  $20\ \text{dB}$  for these spectra, although the device was still working in cw operation. The degradation in device performance compared to the shorter wavelength ridge indicates a stronger heating of the structure with the drive current. This is supported by a much higher current-tuning coefficient of  $0.024\ \text{nm}/\text{mA}$  while the temperature tuning coefficient of  $0.49\ \text{nm}/^\circ\text{C}$  stays nearly constant. This is likely to be caused by a higher thermal transfer resistance between the sample and the copper mount due to variations in the mounting of the samples. The inset in Figure 5 shows L-I-V characteristics of the second ridge at a temperature of  $-22\ ^\circ\text{C}$ . A threshold current of  $201\ \text{mA}$  and a power

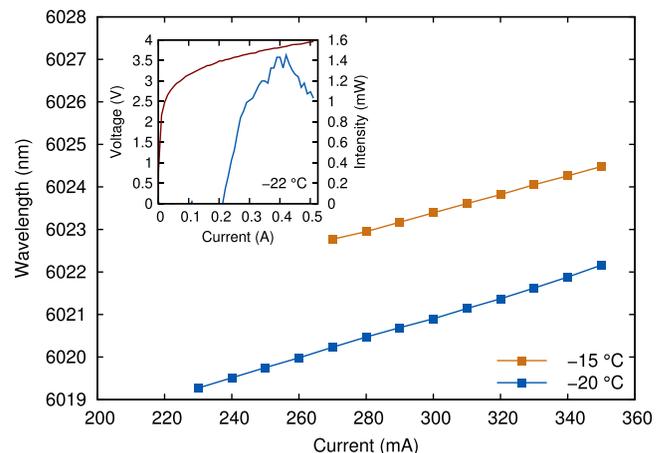


FIG. 5. Current dependent tuning characteristics for a  $3.0\ \text{mm}$  long and  $5.3\ \mu\text{m}/9.3\ \mu\text{m}$  wide ridge with a grating period of  $895\ \text{nm}$  at temperatures of  $-20\ ^\circ\text{C}$  and  $-15\ ^\circ\text{C}$ . The inset shows L-I-V characteristics of this device at a temperature of  $-22\ ^\circ\text{C}$  in cw operation.

consumption at threshold of 726 mW have been measured. The latter compares very well to values reported just recently for QCL-DFBs emitting at surrounding wavelengths for devices with uncoated facets and comparable lengths.<sup>22</sup> However, for short devices with optimized facet coatings, values as low as 310 mW at  $-30^{\circ}\text{C}$  were reported at an emission wavelength of  $5.25\ \mu\text{m}$ .

As both shown DFB devices emit rather at the edges of the gain region (see the inset in Figure 2), even better performances would be expected from devices emitting closer to the center of the gain. Unfortunately, no such lasers could be measured due to a low yield of working devices.

In conclusion, we realized a single mode emission from 11-stage InAs-based ICL-DFB devices based on a lateral metal grating. The narrow ridge devices showed laser emission in cw operation up to temperatures of  $0^{\circ}\text{C}$ . To fulfill the requirements for both, sufficient grating confinement and inhibited current spreading in the active region, a double ridge configuration was examined. In this configuration, the grating is placed above the active region on both sides of a shallowly etched ridge and a second, slightly wider, deeply etched ridge provides the current confinement. SMSRs above 30 dB have been measured in cw operation in the temperature range between  $-20^{\circ}\text{C}$  and  $-10^{\circ}\text{C}$ . With wavelengths up to 6024 nm in the single mode operation, we have demonstrated the longest wavelength ICL DFB.

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