

# Understanding CO<sub>2</sub> adsorption in a flexible zeolite through a combination of structural, kinetic and modelling techniques

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## Supporting information

### Experimental

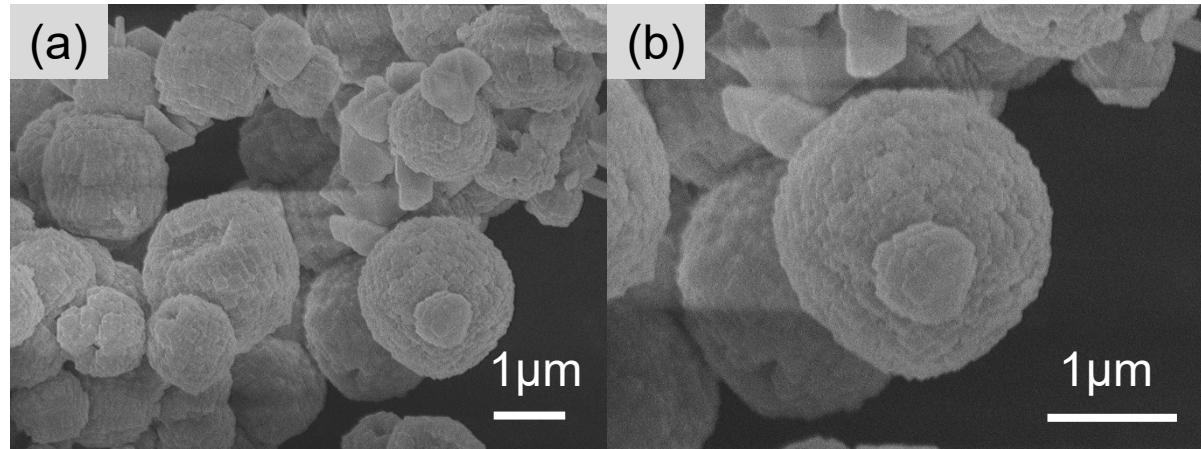


Figure S1: SEM micrographs of (Na,TEA)-ZSM-25 crystals, showing uniform particle size of 1 – 2  $\mu\text{m}$

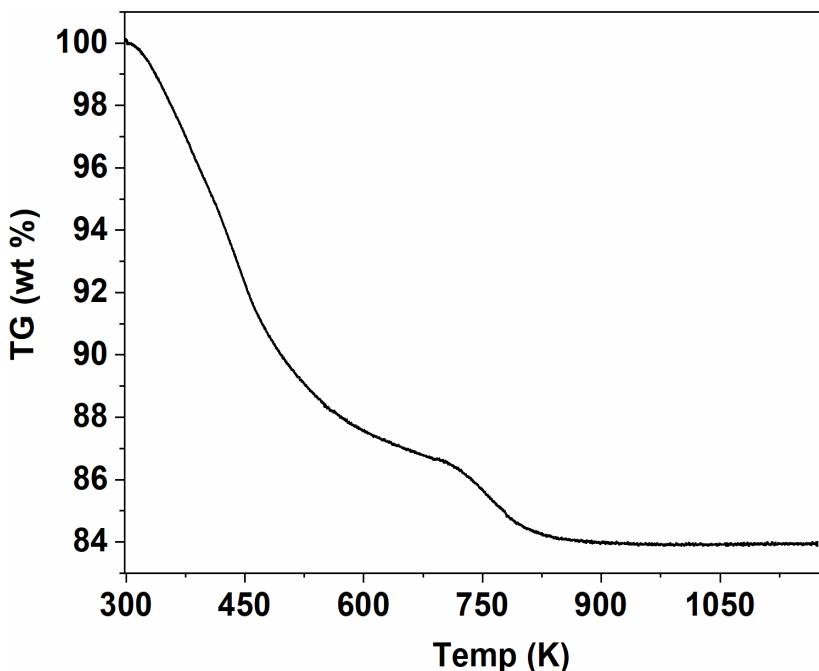


Figure S2: Thermogravimetry on (Na, TEA)-ZSM-25

### The Rigid Adsorbent Lattice Fluid

The Rigid Adsorbent Lattice Fluid (RALF) model has been described in great detail in refs. <sup>1,2</sup>. It was shown that the model can accurately describe and predict equilibrium adsorption behaviour in both ‘frozen’ as well as flexible adsorbents, with a minimum of modelling parameters. The equilibrium behaviour of the system is derived through the residual Gibbs energy, which for a single adsorbate is given by equation 1. Here we opt for the chemical engineering nomenclature as used in various textbooks, where the term residual refers to the departure of a thermodynamic property from that of an ideal gas at the same temperature and pressure<sup>3,4</sup>.

$$\frac{G^R(T, P, N)}{RT} = rN \left[ -\frac{\tilde{\rho}}{\tilde{T}} + \frac{(1 - \tilde{\rho})\ln(1 - \tilde{\rho})}{\tilde{\rho}} + 1 \right] + N(z - 1 - \ln z) \quad S1$$

Equation 1 is the expression for the residual Gibbs energy of the adsorbed phase given in ref.<sup>1</sup> written for a single adsorbate, given that the combinatorial term for a single adsorbate becomes zero due to the rigid nature of the solid. The reduced quantities are defined by:

$$\tilde{T} = \frac{T}{T^*} \quad \tilde{P} = \frac{P}{P^*} \quad \tilde{\rho} = \frac{\rho}{\rho^*}$$

Where  $T^*$ ,  $P^*$  and  $\rho^*$  are the characteristic temperature, pressure and density of the lattice fluid.  $N$  is the total number of moles in the system and  $r$  is the overall number of lattice sites per molecule.

The compressibility factor is as usual, i.e.  $z = \frac{PV}{NRT} = r \frac{\tilde{P}}{\tilde{\rho}\tilde{T}}$ . For an adsorbent, the density of the mixture does not correspond to the equilibrium value as given by an Equation of State. For the compressibility factor of a single component in equilibrium,  $z^{EoS}$ , the following holds:

S2

$$z^{EoS} - 1 = r \left[ -\frac{\tilde{\rho}}{\tilde{T}} - \frac{\ln(1 - \tilde{\rho})}{\tilde{\rho}} - 1 \right]$$

As is evident from equation 1, knowledge of the density of the system is essential to obtain the Gibbs energy. The volume of the adsorbent including the micropores,  $V_s$ , is taken as the system volume and therefore the density is given by:

$$\rho = \frac{\sum_j m_j}{V_s} = \frac{m_s}{w_s V_s} = \frac{\rho_s}{w_s} \quad S3$$

Since in this work we are dealing with a framework which can undergo volumetric changes upon adsorption, this expansion or contraction needs to be taken into account. In its simplest form, neglecting any compressibility effects (which is reasonable under normal adsorption conditions), the solid volume is given by:

$$V_s = V_s^0 + \Delta V_s \quad S4$$

Where  $V_s^0$  is the solid volume under vacuum and  $\Delta V_s$  can either be determined experimentally or a model function.

Through the residual Gibbs energy we can determine the adsorbed and fluid phase chemical potentials by carrying out the derivations with respect to number of moles of component  $k$ , i.e.

$$\frac{\mu_k^R}{RT} = \frac{1}{RT} \left( \frac{\partial G^R}{\partial N_k} \right)_{T,P,N_{j \neq k}} = \ln \varphi_k$$

For the adsorbed phase of a flexible adsorbent this yields (using subscript 1 to denote the single adsorbate):

$$\begin{aligned} \frac{\mu_{1,A}^R}{RT} &= -\frac{\tilde{\rho}}{\tilde{T}} \left( \frac{2 \sum_j \phi_j P_{j1}^*}{P^*} - 1 \right) r_1 + \left[ \frac{(1 - \tilde{\rho}) \ln(1 - \tilde{\rho})}{\tilde{\rho}} + 1 \right] r_1^0 \\ &\quad + \left( 1 + \frac{rN}{r_1 \rho_s} \frac{\partial \rho_s}{\partial N_1} \right) (z^{EoS} - 1) \frac{r_1}{r} - \ln z - \frac{z - 1}{r} \frac{rN}{\rho_s} \frac{\partial \rho_s}{\partial N_1} \end{aligned} \quad S5$$

Whilst for the fluid phase it is given by:

$$\frac{\mu_{1,F}^R}{RT} = \left[ -\frac{\tilde{\rho}_1}{\tilde{T}_1} + \frac{(1 - \tilde{\rho}_1) \ln(1 - \tilde{\rho}_1)}{\tilde{\rho}_1} + 1 \right] r_1^0 + z - 1 - \ln z \quad S6$$

For the calculation of adsorption isotherms, we can now use the usual equilibrium condition, which is for the chemical potentials of component  $k$  to be equal in the adsorbed and fluid phase. Isotherms can be constructed by solving equation 7 for the number of moles adsorbed,  $N_k$ , at any given combination of pressure and temperature.

$$\mu_{k,F}(P, T) = \mu_{k,A}(N_k, P, T) \quad S7$$

## Zero Length Column

The mass balance for CO<sub>2</sub> in the ZLC is:

$$V_s \frac{d\bar{q}}{dt} + V_f \frac{dc}{dt} = -F_{out}c \quad S8$$

Where  $V_s$  and  $V_f$  are the solid and fluid volumes, respectively,  $\bar{q}$  the average adsorbed phase concentration,  $c$  the fluid phase concentration of CO<sub>2</sub>,  $F_{in}$  is the inlet flowrate and  $F_{out}$  is the outlet flowrate.

An overall mass balance (including the carrier gas) on the cell gives the outlet flowrate:

$$F_{out} = F_{in} - \frac{V_s}{c_{tot}} \frac{d\bar{q}}{dt} \quad S9$$

Where  $c_{tot}$  is the total concentration in the ZLC, which is constant and derived from pressure and temperature with the ideal gas law, which is an appropriate equation of state under the measurement conditions.

The average adsorbed phase concentration can be computed from an overall mass balance on the adsorbent as given in the main text:

$$\frac{d\bar{q}}{dt} = -\frac{3}{R} J|_{r=R} \quad S10$$

## Structural characterisation

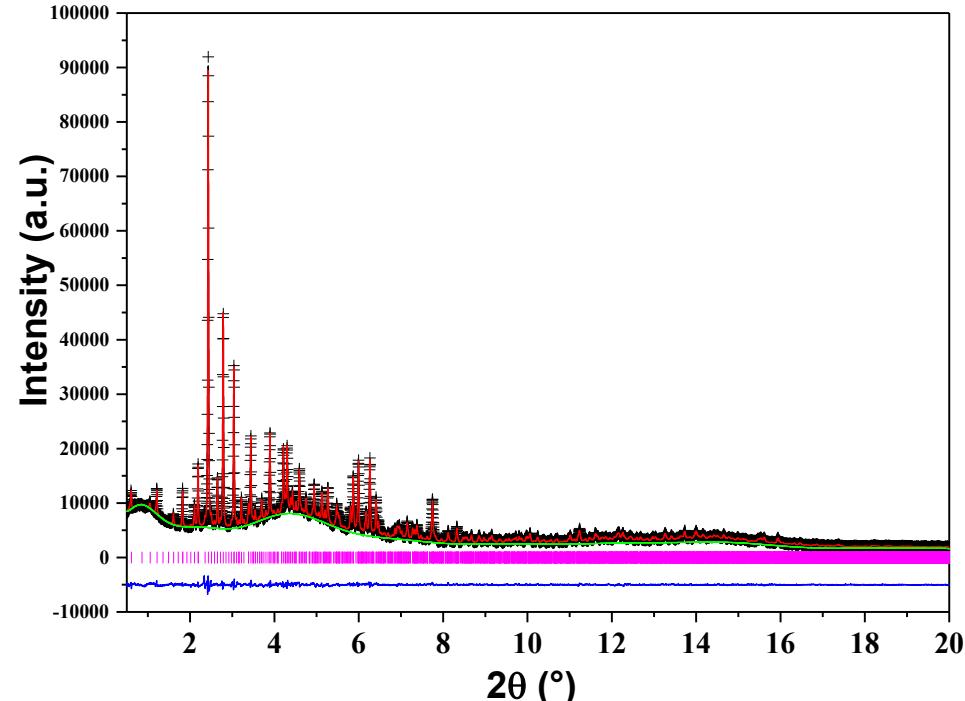


Figure S3: Rietveld refinement of calcined dehydrated (Na,H)-ZSM-25. Synchrotron data in black, calculated pattern in red, background model in green, peak positions in pink, difference between observed and calculated in blue.

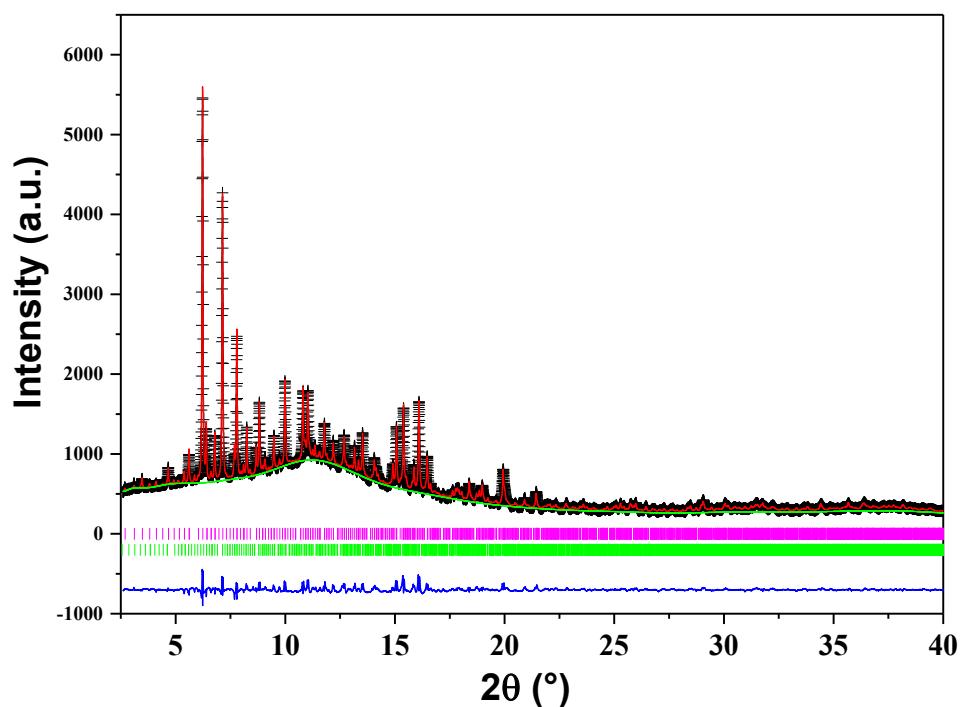


Figure S4: Rietveld refinement of calcined dehydrated (Na,TEA)-ZSM-25. Synchrotron data in black, calculated pattern in red, background model in green, peak positions in pink, difference between observed and calculated in blue.

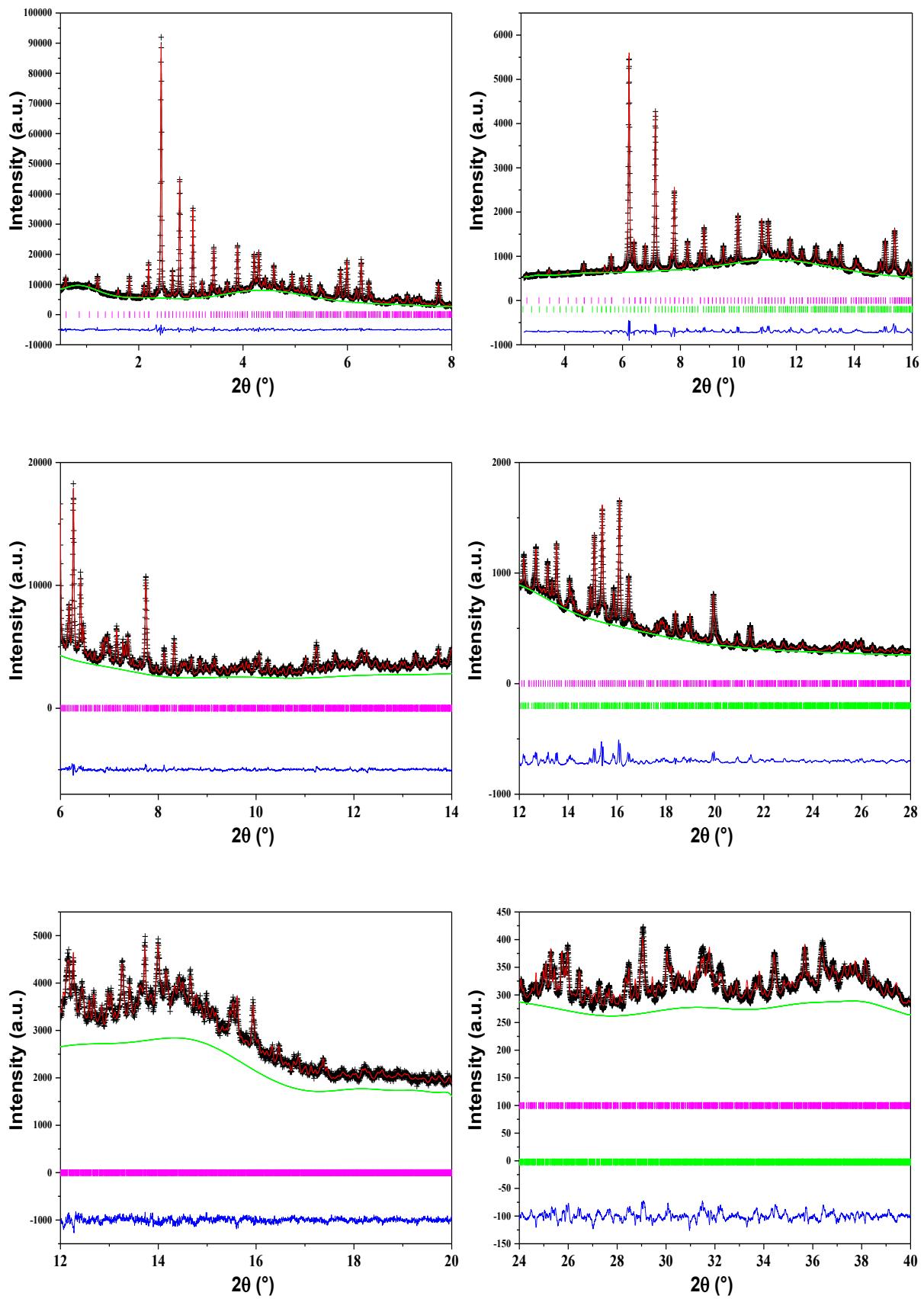


Figure S5: Rietveld plots, zoomed in on different  $2\theta$  ranges for (Na,H)-ZSM-25 (left) and (Na,TEA)-ZSM-25 (right)

Table S1: Refinement summary for dehydrated calcined (Na,H)-ZSM-25 and templated (Na,TEA)-ZSM-25. Also listed for reference is information on hydrated templated (Na,TEA)-ZSM-25 as reported in ref.<sup>5</sup>

Sample	(Na,H)-ZSM-25 (dehydrated)	(Na,TEA)-ZSM-25 (dehydrated)	(Na,TEA)-ZSM-25 (hydrated), ref. <sup>5</sup>
Measured Chemical Formula	$Na_{285}H_{40}[Si_{1106}Al_{325}O_{2880}]$	$Na_{285}N_{40}C_{320}[Si_{1115}Al_{325}O_{2880}]$	$Na_{285}N_{40}C_{320}[Si_{1115}Al_{325}O_{2880}]O_{600}$
Refined Chemical Formula	$Na_{282}[Si_{1106}Al_{325}O_{2880}]$	$Na_{273}N_{38}C_{304}[Si_{1106}Al_{325}O_{2880}]$	$Na_{296}N_{38}C_{305}[Si_{1106}Al_{334}O_{2880}]O_{812}$
T (K)	298	298	298
Space Group	$I\bar{4}3m$	$I\bar{4}3m$	$Im\bar{3}m$
X-ray Source	Synchrotron X-ray, ID-31, ESRF, Grenoble	Synchrotron X-ray, I-11, DLS, Oxfordshire	Synchrotron X-ray, ID-31, ESRF, Grenoble
$\lambda$ (Å)	0.320012	0.826956	0.632480
a (Å)	42.631(1)	42.980(1)	45.0711(3)
V (Å <sup>3</sup> )	77480(5)	79396(6)	91558(2)
R <sub>p</sub>	1.9%	2.3%	4.1%
R <sub>wp</sub>	2.4%	3.1%	5.4%
GOF	1.7	0.7	2.9

Table S2: Cation positions as determined from Rietveld refinements for dehydrated, calcined (Na,H)-ZSM-25

<b>Site</b>	<b>Type</b>	<b>x</b>	<b>y</b>	<b>z</b>	<b>Occ</b>	<b>Mult</b>	<b>Biso</b>
<b>Si1</b>	Si	0.847(2)	0.574(2)	0.525(2)	0.77	48	0.71
<b>Si1</b>	Al	0.847(2)	0.574(2)	0.525(2)	0.23	48	0.71
<b>Si2</b>	Si	0.860(2)	0.593(2)	0.457(2)	0.77	48	0.71
<b>Si2</b>	Al	0.860(2)	0.593(2)	0.457(2)	0.23	48	0.71
<b>Si3</b>	Si	0.807(2)	0.628(2)	0.542(2)	0.77	48	0.71
<b>Si3</b>	Al	0.807(2)	0.628(2)	0.542(2)	0.23	48	0.71
<b>Si4</b>	Si	0.819(2)	0.648(2)	0.470(2)	0.77	48	0.71
<b>Si4</b>	Al	0.819(2)	0.648(2)	0.470(2)	0.23	48	0.71
<b>Si5</b>	Si	0.737(2)	0.644(2)	0.529(2)	0.77	48	0.71
<b>Si5</b>	Al	0.737(2)	0.644(2)	0.529(2)	0.23	48	0.71
<b>Si6</b>	Si	0.749(2)	0.629(2)	0.456(2)	0.77	48	0.71
<b>Si6</b>	Al	0.749(2)	0.629(2)	0.456(2)	0.23	48	0.71
<b>Si7</b>	Si	0.695(2)	0.591(2)	0.541(2)	0.77	48	0.71
<b>Si7</b>	Al	0.695(2)	0.591(2)	0.541(2)	0.23	48	0.71
<b>Si8</b>	Si	0.711(2)	0.576(2)	0.473(2)	0.77	48	0.71
<b>Si8</b>	Al	0.711(2)	0.576(2)	0.473(2)	0.23	48	0.71
<b>Si9</b>	Si	0.627(2)	0.575(2)	0.525(2)	0.77	48	0.71
<b>Si9</b>	Al	0.627(2)	0.575(2)	0.525(2)	0.23	48	0.71
<b>Si10</b>	Si	0.644(2)	0.593(2)	0.458(2)	0.77	48	0.71
<b>Si10</b>	Al	0.644(2)	0.593(2)	0.458(2)	0.23	48	0.71
<b>Si11</b>	Si	0.569(2)	0.076(2)	0.025(2)	0.77	48	0.71
<b>Si11</b>	Al	0.569(2)	0.076(2)	0.025(2)	0.23	48	0.71
<b>Si12</b>	Si	0.583(2)	0.092(2)	0.959(2)	0.77	48	0.71
<b>Si12</b>	Al	0.583(2)	0.092(2)	0.959(2)	0.23	48	0.71
<b>Si13</b>	Si	0.529(2)	0.132(2)	0.040(2)	0.77	48	0.71
<b>Si13</b>	Al	0.529(2)	0.132(2)	0.040(2)	0.23	48	0.71
<b>Si14</b>	Si	0.543(2)	0.149(2)	0.973(2)	0.77	48	0.71
<b>Si14</b>	Al	0.543(2)	0.149(2)	0.973(2)	0.23	48	0.71
<b>Si15</b>	Si	0.704(2)	0.652(2)	0.808(2)	0.77	48	0.71
<b>Si15</b>	Al	0.704(2)	0.652(2)	0.808(2)	0.23	48	0.71
<b>Si16</b>	Si	0.686(2)	0.638(2)	0.180(2)	0.77	48	0.71
<b>Si16</b>	Al	0.686(2)	0.638(2)	0.180(2)	0.23	48	0.71
<b>Si17</b>	Si	0.751(2)	0.566(2)	0.703(2)	0.77	48	0.71
<b>Si17</b>	Al	0.751(2)	0.566(2)	0.703(2)	0.23	48	0.71
<b>Si18</b>	Si	0.737(2)	0.582(2)	0.316(2)	0.77	48	0.71
<b>Si18</b>	Al	0.737(2)	0.582(2)	0.316(2)	0.23	48	0.71
<b>Si19</b>	Si	0.689(2)	0.639(2)	0.737(2)	0.77	48	0.71
<b>Si19</b>	Al	0.689(2)	0.639(2)	0.737(2)	0.23	48	0.71
<b>Si20</b>	Si	0.701(2)	0.652(2)	0.249(2)	0.77	48	0.71
<b>Si20</b>	Al	0.701(2)	0.652(2)	0.249(2)	0.23	48	0.71
<b>Si21</b>	Si	0.685(2)	0.820(2)	0.581(2)	0.77	48	0.71
<b>Si21</b>	Al	0.685(2)	0.820(2)	0.581(2)	0.23	48	0.71

<b>Si22</b>	Si	0.702(2)	0.807(2)	0.431(2)	0.77		48	0.71
<b>Si22</b>	Al	0.702(2)	0.807(2)	0.431(2)	0.23		48	0.71
<b>Si23</b>	Si	0.960(2)	0.688(2)	0.639(2)	0.77		48	0.71
<b>Si23</b>	Al	0.960(2)	0.688(2)	0.639(2)	0.23		48	0.71
<b>Si24</b>	Si	0.972(2)	0.706(2)	0.345(2)	0.77		48	0.71
<b>Si24</b>	Al	0.972(2)	0.706(2)	0.345(2)	0.23		48	0.71
<b>Si25</b>	Si	0.916(2)	0.814(2)	0.541(2)	0.77		48	0.71
<b>Si25</b>	Al	0.916(2)	0.814(2)	0.541(2)	0.23		48	0.71
<b>Si26</b>	Si	0.930(2)	0.796(2)	0.469(2)	0.77		48	0.71
<b>Si26</b>	Al	0.930(2)	0.796(2)	0.469(2)	0.23		48	0.71
<b>Si27</b>	Si	0.929(2)	0.360(2)	0.759(2)	0.77		48	0.71
<b>Si27</b>	Al	0.929(2)	0.360(2)	0.759(2)	0.23		48	0.71
<b>Si28</b>	Si	0.918(2)	0.348(2)	0.258(2)	0.77		48	0.71
<b>Si28</b>	Al	0.918(2)	0.348(2)	0.258(2)	0.23		48	0.71
<b>Si29</b>	Si	0.759(2)	0.359(2)	0.153(2)	0.77		48	0.71
<b>Si29</b>	Al	0.759(2)	0.359(2)	0.153(2)	0.23		48	0.71
<b>Si30</b>	Si	0.260(2)	0.918(2)	0.570(2)	0.77		48	0.71
<b>Si30</b>	Al	0.260(2)	0.918(2)	0.570(2)	0.23		48	0.71
<b>O1</b>	O	0.818(3)	0.592(3)	0.541(3)	1		48	0.29
<b>O2</b>	O	0.850(3)	0.629(3)	0.457(3)	1		48	0.29
<b>O3</b>	O	0.768(3)	0.628(3)	0.543(3)	1		48	0.29
<b>O4</b>	O	0.788(3)	0.632(3)	0.455(3)	1		48	0.29
<b>O5</b>	O	0.707(3)	0.627(3)	0.542(3)	1		48	0.29
<b>O6</b>	O	0.741(3)	0.592(3)	0.457(3)	1		48	0.29
<b>O7</b>	O	0.657(3)	0.592(3)	0.539(3)	1		48	0.29
<b>O8</b>	O	0.681(3)	0.596(3)	0.462(3)	1		48	0.29
<b>O9</b>	O	0.101(3)	0.591(3)	0.537(3)	1		48	0.29
<b>O10</b>	O	0.121(3)	0.591(3)	0.464(3)	1		48	0.29
<b>O11</b>	O	0.539(3)	0.096(3)	0.038(3)	1		48	0.29
<b>O12</b>	O	0.571(3)	0.128(3)	0.959(3)	1		48	0.29
<b>O13</b>	O	0.688(3)	0.620(3)	0.818(3)	1		48	0.29
<b>O14</b>	O	0.685(3)	0.599(3)	0.179(3)	1		48	0.29
<b>O15</b>	O	0.705(3)	0.768(3)	0.652(3)	1		48	0.29
<b>O16</b>	O	0.704(3)	0.789(3)	0.351(3)	1		48	0.29
<b>O17</b>	O	0.740(3)	0.688(3)	0.601(3)	1		48	0.29
<b>O18</b>	O	0.739(3)	0.682(3)	0.379(3)	1		48	0.29
<b>O19</b>	O	0.631(3)	0.572(3)	0.487(3)	1		48	0.29
<b>O20</b>	O	0.789(3)	0.565(3)	0.701(3)	1		48	0.29
<b>O21</b>	O	0.768(3)	0.5692	0.299(3)	1		48	0.29
<b>O24</b>	O	0.351(3)	0.570(3)	0.179(3)	1		48	0.29
<b>O25</b>	O	0.316(3)	0.538(3)	0.820(3)	1		48	0.29
<b>O26</b>	O	0.318(3)	0.539(3)	0.264(3)	1		48	0.29
<b>O27</b>	O	0.351(3)	0.570(3)	0.733(3)	1		48	0.29
<b>O28</b>	O	0.817(3)	0.356(3)	0.492(3)	1		48	0.29

<b>029</b>	O	0.931(3)	0.761(3)	0.682(3)	1	48	0.29
<b>030</b>	O	0.931(3)	0.797(3)	0.351(3)	1	48	0.29
<b>031</b>	O	0.959(3)	0.815(3)	0.456(3)	1	48	0.29
<b>032</b>	O	0.928(3)	0.851(3)	0.540(3)	1	48	0.29
<b>033</b>	O	0.931(3)	0.798(3)	0.509(3)	1	48	0.29
<b>034</b>	O	0.759(3)	0.932(3)	0.460(3)	1	48	0.29
<b>035</b>	O	0.796(3)	0.930(3)	0.571(4)	1	48	0.29
<b>036</b>	O	0.796(3)	0.650(3)	0.848(3)	1	48	0.29
<b>037</b>	O	0.760(3)	0.681(3)	0.157(3)	1	48	0.29
<b>038</b>	O	0.744(3)	0.120(3)	0.348(3)	1	48	0.29
<b>039</b>	O	0.744(3)	0.103(3)	0.654(3)	1	48	0.29
<b>040</b>	O	0.620(3)	0.069(3)	0.241(3)	1	48	0.29
<b>041</b>	O	0.602(3)	0.070(3)	0.757(3)	1	48	0.29
<b>042</b>	O	0.898(3)	0.542(3)	0.189(3)	1	48	0.29
<b>043</b>	O	0.878(3)	0.540(3)	0.812(3)	1	48	0.29
<b>044</b>	O	0.848(3)	0.511(3)	0.208(3)	1	48	0.29
<b>047</b>	O	0.344(3)	0.259(3)	0.042(3)	1	48	0.29
<b>048</b>	O	0.346(3)	0.295(3)	0.929(3)	1	48	0.29
<b>065</b>	O	0.568(3)	0.073(3)	-0.013(3)	1	48	0.29
<b>066</b>	O	0.546(3)	0.150(3)	0.011(3)	1	48	0.29
<b>067</b>	O	0.491(3)	0.134(3)	0.037(3)	1	48	0.29
<b>068</b>	O	0.844(3)	0.575(3)	0.487(3)	1	48	0.29
<b>069</b>	O	0.739(3)	0.642(3)	0.491(3)	1	48	0.29
<b>070</b>	O	0.711(3)	0.574(3)	0.511(3)	1	48	0.29
<b>045</b>	O	0.315(3)	0.315(3)	0.036(4)	1	24	0.29
<b>046</b>	O	0.348(3)	0.348(3)	0.963(4)	1	24	0.29
<b>049</b>	O	0.682(3)	0.682(3)	0.818(5)	1	24	0.29
<b>050</b>	O	0.650(3)	0.650(3)	0.182(4)	1	24	0.29
<b>051</b>	O	0.738(3)	0.738(3)	0.564(3)	1	24	0.29
<b>052</b>	O	0.705(3)	0.705(3)	0.426(4)	1	24	0.29
<b>053</b>	O	0.595(3)	0.595(3)	0.531(4)	1	24	0.29
<b>054</b>	O	0.627(3)	0.627(2)	0.460(4)	1	24	0.29
<b>055</b>	O	0.707(3)	0.651(4)	0.707(3)	1	24	0.29
<b>056</b>	O	0.736(3)	0.652(4)	0.264(3)	1	24	0.29
<b>022</b>	O	0.735(5)	0.653(3)	0.653(3)	1	24	0.29
<b>023</b>	O	0.741(4)	0.683(3)	0.317(3)	1	24	0.29
<b>057</b>	O	0.565(3)	0.040(3)	0.040(3)	1	24	0.29
<b>058</b>	O	0.575(4)	0.074(3)	0.926(3)	1	24	0.29
<b>059</b>	O	0.847(4)	0.537(3)	0.537(3)	1	24	0.29
<b>060</b>	O	0.852(4)	0.575(3)	0.425(3)	1	24	0.29
<b>061</b>	O	0.705(4)	0.573(3)	0.573(3)	1	24	0.29
<b>062</b>	O	0.707(3)	0.540(3)	0.460(3)	1	24	0.29
<b>063</b>	O	0.622(4)	0.541(3)	0.541(3)	1	24	0.29
<b>064</b>	O	0.636(3)	0.575(2)	0.425(2)	1	24	0.29

<b>Na1</b>	Na	0.067(4)	0.067(4)	0.067(4)	0.5(2)	8	1.36
<b>Na2</b>	Na	0.364(3)	0	0	1.0(2)	12	1.36
<b>Na3</b>	Na	0.157(4)	0	0	0.9(2)	12	1.36
<b>Na4</b>	Na	0.074(2)	0.257(2)	0.074(2)	1.0(1)	24	1.36
<b>Na5</b>	Na	0.107(3)	0.401(4)	0.107(3)	0.5(1)	24	1.36
<b>Na6</b>	Na	0.502(3)	0.064(3)	0.064(3)	0.7(1)	24	1.36
<b>Na7</b>	Na	0.423(3)	0.232(2)	0.232(2)	0.7(2)	24	1.36
<b>Na8</b>	Na	0.068(5)	0.402(4)	0.402(4)	0.4(1)	24	1.36
<b>Na9</b>	Na	0.167(4)	0.393(3)	0.393(3)	0.6(1)	24	1.36
<b>Na10</b>	Na	0.363(7)	0.168(5)	0.168(5)	0.3(2)	24	1.36
<b>Na11</b>	Na	0.048(3)	0.172(2)	0.172(2)	0.9(1)	24	1.36
<b>Na12</b>	Na	0.143(3)	0.265(2)	0.265(2)	0.9(2)	24	1.36
<b>Na13</b>	Na	0.169(2)	0.169(2)	-0.035(2)	1.0(2)	24	1.36
<b>Na14</b>	Na	0.212(4)	0.212(4)	0.356(5)	0.5(1)	24	1.36
<b>Na15</b>	Na	0.211(2)	0.561(2)	0.016(2)	0.8(1)	48	1.36
<b>Na16</b>	Na	0.236(2)	0.339(2)	-0.010(3)	0.8(1)	48	1.36

Table S3: Cation positions as determined from Rietveld refinements for dehydrated, templated (Na,TEA)-ZSM-25

<b>Site</b>	<b>Type</b>	<b>x</b>	<b>y</b>	<b>z</b>	<b>Occ</b>	<b>Mult</b>	<b>Biso</b>
<b>Si1</b>	Si	0.850(3)	0.578(3)	0.526(3)	0.77	48	0.71
<b>Si1</b>	Al	0.850(3)	0.578(3)	0.526(3)	0.23	48	0.71
<b>Si2</b>	Si	0.859(3)	0.591(3)	0.460(4)	0.77	48	0.71
<b>Si2</b>	Al	0.859(3)	0.591(3)	0.460(4)	0.23	48	0.71
<b>Si3</b>	Si	0.809(3)	0.633(3)	0.538(3)	0.77	48	0.71
<b>Si3</b>	Al	0.809(3)	0.633(3)	0.538(3)	0.23	48	0.71
<b>Si4</b>	Si	0.820(3)	0.647(3)	0.469(3)	0.77	48	0.71
<b>Si4</b>	Al	0.820(3)	0.647(3)	0.469(3)	0.23	48	0.71
<b>Si5</b>	Si	0.737(3)	0.643(3)	0.534(3)	0.77	48	0.71
<b>Si5</b>	Al	0.737(3)	0.643(3)	0.534(3)	0.23	48	0.71
<b>Si6</b>	Si	0.745(3)	0.634(3)	0.463(3)	0.77	48	0.71
<b>Si6</b>	Al	0.745(3)	0.634(3)	0.463(3)	0.23	48	0.71
<b>Si7</b>	Si	0.697(3)	0.587(3)	0.542(3)	0.77	48	0.71
<b>Si7</b>	Al	0.697(3)	0.587(3)	0.542(3)	0.23	48	0.71
<b>Si8</b>	Si	0.709(3)	0.577(3)	0.469(3)	0.77	48	0.71
<b>Si8</b>	Al	0.709(3)	0.577(3)	0.469(3)	0.23	48	0.71
<b>Si9</b>	Si	0.626(3)	0.575(3)	0.527(3)	0.77	48	0.71
<b>Si9</b>	Al	0.626(3)	0.575(3)	0.527(3)	0.23	48	0.71
<b>Si10</b>	Si	0.642(3)	0.592(3)	0.461(3)	0.77	48	0.71
<b>Si10</b>	Al	0.642(3)	0.592(3)	0.461(3)	0.23	48	0.71
<b>Si11</b>	Si	0.570(3)	0.077(3)	0.028(3)	0.77	48	0.71
<b>Si11</b>	Al	0.570(3)	0.077(3)	0.028(3)	0.23	48	0.71
<b>Si12</b>	Si	0.581(3)	0.091(3)	0.960(4)	0.77	48	0.71
<b>Si12</b>	Al	0.581(3)	0.091(3)	0.960(4)	0.23	48	0.71
<b>Si13</b>	Si	0.533(3)	0.136(3)	0.040(3)	0.77	48	0.71
<b>Si13</b>	Al	0.533(3)	0.136(3)	0.040(3)	0.23	48	0.71
<b>Si14</b>	Si	0.543(3)	0.149(3)	0.972(3)	0.77	48	0.71
<b>Si14</b>	Al	0.543(3)	0.149(3)	0.972(3)	0.23	48	0.71
<b>Si15</b>	Si	0.700(3)	0.652(3)	0.810(3)	0.77	48	0.71
<b>Si15</b>	Al	0.700(3)	0.652(3)	0.810(3)	0.23	48	0.71
<b>Si16</b>	Si	0.689(3)	0.640(3)	0.182(3)	0.77	48	0.71
<b>Si16</b>	Al	0.689(3)	0.640(3)	0.182(3)	0.23	48	0.71
<b>Si17</b>	Si	0.751(3)	0.572(4)	0.703(4)	0.77	48	0.71
<b>Si17</b>	Al	0.751(3)	0.572(4)	0.703(4)	0.23	48	0.71
<b>Si18</b>	Si	0.736(3)	0.579(3)	0.314(3)	0.77	48	0.71
<b>Si18</b>	Al	0.736(3)	0.579(3)	0.314(3)	0.23	48	0.71
<b>Si19</b>	Si	0.690(3)	0.639(3)	0.743(3)	0.77	48	0.71
<b>Si19</b>	Al	0.690(3)	0.639(3)	0.743(3)	0.23	48	0.71
<b>Si20</b>	Si	0.700(3)	0.645(3)	0.248(3)	0.77	48	0.71
<b>Si20</b>	Al	0.700(3)	0.645(3)	0.248(3)	0.23	48	0.71
<b>Si21</b>	Si	0.690(3)	0.822(3)	0.581(3)	0.77	48	0.71
<b>Si21</b>	Al	0.690(3)	0.822(3)	0.581(3)	0.23	48	0.71

<b>Si22</b>	Si	0.701(3)	0.810(3)	0.432(4)	0.77	48	0.71
<b>Si22</b>	Al	0.701(3)	0.810(3)	0.432(4)	0.23	48	0.71
<b>Si23</b>	Si	0.963(3)	0.685(3)	0.635(3)	0.77	48	0.71
<b>Si23</b>	Al	0.963(3)	0.685(3)	0.635(3)	0.23	48	0.71
<b>Si24</b>	Si	0.968(3)	0.703(3)	0.349(3)	0.77	48	0.71
<b>Si24</b>	Al	0.968(3)	0.703(3)	0.349(3)	0.23	48	0.71
<b>Si25</b>	Si	0.917(3)	0.815(3)	0.542(3)	0.77	48	0.71
<b>Si25</b>	Al	0.917(3)	0.815(3)	0.542(3)	0.23	48	0.71
<b>Si26</b>	Si	0.927(3)	0.798(3)	0.469(3)	0.77	48	0.71
<b>Si26</b>	Al	0.927(3)	0.798(3)	0.469(3)	0.23	48	0.71
<b>Si27</b>	Si	0.932(3)	0.360(3)	0.758(3)	0.77	48	0.71
<b>Si27</b>	Al	0.932(3)	0.360(3)	0.758(3)	0.23	48	0.71
<b>Si28</b>	Si	0.919(3)	0.351(3)	0.259(3)	0.77	48	0.71
<b>Si28</b>	Al	0.919(3)	0.351(3)	0.259(3)	0.23	48	0.71
<b>Si29</b>	Si	0.757(3)	0.360(3)	0.153(3)	0.77	48	0.71
<b>Si29</b>	Al	0.757(3)	0.360(3)	0.153(3)	0.23	48	0.71
<b>Si30</b>	Si	0.259(4)	0.918(3)	0.572(3)	0.77	48	0.71
<b>Si30</b>	Al	0.259(4)	0.918(3)	0.572(3)	0.23	48	0.71
<b>O1</b>	O	0.822(6)	0.598(6)	0.540(7)	1	48	0.29
<b>O2</b>	O	0.847(6)	0.626(6)	0.540(7)	1	48	0.29
<b>O3</b>	O	0.771(6)	0.630(5)	0.541(5)	1	48	0.29
<b>O4</b>	O	0.786(6)	0.637(5)	0.461(5)	1	48	0.29
<b>O5</b>	O	0.707(5)	0.625(6)	0.545(6)	1	48	0.29
<b>O6</b>	O	0.736(5)	0.598(6)	0.459(6)	1	48	0.29
<b>O7</b>	O	0.659(5)	0.588(5)	0.537(6)	1	48	0.29
<b>O8</b>	O	0.678(5)	0.590(5)	0.462(5)	1	48	0.29
<b>O9</b>	O	0.102(6)	0.592(6)	0.537(5)	1	48	0.29
<b>O10</b>	O	0.118(5)	0.592(7)	0.464(6)	1	48	0.29
<b>O11</b>	O	0.544(5)	0.100(5)	0.038(6)	1	48	0.29
<b>O12</b>	O	0.569(5)	0.128(7)	0.960(7)	1	48	0.29
<b>O13</b>	O	0.688(6)	0.620(5)	0.823(6)	1	48	0.29
<b>O14</b>	O	0.687(6)	0.601(6)	0.179(7)	1	48	0.29
<b>O15</b>	O	0.702(6)	0.774(5)	0.649(6)	1	48	0.29
<b>O16</b>	O	0.707(6)	0.790(5)	0.354(6)	1	48	0.29
<b>O17</b>	O	0.743(6)	0.683(6)	0.601(6)	1	48	0.29
<b>O18</b>	O	0.742(6)	0.682(6)	0.382(5)	1	48	0.29
<b>O19</b>	O	0.631(5)	0.570(5)	0.489(7)	1	48	0.29
<b>O20</b>	O	0.790(7)	0.569(6)	0.705(5)	1	48	0.29
<b>O21</b>	O	0.771(6)	0.571(6)	0.297(6)	1	48	0.29
<b>O24</b>	O	0.346(6)	0.567(6)	0.179(5)	1	48	0.29
<b>O25</b>	O	0.318(6)	0.542(6)	0.822(6)	1	48	0.29
<b>O26</b>	O	0.320(5)	0.545(5)	0.264(7)	1	48	0.29
<b>O27</b>	O	0.346(5)	0.566(6)	0.737(5)	1	48	0.29
<b>O28</b>	O	0.818(6)	0.351(6)	0.492(6)	1	48	0.29

<b>029</b>	O	0.933(6)	0.762(5)	0.676(5)		1	48	0.29
<b>030</b>	O	0.933(7)	0.792(6)	0.350(6)		1	48	0.29
<b>031</b>	O	0.957(7)	0.816(5)	0.456(6)		1	48	0.29
<b>032</b>	O	0.930(7)	0.847(6)	0.542(6)		1	48	0.29
<b>033</b>	O	0.928(6)	0.799(6)	0.509(7)		1	48	0.29
<b>034</b>	O	0.762(6)	0.927(5)	0.457(7)		1	48	0.29
<b>035</b>	O	0.794(6)	0.929(6)	0.571(6)		1	48	0.29
<b>036</b>	O	0.792(5)	0.652(7)	0.847(6)		1	48	0.29
<b>037</b>	O	0.761(6)	0.681(6)	0.154(6)		1	48	0.29
<b>038</b>	O	0.742(6)	0.119(7)	0.349(6)		1	48	0.29
<b>039</b>	O	0.745(5)	0.101(6)	0.650(6)		1	48	0.29
<b>040</b>	O	0.619(6)	0.072(6)	0.242(6)		1	48	0.29
<b>041</b>	O	0.602(5)	0.070(6)	0.756(6)		1	48	0.29
<b>042</b>	O	0.900(6)	0.542(6)	0.185(6)		1	48	0.29
<b>043</b>	O	0.878(5)	0.542(6)	0.814(6)		1	48	0.29
<b>044</b>	O	0.851(6)	0.508(6)	0.203(6)		1	48	0.29
<b>047</b>	O	0.349(6)	0.262(6)	0.041(6)		1	48	0.29
<b>048</b>	O	0.350(6)	0.293(6)	0.932(5)		1	48	0.29
<b>065</b>	O	0.567(5)	0.075(6)	-0.011(6)		1	48	0.29
<b>066</b>	O	0.546(5)	0.150(6)	0.010(5)		1	48	0.29
<b>067</b>	O	0.492(6)	0.137(5)	0.039(6)		1	48	0.29
<b>068</b>	O	0.846(6)	0.576(6)	0.489(7)		1	48	0.29
<b>069</b>	O	0.735(5)	0.647(6)	0.494(6)		1	48	0.29
<b>070</b>	O	0.714(5)	0.575(5)	0.511(5)		1	48	0.29
<b>045</b>	O	0.318(6)	0.318(6)	0.042(10)		1	24	0.29
<b>046</b>	O	0.348(6)	0.348(6)	0.960(9)		1	24	0.29
<b>049</b>	O	0.683(6)	0.683(6)	0.820(9)		1	24	0.29
<b>050</b>	O	0.657(6)	0.657(6)	0.182(9)		1	24	0.29
<b>051</b>	O	0.736(6)	0.736(6)	0.572(8)		1	24	0.29
<b>052</b>	O	0.707(5)	0.707(5)	0.427(9)		1	24	0.29
<b>053</b>	O	0.596(5)	0.596(5)	0.532(8)		1	24	0.29
<b>054</b>	O	0.625(5)	0.625(5)	0.46110)		1	24	0.29
<b>055</b>	O	0.711(6)	0.648(10)	0.711(6)		1	24	0.29
<b>056</b>	O	0.732(6)	0.652(8)	0.268(6)		1	24	0.29
<b>022</b>	O	0.741(8)	0.654(7)	0.654(7)		1	24	0.29
<b>023</b>	O	0.748(8)	0.678(5)	0.322(5)		1	24	0.29
<b>057</b>	O	0.567(7)	0.043(6)	0.043(6)		1	24	0.29
<b>058</b>	O	0.570(8)	0.070(5)	0.930(5)		1	24	0.29
<b>059</b>	O	0.852(7)	0.544(7)	0.544(7)		1	24	0.29
<b>060</b>	O	0.850(8)	0.570(6)	0.430(6)		1	24	0.29
<b>061</b>	O	0.705(8)	0.572(6)	0.572(6)		1	24	0.29
<b>062</b>	O	0.711(7)	0.542(5)	0.458(5)		1	24	0.29
<b>063</b>	O	0.623(8)	0.544(6)	0.544(6)		1	24	0.29
<b>064</b>	O	0.627(7)	0.570(5)	0.430(5)		1	24	0.29

<b>Na1</b>	Na	0.040(4)	0.040(4)	0.040(4)	1	8	1.36
<b>Na2</b>	Na	0.234(4)	0.234(4)	0.234(4)	0.99998	8	1.36
<b>Na3</b>	Na	0.282(5)	0.282(5)	0.282(5)	0.99998	8	1.36
<b>Na4</b>	Na	0.438(5)	0.438(5)	0.438(5)	1	8	1.36
<b>Na5</b>	Na	0.14(13)	0	0	0.49861	12	1.36
<b>Na6</b>	Na	0.051(3)	0.519(5)	0.051(3)	0.9378	24	1.36
<b>Na7</b>	Na	0.426(5)	0.231(3)	0.231(3)	1	24	1.36
<b>Na8</b>	Na	0.074(5)	0.212(3)	0.212(3)	1	24	1.36
<b>Na9</b>	Na	0.191(5)	0.409(3)	0.409(3)	0.8475	24	1.36
<b>Na10</b>	Na	0.033(6)	0.159(4)	0.159(4)	1	24	1.36
<b>Na11</b>	Na	0.144(6)	0.262(3)	0.262(3)	0.99859	24	1.36
<b>Na12</b>	Na	0.102(3)	0.102(3)	0.470(4)	1	24	1.36
<b>Na13</b>	Na	0.224(3)	0.224(3)	0.372(5)	1	24	1.36
<b>Na14</b>	Na	0.224(3)	0.587(3)	0.013(3)	1	48	1.36
<b>N1</b>	N	0.5	0	0	0.4(2)	6	2.00
<b>C1a</b>	C	0.478	0	0.030	0.2(1)	48	2.00
<b>C1b</b>	C	0.5	0	0.061	0.4(2)	24	2.00
<b>N2</b>	N	0.340	0	0	0.9(2)	12	2.00
<b>C2a</b>	C	0.318	0	0.030	0.4(1)	48	2.00
<b>C2b</b>	C	0.340	0	0.061	0.9(1)	48	2.00
<b>C2c</b>	C	0.362	0	0.030	0.4(1)	48	2.00
<b>N3x</b>	N	0.136	0.136	0.136	0.5(1)	8	2.00
<b>C31ax</b>	C	0.114	0.114	0.114	0.5(1)	8	2.00
<b>C31bx</b>	C	0.136	0.093	0.093	0.2(1)	24	2.00
<b>C32ax</b>	C	0.157	0.157	0.114	0.5(1)	24	2.00
<b>C32bx</b>	C	0.150	0.150	0.079	0.5(1)	24	2.00
<b>N3y</b>	N	0.119	0.119	0.119	0.5(1)	8	2.00
<b>C31ay</b>	C	0.140	0.140	0.140	0.5(1)	8	2.00
<b>C31by</b>	C	0.162	0.162	0.119	0.2(1)	24	2.00
<b>C32ay</b>	C	0.141	0.098	0.098	0.5(1)	24	2.00
<b>C32by</b>	C	0.176	0.105	0.105	0.5(1)	24	2.00
<b>N4x</b>	N	0.266	0.266	0.266	0.5(1)	8	2.00
<b>C41ax</b>	C	0.244	0.244	0.244	0.5(1)	8	2.00
<b>C41bx</b>	C	0.266	0.223	0.223	0.2(1)	24	2.00
<b>C42ax</b>	C	0.287	0.287	0.244	0.5(1)	24	2.00
<b>C42bx</b>	C	0.280	0.280	0.209	0.5(1)	24	2.00
<b>N4y</b>	N	0.200	0.200	0.200	0.5(1)	8	2.00
<b>C41ay</b>	C	0.222	0.222	0.222	0.5(1)	8	2.00
<b>C41by</b>	C	0.243	0.243	0.200	0.2(1)	24	2.00
<b>C42ay</b>	C	0.222	0.179	0.179	0.5(1)	24	2.00
<b>C42by</b>	C	0.257	0.186	0.186	0.5(1)	24	2.00
<b>N5x</b>	N	0.377	0.377	0.377	0.5(1)	8	2.00
<b>C51ax</b>	C	0.355	0.355	0.355	0.5(1)	8	2.00
<b>C51bx</b>	C	0.377	0.334	0.334	0.2(1)	24	2.00

<b>C52ax</b>	C	0.398	0.398	0.355	0.5(1)	24	2.00
<b>C52bx</b>	C	0.390	0.390	0.319	0.5(1)	24	2.00
<b>N5y</b>	N	0.343	0.343	0.343	0.5(1)	8	2.00
<b>C51ay</b>	C	0.364	0.364	0.364	0.5(1)	8	2.00
<b>C51by</b>	C	0.385	0.385	0.342	0.2(1)	24	2.00
<b>C52ay</b>	C	0.364	0.321	0.321	0.5(1)	24	2.00
<b>C52by</b>	C	0.400	0.329	0.329	0.5(1)	24	2.00

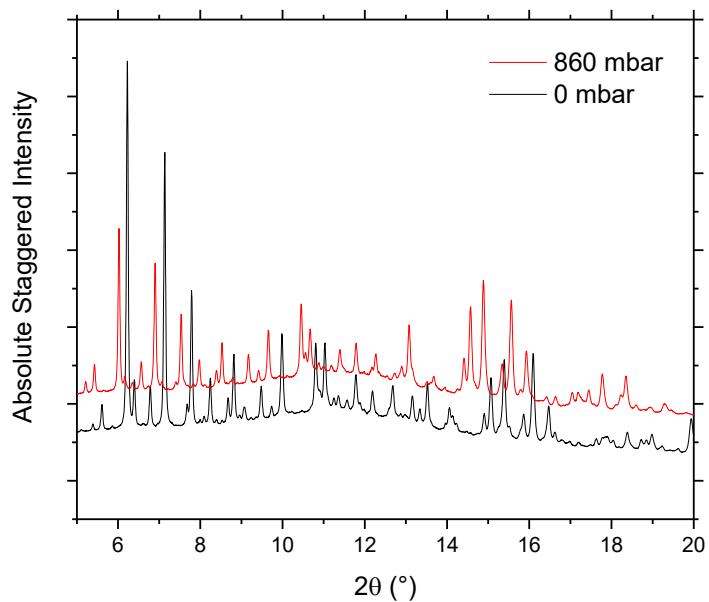
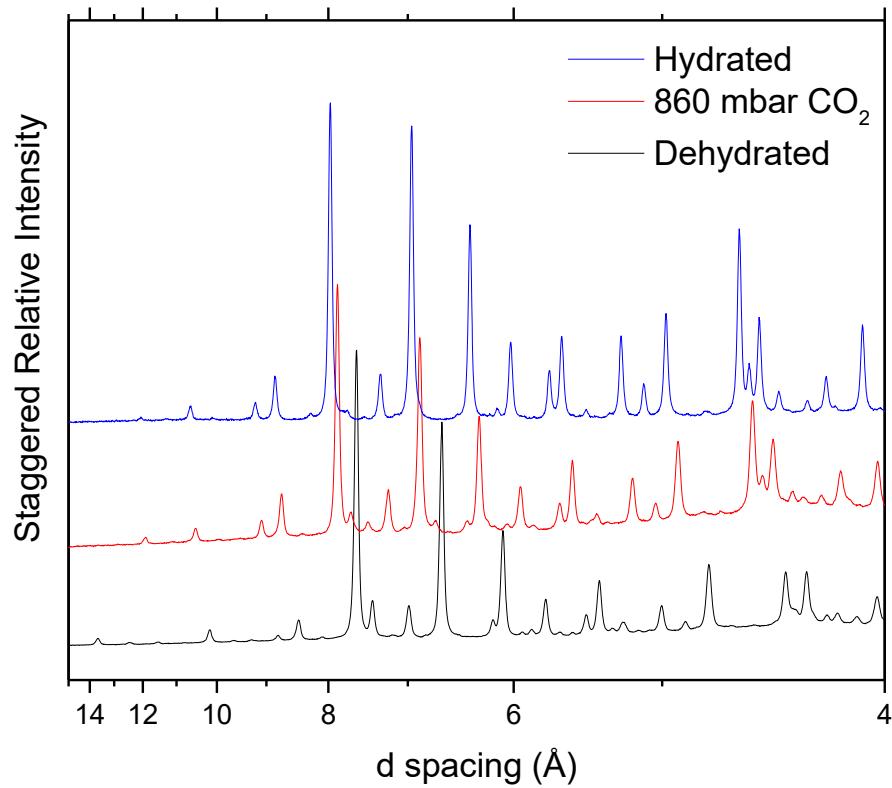
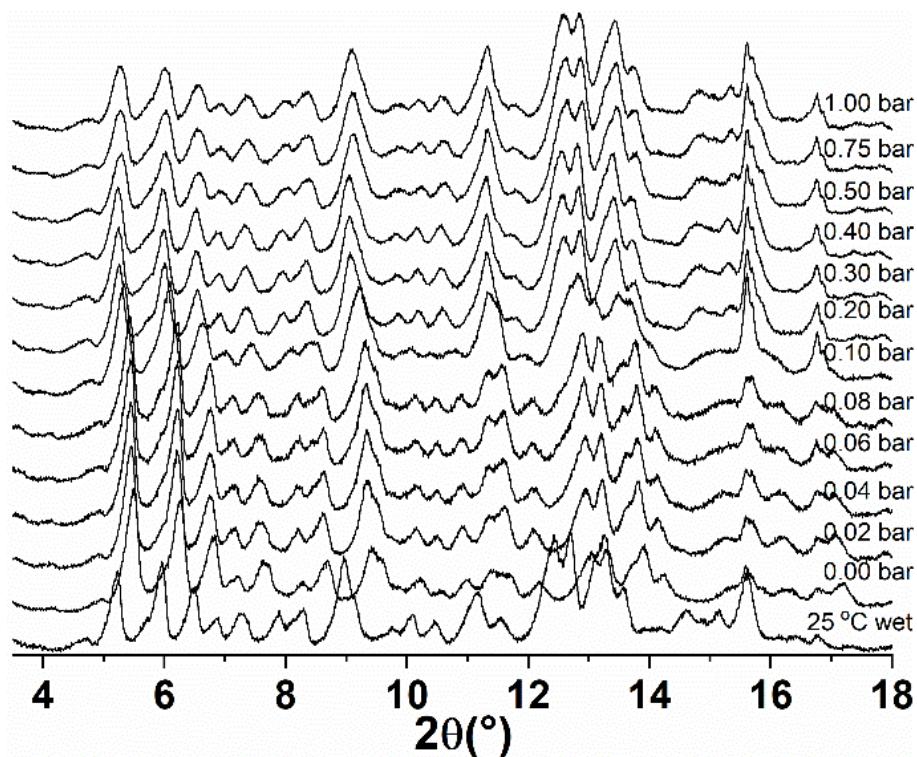


Figure S6: Effect of  $\text{CO}_2$  on X-ray diffraction patterns. Patterns in vacuum and at  $p\text{CO}_2 = 860 \text{ mbar}$ , all at 298 K. The shift in peak positions is due to lattice expansion upon  $\text{CO}_2$  exposure.



*Figure S7:* Comparison of synchrotron XRD patterns of as-prepared samples: dehydrated, exposed to 860 mbar of CO<sub>2</sub> and hydrated (all at 298 K), clearly showing that the d-spacings for the sample exposed to CO<sub>2</sub> is intermediate between dehydrated and hydrated structures.



*Figure S8:* Variable pressure PXRD patterns of (Na,TEA)-ZSM-25 at 298 K.

## Experimental CO<sub>2</sub> isotherms

Table S4: Autosorb isotherm raw data. Sample mass is  $m = 0.1041\text{ g}$

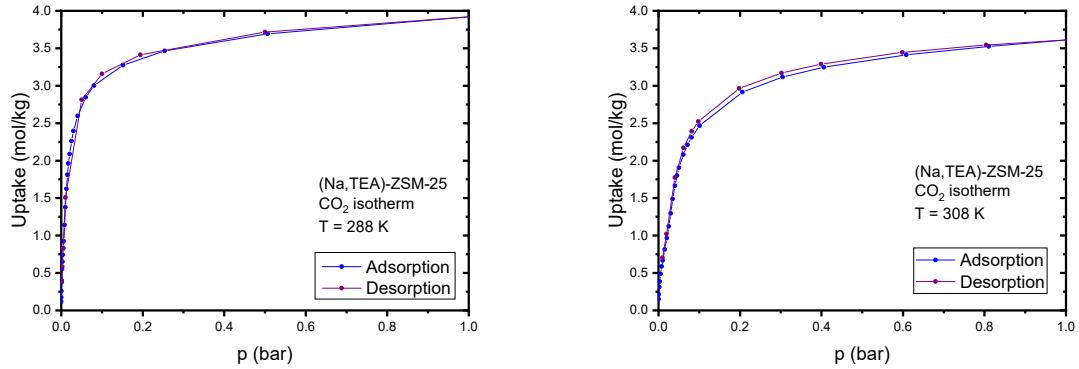


Figure S9:  $\text{CO}_2$  isotherm including desorption branch at 288 K and 308 K, showing minimal hysteresis effects.

Model functions used to describe the volumetric behaviour of ZSM-25

The quadratic volume function used in Figure 4a has the following form:

$$V_s(\bar{q}) = \alpha \cdot (\bar{q} + \beta)^2 + \frac{1}{\rho_0} \quad 11$$

Table S5: Model parameters for quadratic volumetric function in RALF

Quadratic volume function parameter	Value	
$\alpha$	$2.77 \times 10^{-6}$	$\text{m}^3 \text{mol}^{-1}$
$\beta$	0.3	$\text{mol kg}^{-1}$
$\rho_0$	2020	$\text{kg m}^{-3}$

The switch function used in Figure 4b has the following form:

$$V_s = (1 - f(\bar{q})) \cdot V_{s,1}(\bar{q}) + f(\bar{q}) \cdot V_{s,2}(\bar{q}) \quad 12$$

Here  $V_{s,i}(\bar{q})$  are two linear functions of the form:

$$V_{s,i}(\bar{q}) = \alpha_i \bar{q} + \frac{1}{\rho_{i,0}} \quad 13$$

where  $\alpha_i$  and  $\frac{1}{\rho_{i,0}}$  are the slope and intercept, respectively, and  $c$  is a constant.  $f$  is a switch function of the form:

$$f(\bar{q}) = \frac{1}{2} (\tanh\{w(\bar{q} - \bar{q}_{trans})\} + 1) \quad 14$$

where  $\bar{q}_{trans}$  loosely corresponds to the critical amount adsorbed upon which the structural transition occurs and  $w$  describes the steepness of the switch function. The parameters describing this volumetric function are listed in Table S6.

Table S6: Model parameters for switch volumetric function in RALF

Switch volume function parameter	Value	
$\alpha_1$	$5.01 \times 10^{-6}$	$\text{m}^3 \text{ mol}^{-1}$
$\alpha_2$	$4.07 \times 10^{-6}$	$\text{m}^3 \text{ mol}^{-1}$
$\rho_{1,0}$	2020	$\text{kg m}^{-3}$
$\rho_{2,0}$	1879	$\text{kg m}^{-3}$
$n_{trans}$	3.1	$\text{mol kg}^{-1}$
$w$	1.0	

### Single site RALF model

Table S7: Characteristic parameters for  $\text{CO}_2$  (ref. <sup>28</sup>) and (Na,TEA)-ZSM-25 as used in the RALF single site model

Pure component parameters	$\text{CO}_2$	(Na,TEA)-ZSM-25
$P^*$ (MPa)	630	1250
$T^*$ (K)	300	2050
$\rho^*$ ( $\text{kg/m}^3$ )	1515	2640
$M$ (kg/mol)	0.044	$\infty$

Binary parameters	$\text{CO}_2 - (\text{Na,TEA})\text{-ZSM-25}$
$\kappa_{\text{CO}_2,s}$ (quadratic)	-0.22
$\xi_{\text{CO}_2}$ (quadratic)	0.16
$\kappa_{\text{CO}_2,s}$ (switch)	-0.20
$\xi_{\text{CO}_2}$ (switch)	0.25

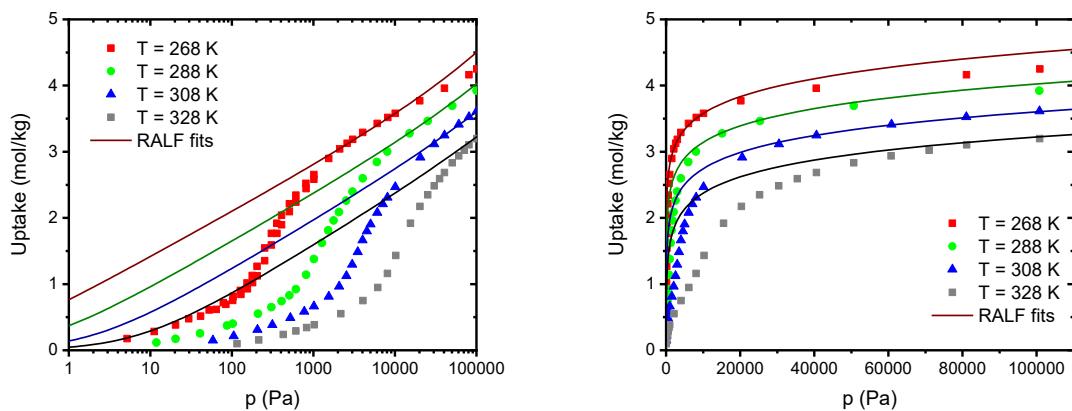


Figure S10: RALF model predictions and experimental data, using a single set of solid characteristic parameters and quadratic volume function.

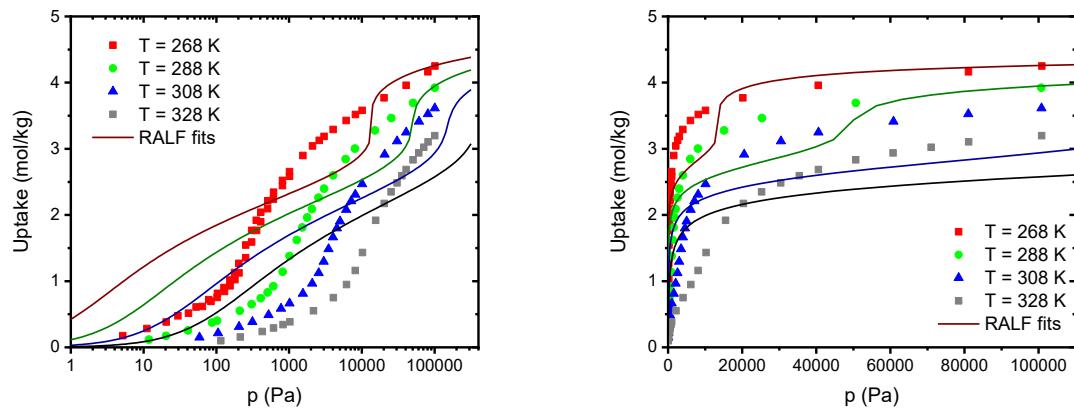


Figure S11: RALF model predictions and experimental data, using a single set of solid characteristic parameters and switch volume function.

### Zero Length Column experiments

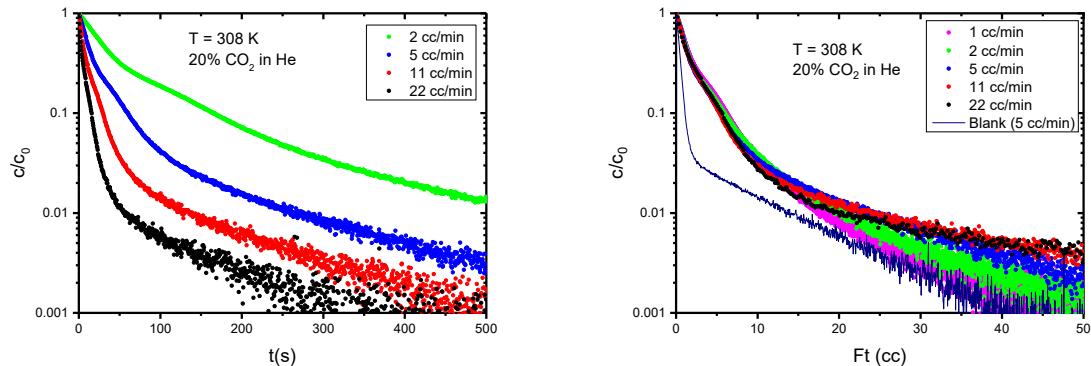


Figure S12: Normalised gas phase concentration as measured by the mass spectrometer, prior to deconvolution. Left)  $c/c_0$  vs. time. Right)  $c/c_0$  vs. flowrate times time ( $Ft$  plot).

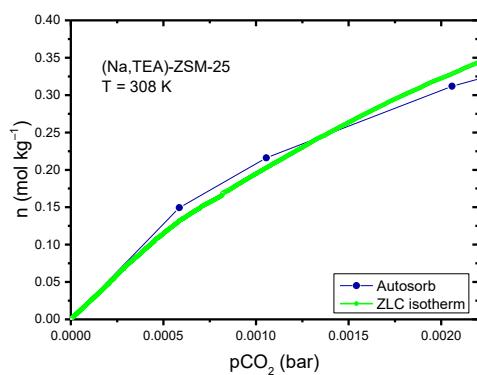


Figure S13: Comparison of Autosorb isotherm and isotherm derived from ZLC data at low flow rates and 308 K. Good agreement of the data at low  $CO_2$  partial pressure is seen for both techniques, suggesting the data collected by volumetric method has reached equilibrium.

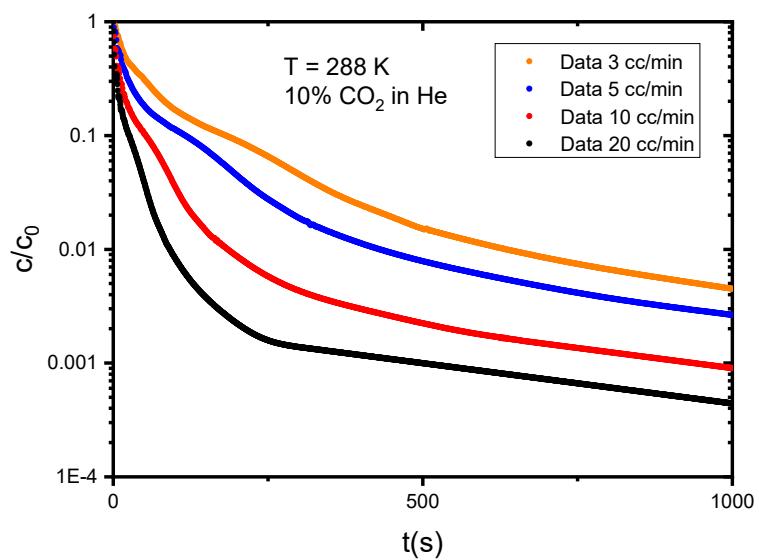


Figure S14:  $c/c_0$  vs time for ZSM-25 at 288 K in  $p\text{CO}_2 = 0.1 \text{ bar}$

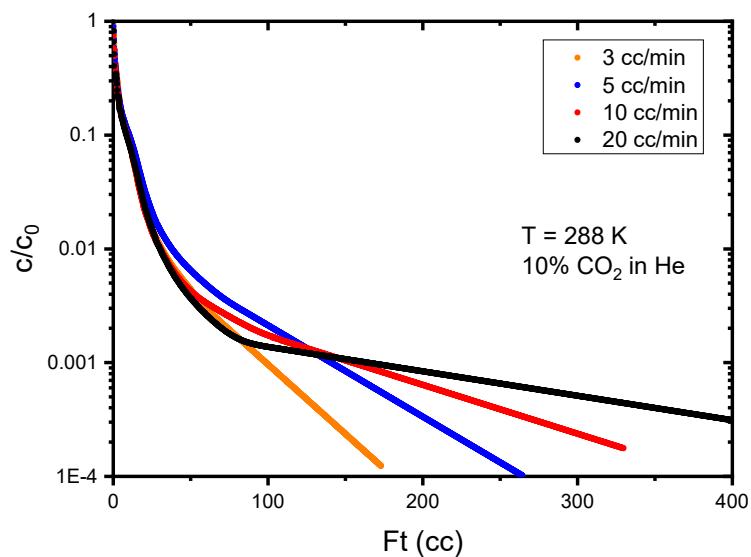


Figure S15:  $c/c_0$  vs.  $Ft$  for ZSM-25 at 288 K in  $p\text{CO}_2 = 0.1 \text{ bar}$

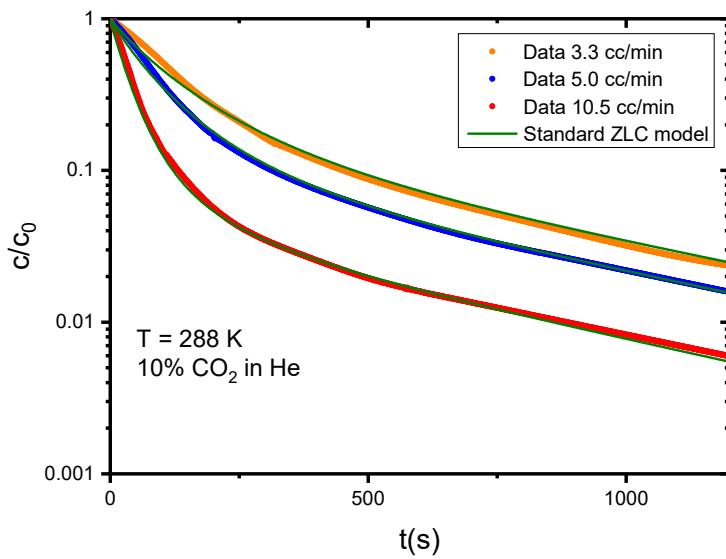


Figure S16: Analysis of 'cut' data using the standard ZLC model assuming linear isotherm (equation Error! Reference source not found.) obtaining an identical value for the diffusivity in the narrow pore structure, i.e.  $D/R^2 = 1.8 \times 10^{-4} \text{ s}^{-1}$ .

Table S8: Model parameters for the standard ZLC model fits to 'cut' and renormalized ZSM-25 data at 288 K

Flow rate (cm <sup>3</sup> /min)	$L_{app}$	$\gamma_{app}$	$D/R^2$ (s <sup>-1</sup> )
3.2	17	0.3	$1.8 \times 10^{-4}$
5.0	26	0.3	$1.8 \times 10^{-4}$
10.5	54	0.3	$1.8 \times 10^{-4}$

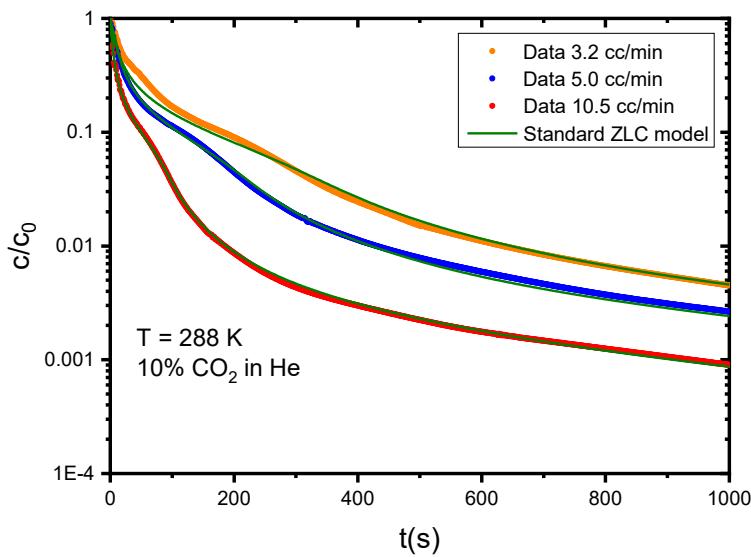


Figure 17: Deconvoluted experimental and simulated ZLC data using RALF model at  $T = 288 \text{ K}$ , showing good agreement using the kinetic model in equation 30, with the parameters in Table S9

## Discussion

Table S9: Kinetic model parameters used to fit full ZLC curves at 288 K

Kinetic model parameter	Value	
$D_0/R^2$	$1.8 \times 10^{-4}$	$\text{s}^{-1}$
$\bar{q}_{\tau,\text{trans}}$	0.6	$\text{mol kg}^{-1}$
$A$	$3.6 \times 10^{-4}$	$\text{s}^{-1}$
$B$	8.3	-

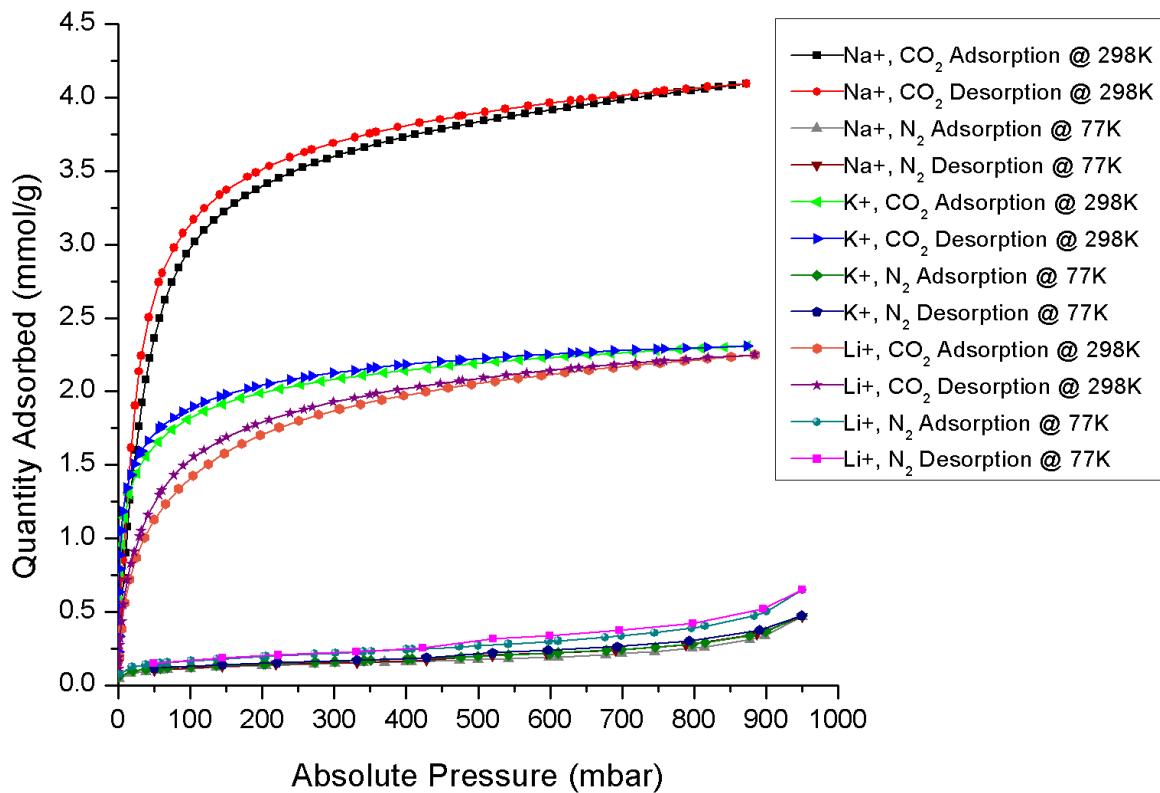


Figure S18: Isotherms for different cation forms of (M,TEA)-ZSM-25 showing that Li and K show a standard type I isotherm, with no step up to 1 bar.

Table S10: Window sizes in dehydrated and hydrated structures of (Na,TEA)-ZSM-25

Cages connected by window	Dehydrated window size (Å)	Hydrated window size (Å)
<i>Ita</i> – <i>d8r</i>	2.6	3.8
<i>d8r</i> – <i>pau</i>	2.4	3.9
<i>pau</i> – <i>d8r</i>	2.6	4.1
<i>d8r</i> – <i>pau</i>	2.5	3.8
<i>pau</i> – <i>oto</i>	2.7	3.0
<i>pau</i> – <i>oto</i>	3.3	3.1
<i>pau</i> – <i>oto</i>	3.3	3.0

<i>oto – phi</i>	2.6	3.5
<i>oto – phi</i>	2.4	3.8
<i>oto – phi</i>	2.3	3.8
<i>oto – phi</i>	2.8	3.5
<i>phi – gsm</i>	2.3	3.4
<i>phi – gsm</i>	2.4	3.4
<i>gsm - gsm</i>	2.4	3.4
<i>phi - oto</i>	2.8	2.8
<i>phi - oto</i>	3.0	2.8
<i>gsm - phi</i>	2.6	3.2
<i>oto – plg</i>	2.5	3.8
<i>oto – plg</i>	2.6	3.8
<i>plg – oto</i>	2.3	3.6
<i>plg – oto</i>	2.5	3.6
<i>phi – oto</i>	2.6	2.5
<i>oto – plg</i>	2.6	3.2
<i>oto – plg</i>	2.2	3.2

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