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PHENYLALANINE AS A COMPLEXING AGENT

by

PAUL A. YEO

A SUMMARY

The complexing power of phenylalanine with protons and transition metal ions is examined. The relevance of phenylananine and the transition metals to biological systems is discussed. Computational methods of calculation were used to determine the stability constants of the complexes and the two main programs, SCOGS and LETAGROP VRID are compared. A program, RWCALCOR, was developed for use in the calorimetric work and the mathematics of this program are given. The experimental details and results are then given and finally discussed.

Phenylalanine is a diet essential amino-acid for homo sapiens and features prominently in the genetic disorder phenylketoneuria. It is also an important precursor to the C_6H_5 -C-C-C group of compounds. The transition metal ions are important features of many enzyme systems and have been found to be bound to a variety of amino-acids in the blood stream.

This work was carried out using the constant medium method where the concentration of a background salt (3.00M NaClO₄) is so high that the activities of the reacting species are kept constant. The Gibbs free energy of the complexation reaction is calculated by determining the stability constant of the reaction and then using the reaction isochore

The stability constant is obtained by following the hydrogen ion concentration with an electrode system of a glass electrode and a standard calomel electrode. The enthalpy of the reaction was determined firectly by using an isothermal titration calorimeter, whence the entropy of the reaction could be found from the Gibbs-Helmholdz relationship

$$\Delta G^{O} - \Delta H^{O} = -T \Delta S^{O}$$

The calculation of stability constants from titration data was achieved by means of computer programs. The main program beed was SCOGS which uses a non-linear least squares technique to minimise the function

This was compared, using both experimental and hypothetical data, with LETAGROP VRID - mathematically a more ♥igorous program.

The protonation results were compared with (i) results for the same ligand in different media and (ii) results for similar ligands in the same medium. This was gone quantitatively for (i) using an extension of the Debye-Hückel equation, and qualitatively for the similar ligands tryptophan and histidine.

The metal ions studied were Cu(II), Ni(II), Co(II), Fe(II) and Fe(III). These were found to obey the Irving-Williams series with phenylalanine and for the ions studied calorimetrically, Cu(II), Ni(II), Co(II), the enthalpy was found to be the governing factor. The nickel and cobalt systems formed an insoluble hydrated 1:2 complex due to its high lattice energy, but iron(II) formed a 1:3 complex. Hydrolysis was seen to be an important factor for copper(II) and even more so for iron(III) as a previously unreported type of complex, Fe₂(OH)₂aa₂, was found.

The calorimetric study of iron(II) was precluded due to oxidation of the system. The calorimetric study of the iron(III) system was abandoned due to difficulties in calculation.

A further study of iron(II) and iron(III) with amino-acids is considered to be a logical extension of the work in this thesis.

To

Mum and Dad

PHENYLALANINE AS A COMPLEXING AGENT

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Acknowledgements

During the course of this work I have incurred the debt of several people and I would like to take this opportunity to thank them.

I would like to thank the Department of Chemistry of the University of St. Andrews for providing the laboratory and library facilities where this work was carried out and the University for providing a maintenance grant to myself.

I would thank the members of staff of the Department for providing both a happy and a stimulating environment for research and particularly Mrs. Patricia Cooper who, with great patience typed this thesis.

My greatest debt, however, is to my supervisor,

David R. Williams, who, over three years, has been a mentor, supervisor,

and teacher, but most of all a friend.

NOMENCLATURE

[]	concentrations
()	activities
A & A'	total concentrations of ligands A & A'
a & a'	concentrations of free A & A'
B & B'	total concentrations of metals B & B'
b & b	concentrations of free B & B'
E	electromotive force
Ej	liquid junction potential
Eo	standard electrode potential of glass/calomel
	electrode pair
F	faraday
f	activity coefficient
Н	total concentration of hydrogen ions
h	concentration of free hydrogen ions
I	ionic strength
Kan	stepwise formation constant for a protonation reaction
K _n	stepwise formation constant for complexation reaction
K _w	ionic product of water
р & р'	number of ligands A and A' in a complex
q & q'	number of central groups (metals) B & B' in a complex
r	number of hydrogen ions in a complex
R	gas constant
s	standard deviation
T	absolute temperature

\mathbf{z}	number of electrons involved in a redox process
ž	average number of ligands A bound to one central
	group B
β_{pqr}^{o}	thermodynamic overall formation constant of ${}^{A}_{\ p}{}^{B}_{\ q}{}^{H}_{\ r}$
β _{pqr}	concentration overall formation constant of ${}^{A}p{}^{B}q{}^{H}r$
$\triangle G_o^o$	thermodynamic standard Gibbs free energy change
△G° △H°	thermodynamic standard enthalpy change
$\triangle s_o^o$	thermodynamic standard entropy change
	where thermodynamic refers to water as the
	standard solvent
$\triangle G^{\mathbf{o}}$	standard Gibbs free energy change
∨ _{Ho}	standard enthalpy change
$\triangle s^{o}$	standard entropy change
	with 3.00 M (Na)ClO $_4$ as the standard solvent

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DECLARATION

I declare that this thesis is my own composition, that the work of which it is a record has been carried out by myself and that it has not been submitted in any previous application for a Higher Degree.

This thesis describes the results of research carried out at the Chemistry Department, United College of St. Salvator and St. Leonard, University of St. Andrews, under the supervision of Dr. David R. Williams since 1st of October, 1968.

CERTIFICATE

I hereby certify that Paul Yeo has spent eleven terms of research work under my supervision, has fulfilled the conditions of Ordinance No. 16 (St. Andrews) and is qualified to submit the accompanying thesis in application for the degree of Doctor of Philosophy.

DAVID R. WILLIAMS

CHAPTER I

INTRODUCTION

The acquisition of knowledge about living systems has proceeded remarkably in the last decade. New techniques have played a large part in these advances but the interplay of the various disciplines of co-ordination chemistry, inorganic biochemistry, organometallic chemistry, enzymology and molecular biology, has made a significant contribution. The theoretical advances of the thirties, culminating in Pauling's "The Nature of the Chemical Bond" , inspired Hedges to write "Inorganic Chemistry is again coming into its own"2. This comment is relevant again today, but now the renaissance is due to a more balanced advance in both theoretical and experimental fields. The discovery of new experimental spectroscopic techniques, combined with an increased sophistication of instrumentation generally, has revealed new areas of study and has extended existing areas beyond recognition. The development of high speed digital computers has had a profound effect on science and technology, and chemistry is no exception,

The division of chemistry into physical, inorganic and organic has always been recognised as an oversimplification and these divisions, in recent times, have become increasingly less meaningful. Today, this is shown by the vast field of organometallic chemistry, and by the fact that entire journals are devoted to physical organic chemistry. And thus, the unification of scientific disciplines has produced a series of bastardised names for these new fields of research (e.g. organometallic chemistry and inorganic biochemistry). Inorganic

biochemistry is a term that was coined by Williams³ to describe the study of inorganic, particularly metal, compounds in biological systems and the use of metal co-ordination compounds as models for metalloenzymes.

as long ago as 1500 B.C., when a Prince Iphyclus was cured of his impotence by the administration of a suspension of rust in wine⁴, but it is only in the last twelve years that inorganic biochemistry has emerged as a field in its own right. Of the eighty-seven naturally occuring elements, twenty can be considered as essential to the human body and, of these, three classes exist; (a) the non-metals, H, C, O, N, S, P, Cl, Br, F and I; (b) the bulk metals, Na, K, Ca, Mg; and (c) the trace metals, Mn, Fe, Co, Cu, Zn and Mo. The remaining metals, particularly the heavy metals Hg and Pb, are becoming increasingly important due to the pollution of the environment by modern day living. Knowledge of the role of the above classes of elements in the body is quite well established;

class (a) form (i) simple organic molecules - the amino acids, which polymerise to peptides which in turn help to form highly complicated structures such as DNA and proteins, and, (ii) the more complicated structures steroids, lipids and carbohydrates;

class (b) is also subdivided, (i) the charge carriers, K⁺ and Na⁺, these will almost certainly be aquated cations, and (ii) Mg²⁺ (aq) and Ca²⁺ (aq), which are of prime importance in the action of adenosine triphosphate (ATP), the most important store of energy in the human body, and also act as structure formers and triggers in the body³;

class (c) has divisions that are not as well defined but, essentially, Cu, Fe, Mo, and to some extent Mn, act as catalysts in redox reactions whereas Zn controls pH by hydrolysis. The rôle of cobalt is not yet clearly understood at the molecular level except for its action in corrinoid enzymes⁵. When the complexing power and the donating ligands are examined, the chemistry of the two classes of metals are contrasted and the reasons for their differing biological rôles are revealed.

 $\frac{\text{Table } \mathbf{1}.}{\text{Classification of metal ions in vivo}}$

	Na, K	Mg, Cu, (Mn)	Zn, (Co)	Cu, Fe, Mo, (Mn)
Ligand atoms	О	0	N & S	N & S
Strength of bond*	5,85	13,12	23.41	36.24
i.e.	weak	moderate	strong	strong

^{*}These figures refer to -\Delta H, (enthalpy kJ mol -1) for the formation of the metal -EDTA complex. In each group the figure for the first metal is quoted 6..

At the pH of blood (7.35-7.42), the extent of complexation of class (b) is small and relatively unimportant; conversely, class (c) forms strong complexes at this pH and therefore the study of these complexes and their formation is of great biological importance.

the importance of stereochemistry to biological systems cannot be underestimated; the reproduction of genetic material is dependent upon the double-helix structure of DNA, and the action of most metalloenzymes is dependent upon the geometry of the metal 7-10. As a particular example, the complexes of iron show a remarkable variation in co-ordination and reactivity in the body. Nature equips iron with a stereochemistry that is irreproducible in solution, but one of the most wide spread in mammals, i.e. haemoglobins, although the formation of a macromolecule which can reversibly complex molecular oxygen has been imitated using a polystyrene film 11. In nature's macromolecule, iron has, essentially, octahedral co-ordination where four planar positions are occupied by the donor nitrogens of a porphyrin ring and an axial position by an imidazole nitrogen from a histidyl residue 12.

Figure 1.
The iron-porphyrin ring system.

The function of the sixth co-ordination site is to reversibly bind and release molecular oxygen. Cytochrome C has the same basic structure, but having histidyl residues occupying both of the axial sites. These histidines are portions of peptide chains which contain cysteine residues which are in turn attached to carbons (1) and (2). Cytochrome C is an electron-transferring protein and is intimately linked with the interconversions between the ferrous and ferric states of the haem iron 12. The third type of complex is peroxidase, where the sixth position is used for complexing hydrogen peroxide. Here, as in the haemoglobins, the bond between substrate and iron is continuously made and broken but, unlike the haemoglobins, the iron is oxidised to the iron (III) state, although there is evidence that it is iron (IV) 13.

Whilst kinetics and stereochemistry play a large part in biological systems, thermodynamics has its place, as is shown by the importance of ATP and the frequency with which it is invoked as taking a part in biological reactions.

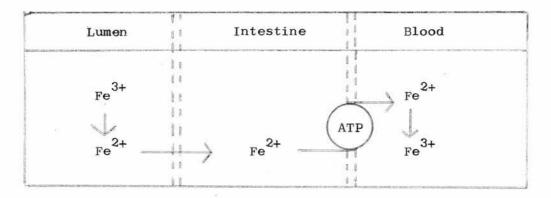


Figure 2

The active transport mechanism for intestinal regulation and control of iron uptake.

ATP is also essential to the biosynthesis of squalene, the precursor of the steroid system 14 .

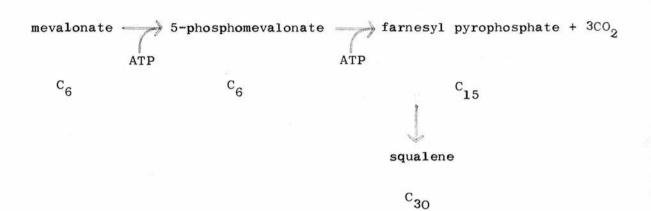


Figure 3 The biosynthesis of squalene.

The conventional view of the mode of action of ATP is that the hydrolysis of one phosphate group provides a large amount of energy to drive other reactions. Recently, however, there has been much discussion concerning the validity of this theory $^{15-17}$. Unfortunately, the possibility of catalysis by magnesium ions was omitted from the discussion 18 .

More recently, a "breakthrough" in the action of aspirin was reported 19. Again the possible importance of a metal ion was omitted from consideration even though speculation has been rife for many years 20. The understanding of rôle of aspirin is that it inhibits the formation of prostaglandins but in 1954 20 Schubert suggested that the rôle of aspirin was to "... remove or inactivate excess copper present in an intracellular site." and, as yet, these two theories have not been linked.

Even though the field of inorganic biochemistry is expanding rapidly,

its influence is not yet as widespread as its importance due to the need for more relevant experimental data.

The methods currently available for studying the formation, electronic structure and three-dimensional structure are numerous but can conveniently be classified into spectroscopic, potentiometric and calorimetric techniques.

Spectroscopy

- (a) Mössbauer:- The use of this nuclear gamma-ray resonance spectroscopy has been extensive for iron containing species, and for samples in the solid state but, due to the widespread abundance of iron in biological systems, this is no real constraint as it has several advantages over other methods of resonance spectroscopy. Firstly, there are no interfering signals from other atomic species and secondly, the Mössbauer nuclide does not perturb the electronic environment being studied. Mössbauer has been used to study the haemoproteins, haem prosthetic groups and iron-sulphur proteins.
- (b) Nuclear Magnetic Resonance: This technique can be applied to any compound containing a nucleus with a spin, but is usually applied to the simplest nucleus, that of hydrogen, and this yields volumes of information about any species containing this nucleus. Both complex molecules ²³ and simple complexes ²⁴ of biological importance have been studied by nmr.

- (c) Nuclear Quadrupole Resonance: For a nucleus to show a nqr signal it must have a nuclear spin of one or greater (i.e. I > 1). The main nuclei studied have been the halogens, except fluorine 19 which has no nqr, and cobalt -59^{25} ; this means that nqr has had no significant effect on the study of biological complexes as yet, although it may be possible to apply the technique with some success.
- (d) Electron Paramagnetic Resonance: Complexes with unpaired electrons will give an epr signal, hence, Cu(II), Fe(III), Co(II) and Mo(V) can be studied by this technique. The elucidation of the interaction between molybdenum and riboflavin was carried out by using epr and its importance emphasised. "... the case of adjacent radicals is one of great importance in biological systems. Electron paramagnetic resonance is almost the only method which will detect such a situation." 18
- (e) Crystallography:- X-ray spectroscopy is by far the most important branch of crystallography with the more precise neutron and electron diffraction playing only a minor part. The elucidation of the structure of complex molecules has played a great part in the advances made in the biological sciences in the last twenty-five years. This has been recognised by the award of the Nobel Prize several times to crystallographers, including to Hodgkin for the elucidiation of the structure of insulin and vitamin B₁₂.
- (f) Optical Rotatory Dispersion and Circular Dichroism:- These techniques are used with optically active complexes and hence involve a degree of preparative difficulty. They have been applied with success to complexes of transition metals and optically active amino acids 27,28.

(g) Infra-Red and Ultraviolet Spectroscopy: These more conventional forms of spectroscopy continue to yield a great deal of information about the electronic configuration of the central metal ion, the type of bonds formed and the extent of formation of complexes 29.

Potentiometry

This is a method of determining the activity of a species by means of an electrode pair and when applied to complex chemistry it is possible to evaluate the formation constants of complexes in solution. The glass electrode is by far the most important as this determines the hydrogen ion activity in solution; this in turn means that a reaction dependent upon hydrogen ion activity can be followed in solution. Ligands that complex with metal ions also associate with protons in solution and so the complex formation reaction, being competitive, is pH dependent. This will be dealt with in greater detail in Chapter II.

There are several other ion-sensitive electrodes commercially available but as yet they do not have the applicability, stability and sensitivity of the glass electrode. The most widely used of these electrodes are the fluoride electrode and the calcium electrode although new electrodes, such as amino acid electrodes 30, are becoming more widely used.

Calorimetry

This technique gives the enthalpy of, i.e. the strength, of a metal-substrate bond being formed in solution, and is usually used

conjunction with potentiometry. Together these methods give the Gibbs free energy, $\Delta \, \text{G}^{\text{O}}$, the entropy, $\Delta \, \text{S}^{\text{O}}$ and the enthalpy, $\Delta \, \text{H}^{\text{O}}$ changes involved in the formation of complexes. This will be given more consideration in Chapter II.

The methods chosen to study complexes, depend upon the complexes chosen for study. Either natural systems can be examined, which involves such difficulties as arise from the complexes involving high molecular weight proteins and, in general, the higher the molecular weight the more limited are the solution studies, so that a wider range of techniques are necessary, or simple, complexes may be researched and the results extrapolated to apply to biological systems. The latter has been the approach used by Perrin's school (Canberra) and the collection of large quantities of data on simple systems have been combined to produce important biological conclusions 31.

This also, has been the approach used in the present study, where the complexing between phenylalanine (an important biological amino acid) and iron (II and III), cobalt (II), nickel (II), copper (II) and protons (Fe, Co & Cu are trace metals in vivo) is examined using in vitro potentiometry and calorimetry. For aqueous complex studies, these two techniques are the most economical in terms of conclusions yielded per given amount of data and time. This economy is further enhanced by analysing the results using powerful computer programs.

The <u>in vivo</u> roles of the metals used have already been mentioned, phenylalanine's importance is also worth consideration. It is diet essential amino acid for <u>homo</u> <u>sapiens</u>, where it has two main reaction paths (figure 5)

Figure 5
Phenylalanine in vivo

To the right hand side, tyrosine is formed by the action of phenylalanine hydroxylase, and from this the important pigment melanin. To the left hand side, phenylpyruvic acid and phenylacetic acid are formed by transamination; normally this reaction occurs only to a minor extent but if there is a lack of phenylalanine hydroxylase this reaction predominates and produces an excess of the acids which cause brain damage. This disease is called phenylketonuria and is an inborn disorder, hence, all newborn children in Britain are tested for an excess of phenylalanine which, if present, is treated by giving a phenylalanine-free diet to the child. In plant life, too, phenylalanine has an important role, as it stands at the head of the biosynthetic sequence that leads to the C₆-C-C-C class of compounds, e.g. cinnamic acids, and is also the precursor of terphenyls and numerous alkaloids including mescalin 32.

CHAPTER II

THEORETICAL CONSIDERATIONS

The study of complex formation in solution, in common with most branches of chemistry, has a series of milestones, represented by the names of scientists, who contributed to the field. Werner was the founder of modern co-ordination chemistry and his paper on the stereochemistry of complexes sinspired Bodlander and N. Bjerrum and N. Bjerrum the acceptance of the constant ionic media method (see later) and the work of J. Bjerrum and Schwarzenbach in the late 1930's and early 1940's, which was closely followed by the work of Leden, the theoretical work of the Rossotti's and the incalculable contribution of Sillen, whose sad death was announced recently 39.

Consider the formation of a complex $A_p B_q H_r$. In aqueous solution; the complex will be associated with a number of water molecules and the formation can be represented by

$$pA(H_2O)_w + qB(H_2O)_x + rH(H_2O)_y \rightleftharpoons A_pB_qH_r(H_2O)_z + (pw + qx + ry - z)H_2O$$
[1]

In practice the activity of free water is assumed constant and the water of hydration is omitted from equations

Hence
$$pA + qB + rH \rightleftharpoons A_pB_qH_r$$
 (2)

^{*} Nomenclature is given on page i.

The values of p, q and r are integers, positive or zero for p and q, but possibly negative for r as hydrolysed species are formed. The constant used to define the system in terms of activities is called the thermodynamic formation constant.

$$\beta^{o}_{pqr} = \frac{(A_{p}B_{q}H_{r})}{(A)^{p}(B)^{q}(H)^{r}}$$
[3]

$$= \frac{\left[A_{\mathbf{p}}^{B_{\mathbf{q}}^{H_{\mathbf{r}}}}\right]}{\left[A\right]^{\mathbf{p}} \cdot \left[B\right]^{\mathbf{q}} \left[H\right]^{\mathbf{r}}} \cdot \frac{f_{A_{\mathbf{p}}^{B_{\mathbf{q}}^{H_{\mathbf{r}}}}}}{\mathbf{p}f_{A} \cdot \mathbf{q}f_{B} \cdot \mathbf{r}f_{H}}$$
[4]

If the activity coefficients of all species are held constant then a new constant can be defined in terms of molar concentrations

$$\beta_{pqr} = \frac{[A_p B_q H_r]}{[A]^p, [B]^q, [H]^r}$$
 [5]

A third constant sometimes encountered is the mixed constant, so called because some terms are concentrations and some are activities (usually only the hydrogen ion is quoted as an activity).

The simplicity of these definitions does not extend into practice and many problems arise. The use of equation [4] is limited to systems where, either the activity coefficients can be calculated, and in systems where there are numerous stepwise species this is difficult, or where the results can be extrapolated to zero ionic strength. Equation [5] is used frequently, but the thermodynamics of the system can only be compared to other systems with a similar ionic background. Activity coefficients may be held constant by working in a solution of sufficiently

high ionic background such that ion pair effects are constant. This can be achieved by using a salt which contains ions having no complexing tendencies, and so the usual choice is sodium, or sometimes lithium, perchlorate. In monitoring the reaction by potentiometry, use is usually made of the Nernst equation

$$E = E^{0} + \frac{RT}{zF} \cdot \ln \frac{(K)^{k} \cdot (L)^{1}}{(M)^{n} \cdot (N)^{n}}$$
 [6]

(For reaction kK + 1L = mM + nN)

This calls for a definition of unit activity (i.e. the standard state) of the species present.

For the glass electrode

$$E = E^{O} + \frac{RT}{zF} \quad ln (H)$$
 [7]

The choice of standard state is arbitrary and related to the selection of a standard solvent.

For a cell
$$- Pt(H_2) \begin{vmatrix} x^-ClO_4^- \\ H^+ Na^+ \end{vmatrix} Ag, AgX +$$

If the standard solvent is water then

$$E = E_{aq}^{o} - \frac{RT}{F} \ln [H^{+}][X^{-}] - \frac{2RT}{F} \ln f$$

$$E_{aq}^{o} = \lim_{[H^{+}][X^{-}]} C_{tot} \rightarrow 0$$

$$E_{tot}^{o} \rightarrow 0$$

$$E + \frac{RT}{F} \ln [H^{+}][X^{-}]$$

This implies,

$$\begin{array}{ccc} & \text{limit} & \text{f = 1} \\ \text{[H}^+] & \text{[X}^-] & \text{C}_{\text{tot}} \rightarrow 0 \end{array}$$

(where CTOT =
$$\frac{1}{2}$$
 \sum_{i} Ci Zi = [X] + [ClO₄] = [H] + [Na] and

where f is the mean activity coefficient).

But, if the standard state is chosen as a solvent with a defined composition then

$$E = E_{\text{NaX}^{0}} - \frac{RT}{F} \ln [H^{+}][X^{-}] - \frac{2RT}{F} \ln f$$

$$E_{\text{NaX}^{0}} = \lim_{[H^{+}][ClO_{4}] \to 0} \left(E + \frac{RT}{F} \ln [H^{+}][X^{-}]\right)$$

$$[X^{-}][Na^{+}] \to C_{\text{tot}}$$
[9]

This implies,

$$\begin{array}{ll}
\text{limit} & \text{f'} = 1 \\
[\text{H}^+] [\text{ClO}_4^-] \to 0 \\
[\text{X}^-] [\text{Na}^+] \to c_{\text{tot}}
\end{array}$$

where f' is the mean activity coefficient.

Hence these results obtained may be extrapolated to the standard solvent, but Biedermann has shown this to be unnecessary as in 3.00 M NaClO₄, the sum of the concentrations of the ions in a reaction $(A^- + B^+ \rightleftharpoons AB)$ does not exceed 0.15 M then the error in a potentiometric reading does not exceed $\stackrel{+}{=}$ 0.1 mV. This latter approach is the one used in this work.

The thermodynamic quantity obtainable from the stability constant is the Gibbs free energy of the reaction, which is related to the stability constant by the reaction isotherm 40 .

$$\Delta_{G}^{o} = - RT \ln \beta,$$
 [10]

where ΔG^{o} is the standard Gibbs free energy, with 3.00 M sodium perchlorate as standard solvent. Further thermodynamic parameters can be obtained by determining β_{pqr} at different temperatures and then invoking the reaction isochore 40 ,

$$\left(\frac{\mathbf{\lambda} \ln \beta}{\mathbf{\lambda} T}\right)_{p} = \frac{\Delta_{H}^{o}}{RT^{2}} \qquad [11]$$
Integrating
$$\ln \frac{\beta_{2}}{\beta_{1}} = -\frac{\Delta_{H}^{o}}{R} \left(\frac{1}{T_{2}^{2}} - \frac{1}{T_{1}^{2}}\right) \qquad [12]$$

but this is assuming that $\triangle H^0$ does not vary with temperature. This is very often a false assumption 42 , and so, the method is not reliable.

The enthalpy of formation can also be obtained, directly, by calorimetry, and by then using the Gibbs-Helmholtz equation 40 ,

$$\Delta G^{\circ} = \Delta H^{\circ} - T \Delta S^{\circ}$$
 [13]

values of the entropy of the reaction can be calculated. The enthalpy change is related to the difference in the bond and solvation energies of the products and reactants, whereas the entropy change is related to the change in randomness which accompanies the reaction.

Influence of the medium on the thermodynamic quantities,

The relationship between the quantities obtained in 3.00 M sodium perchlorate and the quantities, ΔG_0^0 , ΔH_0^0 and ΔS_0^0 , referring to the more usual thermodynamic standard state, pure water, is worthy of consideration, if, for no other reason, at least to compare results for the same reaction in different media. The thermodynamics of the

formation of cadmium (II)-halide and -acetate complexes have been studied at various ionic strengths 43 (I) and it was found that the thermodynamic quantities are only slightly affected by changes of I in the range 0.3 - 3.0 M. The heat of ionisation of water ($\triangle H_W$) has also been determined at various ionic strenths 44,45 and this quantity varies linearly with I in the range 0.5 - 3.0 M. $\triangle G^{\circ}$, however passes through a minimum at I \approx 0.5, which is due to a sharp increase in the $\triangle G^{\circ}$ term up to .5M (fig.6a). This minimum has also been noted by Dyrssen et al for several other systems 46 (Figure 6b).

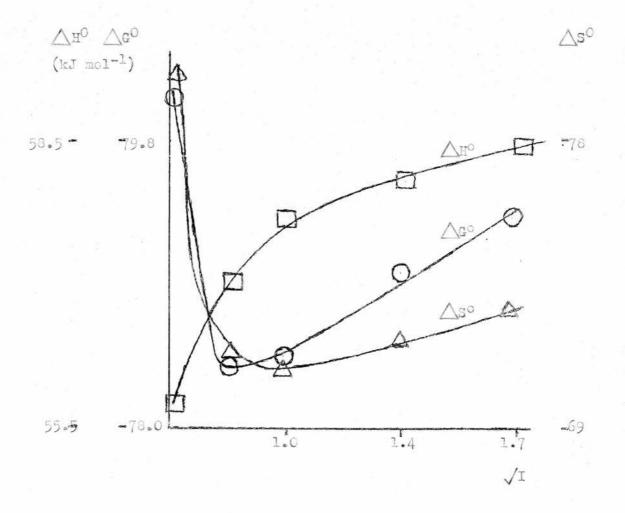


Figure 6a, Variation of ΔG^{O}_{W} , ΔH^{O}_{W} and ΔS^{O}_{W} with ionic strength.

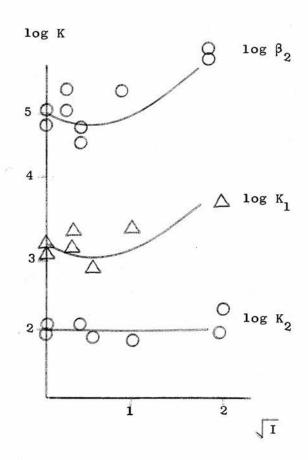


Figure 6b. Variation of $\triangle G^{0}$, $\triangle H^{0}$ and $\triangle S^{0}$ with $\sqrt{\Gamma}$ for Ag+ Cl⁻ system

The significance of the thermodynamic quantities:-

Enthalpy.

Complex formation is favoured by negative heat changes. Enthalpy changes, which are independent of the composition as a whole 47, in aqueous solution are the heat changes which accompany the replacement of water by other ligands. Large (-40 kJ mol -1) heat changes are attributed to the formation of essentially covalent bonds. The change

in standard enthalpy, Δ_H^o , can be considered to consist of two portions, Δ_{H_I} , the internal part, and Δ_{H_E} , the environmental part. Δ_{H_I} can be considered to be the heat change for the reaction

$$pA(g) + qB(g) + rH(g) = A_p q^H r(g)$$
 [14]

To evaluate \triangle H_I it is necessary to determine the heats of hydration of the ligand, the metal ion, the proton and the complex as is in figure 7.

$$pA(H_{2}O)_{w} + qB(H_{2}O)_{x} + rH(H_{2}O)_{y} \xrightarrow{\triangle_{H}O} A_{p}B_{q}H_{r}(H_{2}O)_{z} + (pw + qx + ry - z)(H_{2}O)$$

$$\downarrow -\triangle_{H_{h}, A_{p}B_{q}H_{r}}$$

$$A_{p}B_{q}H_{r}(g) + (pw + qx + ry)H_{2}O$$

$$\downarrow -\triangle_{H_{I}}$$

$$pA(g) + qB(g) + rH(g) + (pw + qx + ry)H_{2}O$$

$$\downarrow -p\triangle_{H_{h}, A}$$

$$pA(H_{2}O)_{w} + qB(g) + rA_{(g)} + (qx + ry)H_{2}O$$

$$\downarrow -q\triangle_{H_{h}, B}$$

$$pA(H_{2}O)_{w} + qB(H_{2}O)_{x} + rH_{(g)} + ryH_{2}O$$

Where \triangle_{h}^{H} , $A_{p}^{B}{}_{q}^{H}{}_{r}$, \triangle_{h}^{H} , B_{r}^{A} , \triangle_{h}^{H} , A_{r}^{A} and \triangle_{h}^{H} , A_{r}^{A} are the heats of hydration of $A_{p}^{B}{}_{q}^{H}{}_{r}$, B_{r}^{A} , A_{r}^{A} and A_{r}^{A} respectively.

Determination of the internal part of $\triangle H^0$.

 Δ_{T} is then given by Hess' law

$$\Delta_{H_{I}} = \Delta_{H}^{o} + q\Delta_{h, B} + p\Delta_{h, A} + r\Delta_{h, H} - \Delta_{h, A_{p}B_{q}H_{r}}^{H}$$
[15]

and the environmental part by

$$\Delta H_{E} = \Delta H_{O} - \Delta H_{I}$$
 [16]

The heats of hydration of several metal ions have been reported 48, but values of the heats of hydration of ligands, and of complexes, are much more difficult to obtain. Values for ligands can be obtained from thermodynamic cycles, which involve dissolving the ligand in acid solution. Unfortunately, an experimental value of the electron affinity of the ligand is required 49, and few values exist. At the present time there is no satisfactory way of evaluating the heats of hydration of complex ions, however, values can be calculated using the Born charging equation 49

$$\Delta H_{h} = -\frac{10.Z^{2}.e^{2}}{2.R} \left(1 - \frac{1}{D} + \frac{T}{D^{2}} \cdot \left(\frac{\partial D}{\partial T} \right)_{P} \right)$$
 [17]

where Ze = product of charge on ion and electronic charge

R = radius of central ion plus diameter of water molecule, nm,

D = dielectric constant of medium

T = temperature, K.

The values obtained from using equation [17] should be considered approximate, but can give a guide to trends along a series of metal ions or of similar ligands.

Entropy.

The change in entropy on complexation of a metal ion is very dependent upon the ligand. If the ligand is uncharged, then solvent will be less ordered around the complex than the metal ion, but if the ligand is charged then, on complexation, there will be a decrease in the number of ions, neutralisation of the electrical charge, attenuation of the remaining charge, and displacement of water from the hydration spheres of the reactants. For a chelating ligand, further factors, such as loss of configurational entropy, must be taken into account. Reactions are favoured by an increase in entropy and so the factors favouring complexation are a decrease in the number of ions, neutralisation of charge, and a less ordered solvent. Those factors inhibiting the formation of complexes are the loss of translational entropy to vibrational and rotational entropy, and the loss of rotational entropy for polyatomic ligands. For most complex formation reactions, however, the ligational entropy changes are positive 50,51.

Gibbs Free Energy

The Gibbs free energy is the criterion for the thermodynamic feasibility of a reaction and, for a reaction to proceed, ΔG^0 must be negative. Its dependence on the enthalpy and entropy is shown in equation [13] and so a reaction is possible with either unfavourable entropy or unfavourable enthalpy as long as the favourable variable is predominant.

 $\frac{\text{Table II}^{50}}{\Delta G^{0} \text{ upon } \Delta H^{0} \text{ and } \Delta S^{0}.*}$ Dependence of ΔG^{0} upon ΔH^{0} and $\Delta S^{0}.*$

AB	- ∆ G ^o	∆ H°	Δs°
[CaOOCH] ⁺	8,11	4.17	41.8
[CaOOCCH ₃] ⁺	7.07	3.76	37.6
[CeSO ₄] ⁺	19.20	19,66	129,6
[MgOOCH] +	8.11	-7.5	4.2
[MgOOCCH3]+	7.07	-6.27	4.2
[CeClO ₄] ²⁺	10.87	-49.35	-129.6

 $^*\Delta_G{}^o$ and $\Delta_H{}^o$ in kJ mol⁻¹; $\Delta_S{}^o$ in J K⁻¹ mol⁻¹

It can be seen from Table II that a negative ΔG^o is not sufficient to describe a reaction and ΔH^o and ΔS^o are valuable parameters to determine.

Methods of Calculation

In considering the formation of the complex ${}^{A}_{p}{}^{B}_{q}{}^{H}_{r}$ (Equations [1] and [2]) the Gibbs free energy change is given by equation [10].

i.e.
$$\Delta G^{\circ}$$
 = - 2.303 RT log β_{pqr}

Hence $\triangle G^{O}$ can be obtained directly from a knowledge of the formation constant. In this study, the formation constants were obtained by following the hydrogen ion concentration during a titration of the

reactants A and B. For initial calculations, the function \bar{Z} , defined as the number of ligands bound to each central group 38 , was plotted against -log a, which is known as the "formation curve". This treatment of data is only useful for mononuclear complexes as, for polynuclear complexes, (including protonated species) the function \bar{Z} has little signficance. Mathematically \bar{Z} is defined as

$$\bar{Z} = \frac{[AB] + 2[A_2B] + \dots}{[B] + [AB] + [A_2B] + \dots} = \frac{\sum_{1}^{N} n\beta_n a^n}{\sum_{0}^{N} \beta_n a^n}$$
[18]

Practically, \bar{Z} can be determined from a knowledge of the total concentrations of A, B and H in solution, the values of the formation constants of any species AH_r and the free hydrogen ion concentration, h.

From [18] $\bar{Z} = \frac{\text{Bound ligand concentration}}{\text{Total metal concentration}}$

Bound ligand concentration = Total ligand - (Free ligand + protonated ligand = A-(a + $\sum_{1}^{N} \mathbf{Q}_{n} \beta_{n} h^{n}$) $= A-a(1 + \sum_{1}^{N} \beta_{n} h^{n})$ [19]

But the free ligand concentration is obtained from a mass balance equation

$$H = h - \frac{h}{W_k} + \sum_{1}^{N} n[AH_n]$$

$$= h - \frac{h}{W_k} + \sum_{1}^{N} an\beta_n h^n$$
i.e. $a = (H - h + h/W_k) / \sum_{1}^{N} n\beta_n h^n$ [20]

hence from [19] and [20] Z can be obtained.

The transformation of \bar{Z} , -log a plots into formation constants, by graphical means, has been extensively reviewed by Rossotti and Rossotti 38 . The methods used in this study were numerical methods using high speed digital computers (see Chapter III). The aim was to reproduce the experimental \bar{Z} , -log a curve using constants obtained from the computer programs.

The change in enthalpy, $\triangle H^{\circ}$, was measured directly by calorimetry. The concentrations of the species in the calorimeter were determined by using HALTAFALL⁵², a computer program, and then changes in concentration, together with the corrections necessary for the heats of formation of water, of deprotonation and of hydrolysis were calculated using RWCALCOR (Chapter III and Appendix 1).

This treatment yields the experimental parameters, heat evolved and change in concentration of species under study. From this—the change in enthalpy can be calculated numerically (Chapter III) or graphically. A plot of heat evolved per mole of metal against the degree of formation, \bar{Z} , will yield ΔH_1^0 at $\bar{Z}=1$, ΔH_2^0 at $\bar{Z}=2$ etc., for simple systems with well separated heats.

 Δ S° can now be calculated from equation [13].

CHAPTER III

COMPUTATIONAL ASPECTS

The advent of the computer has had a profound effect on the chemists' approach to numerical problems. It would not be an exaggeration to say that crystallography has been revolutionised, and even menial tasks, such as drawing mass spectrometry spectra, are lending themselves to programing 53.

Crystallography was the first branch of chemistry to use the computer nearly twenty-years ago ⁵⁴ as the type of calculation carried out was fairly straight forward, but long and tedious. Perhaps the biggest strides taken in chemistry, using a computer, have been in the field of quantum mechanics. The large storage space and the speed at which calculations are performed in the latest generation of computers have enabled quantum chemists to tackle hitherto impossible calculations ⁵⁵.

Computers are used extensively in analytical chemistry ⁵⁶ for processing data obtained by physical methods. Chromatography, mass spectrometry, nmr and chemical literature lend themselves to the setting up of libraries of information for future comparison and retrieval. Phase equilibria ⁵², nmr ⁵⁷, esr ⁵⁸ and calorimetry ⁵⁸ have prompted programs where trial parameters are used to produce simulated distribution curves, spectra and thermograms respectively. General curve analysis is also employed in spectroscopy and electroanalytical chemistry. Another branch of chemistry where the computer has had a large impact is in the calculation of formation constants by various numerical approaches. These computations have been the

subject of two recent reviews 60,61 and have inspired a great deal of interest in solution chemistry in recent years.

Many programs, of varying complexity, have been written to determine formation constants, and the type of program chosen depends upon several factors. For simple systems, AB or HA, non statistical programs are adequate, although, if the constants are overlapping a linear least squares technique is more applicable. For more general systems, i.e. those involving polynuclear, hydrolysed or protonated species, a more general non-linear least squares program must be used. The availability of a high speed digital computer with a large storage capacity is a criterion for the use of the latter type of program, as also, is the necessary time needed for familiarisation with the use of the program. As the present work included a search for protonated and hydrolysed species, a general program was required to calculate the stability constants. Two such programs, SCOGS 63 and LETAGROP VRID 64-68, have been described in the literature and both were available for use. LETAGROP was stored on the Atlas computer at Chilton and SCOGS on the St. Andrews IBM 360/44, hence, for geographical reasons, most of the present work used SCOGS.

Both programs depend up Taylor's series, a mathematical method of expressing a function in terms of its derivatives.

If
$$y = f(k_r; a_r)$$
 where $r = 1$ to M [1]

where y = a measured quantity

a = variable, but accurately known, quantities.

k = unknown constants.

Then Taylor's series gives an expression

$$U = U_0 + \sum_{1}^{M} \left(\frac{\partial U}{\partial R_+} \right) S R_+ + \sum_{3}^{m} \left(\frac{\partial \left(\sum_{k=1}^{M} \left(\frac{\partial U}{\partial R_+} \right) S R_k \right)}{\partial R_+} \right)$$
 [2]

where U is the error square sum

$$u = \sum_{i} \left(y - i \left(\sum_{j=1}^{M} f_{i_{1_{i_{1}}}} \frac{y}{y} \sum_{j=1}^{M} a_{f_{i_{2}}} \right) \right)^{2}$$

The "best" values are those which minimise this sum i.e. U. At this point the two programs begin to differ in rigour.

LETAGROP VRID

In this program equation [2] is the equation of a "pit" with v_0 the minimum point. The values of k_r are incremented to give not only the minimum point, v_0 , but also a map of the surroundings. The function v_0 is v_0 and so the quantity minimised is

$$U_{i} = \sum_{i} (\bar{z}_{calc} - \bar{z}_{expt})^{2}$$
 [3,L]

Equation [2] represents a generalised ellipsoid in 'M + 1) dimensional space. A measure of the spread of data around \mbox{U} is enclosed in the "D boundary" 64 .

$$U = U + \frac{U}{\rho}$$

$$[4]$$

When n is the number of experimental points and as generally n>>M

$$U \approx U_0 + \frac{U_0}{n}$$
 [5]

The D boundary is, again, a generalised ellipsoid but this time in M dimensional space with the "least squares" point (k_r") at its centre. The "standard deviation" can be calculated from the D boundary because it is identical with the range of values each k_r can assume on the boundary. The VRID block for was added to overcome the problem of a "skew pit", which arises from correlation of shifts and causes incorrect convergence. The shifts are altered by a "twist matrix" so that they are made along the axes of the skew pit rather than the co-ordinate axes.

SCOGS (appendix 2)

This is a more general program than LETAGROP VRID, when applied to stability constant work, because it can deal with up to twenty complexes of the type $A_pA'_p$, $B_qB'_q$, H_r . For the jth complex this leads to a stability constant

$$\beta_{j} = \frac{\begin{bmatrix} A_{p_{j}} & A'_{p'_{j}} & B'_{q_{j}} & B'_{q'_{j}} & H_{r_{j}} \end{bmatrix}}{\begin{bmatrix} A_{j} & B'_{q'_{j}} & A'_{j} & A'_{q'_{j}} & A'_{q'_{j}} & A'_{r_{j}} \end{bmatrix}}$$
[6]

or
$$C_j = \beta_j \cdot a^j \cdot a^j \cdot b^j \cdot b^j \cdot b^j \cdot h^j$$
 [7]

(NOTE: There is provision for the use of the activity coefficient of the hydrogen ion and hence SCOGS can give mixed constants.)

For N complexes

$$A = \sum_{1}^{N} (a + p_j \beta_j C_j)$$
 [8]

$$A' = \sum_{1}^{N} (a' + p'_{j}\beta_{j}C_{j})$$
 [9]

$$B = \sum_{i}^{N} (b + q_{j}\beta_{j}C_{j})$$
 [10]

$$B' = \sum_{1}^{N} (b' + q'_{j}\beta_{j}c_{j})$$
 [11]

If a, a', b and b' were known then A, A', B and B' would be the experimental values. But, as they are not known, let

$$f(a) = A_{expt} - A \quad (equal to zero for true values of a, a', b and b')$$

$$= A_{expt} - (a + \sum_{j=1}^{N} p_{j} \beta_{j} C_{j}) \quad [12]$$

similarly

$$f(a') = A'_{expt} - (a' + \sum_{j=1}^{N} p'_{j}\beta_{j}C_{j})$$
 [13]

$$f(b) = B_{expt} - (b + \sum_{j=1}^{N} q_{j} \beta_{j} C_{j})$$
 [14]

$$f(b') = B'_{expt} - (b' + \sum_{j=1}^{N} q'_{j}\beta_{j}C_{j})$$
 [15]

Values of a, a', b and b'(and hence C_j; equation [7]) are now obtained by a Newton-Rapheson iterative method. This minimises the functions [12]-[15] by calculating shifts that will simultaneously minimise all four functions. Progressing through each point, least squares equations are built up and solved, by matrix inversion, to yield shifts in constants. These shifts are obtained from Taylor's series but unlike the "pit mapping" procedure, only the first order terms are used. The quantity minimised is

$$U = \sum_{i} (Titre_{expt} - Titre_{calc})^{2}$$
 [3.8]

The calculated titre is obtained from the current set of constants and the experimental value of the hydrogen ion concentration.

The original SCOGS has been amended somewhat (Appendix 2), mainly in input and output. The input has been generalised to deal with any titrant, and the output contains several calculated functions, such as \bar{Z} . The size of the program has been increased to simultaneously refine up to thirty individual experiments of a total of five hundred readings.

SCOGS or LETAGROP

Although both the Gaussian and the "pit mapping" approaches have been in use for several years, no conclusions have been reached as to which method is "best". One criterion used to differentiate between them, is the range of the initial guess of each β required. Naturally Sillen favoured "pit mapping" and Perrin favours Gaussian 60, but Tobias 70, who could be assumed to be unbiased, as he has used both methods, favours the Gaussian approach. Further criteria are the rigour of the mathematics, the ability to refine difficult systems and the avoidance of the false minimums, but the ultimate criterion must be the reproduction of experimental parameters from the constants obtained, LETAGROP was devised as a "supplement to graphical methods" but since 1962 it has become a method in its own right; whereas SCOGS was conceived as a numerical method and, if it is used correctly, should be the faster method. It must not be forgotton, however, that LETAGROP has a wide applicability that extends far beyond potentiometry.

The two programs were compared with two sets of data of a different nature.

(a) Phenylalanine

This data was obtained from a study of the protonation of the ligand

The collection of the data is discussed in Chapter V. The data obtained was (-log h, titre) and for input into LETAGROP this was processed, by RWZASCOG (Appendix 2) to $(\overline{Z}, -\log h)$. The same ninety-five readings were used in the two programs to determine constants for the following equilibria

$$H + A \Longrightarrow HA \qquad K_{a_{1}} = \frac{[HA]}{[H][A]}$$

$$H + HA \Longrightarrow H_{2}A \qquad K_{a_{2}} = \frac{[H_{2}A]}{[H][HA]}$$

The results obtained are given in Table III.

Table III
Formation constants of Phenylalanine

	scogs	LETAGROP
pKa	9.610 ± 0.005	9,583 + 0.011
pK _a	2.754 ± 0.011	2,728 ± 0.016

As a further comparison, the values of \bar{Z} calculated from the SCOGS "constants" were run, with the experimental -log h values, on LETAGROP

and the following constants were obtained

$$pK_{a_1} = 9.587 \pm 0.011$$

$$pK_{a_2} = 2.684 \pm 0.016$$

The results obtained from LETAGROP, for both the experimental \overline{Z} and the values obtained from the SCOGS "constants", show no significant difference. It must be concluded, therefore, that the two programs give consistent results for this data with an error of $\frac{1}{2}$ 0.016,

(b) Acetic acid

The data used is a potentiometric study of the dimerisation of 71 . The following are the equilibria involved and the published results

[H] + [A]
$$\rightleftharpoons$$
 [HA] $B_{11} = 9.234 \times 10^6 \text{ M}^{-1}$
[H] + 2[A] \rightleftharpoons [HA]₂ $B_{12} = 1.111 \times 10^7 \text{ M}^{-2}$
2[H] + 2[A] \rightleftharpoons [H₂A₂] $B_{22} = 2.49 \times 10^{13} \text{ M}^{-3}$

These results were obtained by both graphical methods and by using LETAGROP⁷¹. When the same experimental data was used in SCOGS no convergence could be obtained despite using a variety of values for the input constants. Convergence was obtained when only two constants were used, but the standard deviation was so large that the results were meaningless.

This lack of convergence was examined more closely by using a simulated set of data obtained from HALTAFALL. This data was designed such that a metal-ligand interaction was examined, as in SCOGS' original

conception, and that two of the constants should lie close to one another.

(c) Simulated Data

The hypothetical system consisted of five equilibria including the phenylalanine equilibria shown in (a). The remaining equilibria and constants were

A + B
$$\rightleftharpoons$$
 AB log B₁ = 6.990
2A + B \rightleftharpoons A₂B log B₂ = 7.041
3A + B \rightleftharpoons A₃B log B₃ = 13.792

Nine experiments were simulated giving a total of ninety-nine readings to be refined together.

<u>Table IV</u>
Simulated data for the testing of SCOGS. Initial concentrations

Metal	concentration*	Ligand Concentration*
	20.0	30.0
	20.0	20.0
	20.0	10.0
	10.0	30.0
	10.0	20.0
	10.0	10.0
	5.0	30.0
20	5.0	20.0
	5.0	10.0

For all simulated titrations, the initial volume was 24.94 ml, the

^{*}concentration in mM.

titrant was sodium hydroxide (0.100 M) and each addition was of 2.00 ml stepwise up to a total of 20.00 ml.

Convergence was unobtainable using SCOGS demonstrating that the program is suspect when formation constants lie close together.

A FORTRAN version of LETAGROP⁷², LGVRID, became available towards the end of this work and, although the formation constants obtained were the same as from SCOGS, the program seems particularly sensitive to the parameter stegbyt⁷³ as this parameter controls the search for a minimum. The program must still be considered to be under development.

LETAGROP cannot be faulted in any way except in the complexity of its use and the understanding of its mechanics. This complexity is caused by its wide applicability to solution chemistry problems, and as such cannot be a valid criticism. SCOGS, however, can be faulted in its inability to refine constants which are close to each other, and when dealing with systems, such as the formation constants of D- and L-amino acid - metal complexes, then SCOGS should not be used.

HALTAFALL

This program has been used for predicting concentrations of species, from formation constants, previously in this laboratory 74 .

RWCALCOR (Appendix 1)

From an input consisting of the concentrations of the complexes under study, obtained from SCOGS or HALTAFALL, and the experimental heat

this program calculates the change in concentration of each species and heat corrections. Up to twenty complexes of the type $A_p B_q H_r$, where p, q and r are positive or zero, but r can also be negative, can be handled, but the core capacity of the I.B.M. 360/44, limits the number of points per experiment to twenty-five. The program can be used to determine heats of protonation, heats of hydrolysis and heats of formation of $A_p B_q H_r$ simultaneously but this is not regarded as the best use of the program. Experiments should be designed to obtain the heats of formation of $A_r H_r$ and $B_q H_r$ (where r is -ve) separately, whence, these values can be used to calculate corrections for experiments to obtain the heats of formation of the more complex, $A_p B_q H_r$, species. The output, pertinent to the calculation of heats of formation, is the corrected experimental heat, Q, associated with the formation of s complexes, and the change in concentrations, n_g , of these complexes. For the Nth point

$$Q_{N} = \sum_{1}^{S} (\Delta_{H_{S}}, \Delta_{n_{S}})_{N}$$

where Q_N is in joules

$$\triangle H_{S}$$
 is in J mol⁻¹

$$\Delta$$
n_s is in mol

For s complexes, s values of N are needed to solve for the heats of formation but, generally, more values than this are determined experimentally and then the following "least squares" method can be used.

Suppose the "best" heats are $\triangle_{\text{H'}_1}$, $\triangle_{\text{H'}_2}$... $\triangle_{\text{H'}_3}$

i.e.
$$\sum_{1}^{s} (\Delta_{H'_{s}}, \Delta_{n_{s}})_{N} - Q_{N} = 0$$

Then let
$$F = \sum_{1}^{M} (Q_N - \sum_{1}^{S} (\Delta_{H'_S} \Delta_{n_S})_N)^2$$

The "best" values of the heats are obtained by minimising the function

$$\frac{\Delta_{\mathrm{F}}}{\partial (\Delta_{\mathrm{H'}_{\mathrm{S}}})} = 0 = -\sum_{1}^{\mathrm{M}} (2\Delta_{\mathrm{n}_{\mathrm{S}}} \cdot (Q_{\mathrm{N}} - \sum_{1}^{\mathrm{S}} \Delta_{\mathrm{H'}_{\mathrm{S}}} \cdot \Delta_{\mathrm{n}_{\mathrm{S}}})).$$

There will be s functions of this type that can be solved as s simultaneous equations, to give values of $\triangle H'_S$ which are the "best" constants for the set of experimental results, 1 to M.

A program RWSOLV (appendix 3) was available to calculate "H_S's in this manner, it was also added on to the end of RWCALCOR to facilitate speedy calculation. The three versions of RWCALCOR that were used in this work were RWCALCR1, which does not contain RWSOLV, RWCALCR2, which calculates the heats of formation for each experiment individually and RWCALCR3, which gives heats of formation for all the experiments combined together.

RWZASCOG (Appendix 2)

This, too, was an established program but the input was altered to make it consistent with that of SCOGS.

Whilst considerable advantages can be ascribed to the use of a computer, there are numerous pitfalls. A degree of knowledge of computer languages is necessary to avoid simple, time consuming errors such as format errors. Access to the computer should be good, so as

to be able to take advantage of the peripheral facilities and so evade winecessary duplication of punching, program language and system knowledge. The use of "trial parameter" programs, such as SCOGS and LETAGROP, is a technique in its own right and has to be mastered. The usual criterion in this type of program is that, the set of constants giving the smallest standard deviation is the "best" set of constants to describe the experimental data. But, this criterion must not be imposed too rigourously as the possibility of obtaining a constant that describes a chemically non-sensical species or a constant that gives concentrations of species that have no physical significance are all too obvious. A knowledge of the program combined with a degree of chemical intuition and knowledge can give meaningful results, although the danger always exists of misinterpretation of data due to a bias either way. The editing of data is a problem for all experimenters and the recognition of poor results is as important as the interpretation of good results. Editing should be confined to pruning results from areas of low experimental accuracy.

To chemists the computer has become as important a tool as some spectroscopic techniques. The speed of calculation and the use of iterative procedures are useful and relevant to chemical calculations and whilst the computer is not indispensible it is certainly a great boon.

CHAPTER IV EXPERIMENTAL TECHNIQUES

Potentiometry and calorimetry were carried out in special vessels (Chapters V and VI respectively), and using solutions prepared and analysed by the following methods.

Water:-

All the water used for solutions was 'Elgastat' deionised, boiled and cooled by the passage of oxygen-free nitrogen. The resistivity of water was then better than 2 MAcm⁻¹.

Sodium Perchlorate:-

This had to be used in pure state, as an impurity of 1 part in 10^5 could give an error of 1%, when dealing with 1 mM metal ions. Solutions of sodium perchlorate were made by, either dissolving the monohydrate (Merck 'Puriss') in water, or by neutralising perchloric acid (Fisons A.R.) with sodium carbonate (Fisons A.R.). The solution (> 6.00 M) was then filtered through a sintered glass funnel (porosity 4), its pH adjusted to 9-10 and allowed to stand for a minimum of seven days. The precipitate of silica and heavy metal oxides and hydroxides was removed by filtration through a micropore (450 nm pore diameter) filter (Millipore Ltd.). Carbon dioxide was removed by making the solution acidic (~pH 2) and boiling then cooling under nitrogen. From this point two alternatives were possible i.e. either crystals of NaClO₄ were made or a standard solution was prepared and analysed.

(i) Crystals:- These were prepared from the above solution by adjusting its pH to 7 and heating in an evaporating basin to 140°C.

After cooling to 105°C, the slurry was filtered through a sintered glass funnel (porosity 3) and dried in an oven at 110°C. The pH of

- a 3.00 M solution was in the range 5.5 to 7.0.
- (ii) Standard solution:- After adjusting the pH to 7 the solution was analysed by cation exchange 75a and flame photometry 75b .

Perchloric acid: -

Concentrated perchloric acid (Fisons A.R.) was diluted to make a primary stock solution of ~1 M, which was further diluted to 0.1 M to be used as a working stock solution. Both solutions were analysed by titrating against sodium carbonate (Fisons A.R.) (methyl orange as indicator) 75c, and checked with standard sodium hydroxide solution 75d. Sodium hydroxide:-

1.00 M and 0.100 M solutions were obtained from ampoules (B.D.H. concentrated volumetric solutions) and their molarity was checked against standard acid solution 75d and standard potassium hydrogen phthalate (Fisons A.R.) 75e.

Metal Solutions:-

Metal perchlorates (G. Frederick Smith, Chemical Co.) were dissolved, allowed to stand for several days, filtered through micropore filters (450 nm) and analysed by two independent methods.

Copper (II): Electrodeposition 75f and EDTA 75g (Fast sulphon black F.)

Nickel (II): Electrodeposition 75h and EDTA 75i (murexide)

Cobalt (II): Electrodeposition 75j and EDTA 75k (xylenol orange)

Iron (III): Jones reductor ⁷⁵¹ and sulphurous acid ^{75m}

followed by titration with standard potassium

dichromate (Fisons A.R.) ⁷⁵ⁿ (sodium diphenylamine as indicator).

Commercial Iron (II) perchlorate was analysed for purity and was found to contain up to 4% iron (III), hence, iron (II) perchlorate was prepared by dissolving iron sponge (Johnson Matthey Chemicals 'Specpure') in standard perchloric acid ⁷⁶. The solution was analysed by oxidation with potassium dichromate ⁷⁵ⁿ and the results obtained by this method agreed with those obtained from the weight of iron dissolved. Solutions prepared in this manner were stable for up to a week but when made 3.00 M in (Na)ClO₄, significant oxidation had occured in 24 hours.

The concentration of hydrogen ions in the metal solutions was obtained by means of Gran plots 77 .

EDTA:-

Solutions were made up from ampoules (B.D.H. concentrated volumetric solutions) and their molarities checked against magnesium chloride (Fisons A.R.)

Phenylalanine:-

DL-β-phenylalanine was obtained commercially (B.D.H. Biochemical grade), dried, and subjected to analysis C, 65.25; H, 6.92; N, 8.47 (Calculated C, 65.45; H, 6.67; N, 8.57%) mp. 284°C. It was, thus, used without further purification.

Nitrogen: -

Oxygen-free nitrogen (British Oxygen) was further de-oxygenated by passage through chromous chloride and then "scrubbed" in 3.00 M sodium perchlorate, both of which were thermostated at 25°C.

Solutions were analysed prior to the ionic background being made 3.00 M due to difficulties of analysis in this medium. All solutions were stored under nitrogen and sealed with "Parafilm" (Gallenkamp).

Apparatus:-

Volumetric apparatus ('E-mil (Green line)' M.J. Elliott) was provided with calibration certificates. Several calibrations were checked but all were found to agree with the certificates. The apparatus was calibrated at 20°C hence all solutions were stored at this temperature before use.

All apparatus was cleaned regularly with 'Quadralene' (Quadralene Chemical Products) and alcoholic potassium hydroxide. Before use, apparatus was washed with demineralised water, 'Elgastat' water, alcohol and anaesthetic ether and then dried by suction.

CHAPTER V

POTENTIOMETRY

The determinations were carried out at 25.0°C and with an ionic background of 3.00 M in (sodium) perchlorate. The hydrogen ion concentration was followed by using a cell of the type

A sodium chloride salt bridge was employed because potassium ions form insoluble potassium perchlorate in the porous plug of the calomel electrode. The electrode pair (Activion; glass, 17SB; calomel, RCB) and a Beckman research pH meter were used, to give readings reproducible to 0.1 mV. A toughened glass electrode (Activion 27SB) was tested but the linear response to -log h was limited to the range 2-9, which was too narrow for the present study.

The reaction cell, figure 8, contained ligand, acid, metal perchlorate and sufficient sodium perchlorate to produce an ionic background of 3.00 M (Na) ClO₄. Polynuclear formation and hydrolysis were investigated by varying -log h, titrimetrically, for different concentrations and ligand to cation ratios.

The electrode pair was calibrated by a titrimetric procedure, whence the ionisation constant of water, $\mathbf{K}_{\mathbf{w}}$ could be checked.

The emf of the above cell is given by

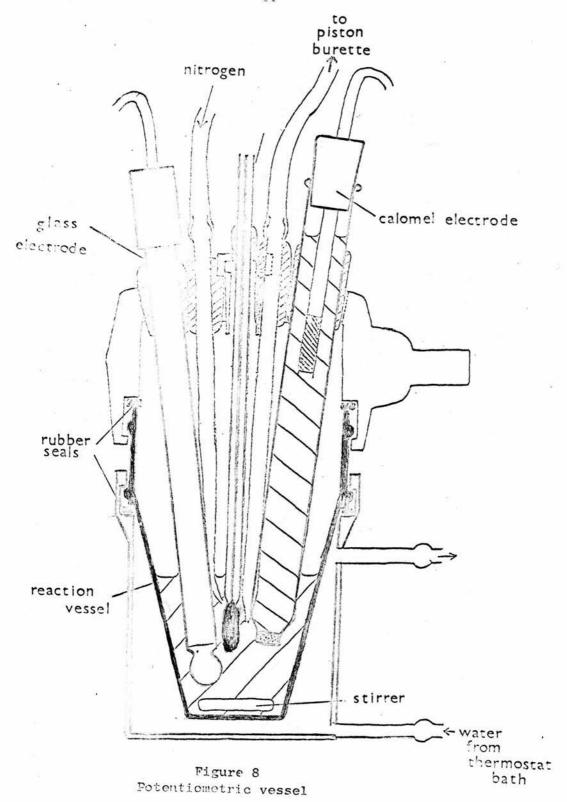
$$E = E^{o} + \frac{RT}{zF} \ln h + E_{j}$$

i.e $E = E^{o} + 59.162 \log h + E_{j}$ at $25^{o}C$ (1)⁴¹

Where E is the emf

E is a constant

and E is the liquid junction potential.



If E_j is constant then a plot of E vs -log h ought to give a straight line of slope -59.162 mV(-log h)⁻¹. Values of -log h > 7 were calculated using a value of -log K_w = 14.22^{78} .

Table V. Electrode calibration

24.98 ml perchloric acid $(7.245 \times 10^{-3} \text{ M})$ titrated with sodium hydroxide (0.5000 M) using an 'Agla' syringe.

ml added	mV	-log h
0.000	309.9	2,140
0.270	268.1	2.740
0.325	233.2	3.137
0.340	200.1	3,363
0.350	69.9	3,628
0.355	-101.5	3,863
0.360	-148.4	4,417
0.370	-183.6	10.411
0.390	-209.3	10.939
0.460	-239,3	11.495
0.500	-246.9	11.647
Standard solutions	of h	
	364.5	1,142
	329.4	1.744
	240.4	3.251

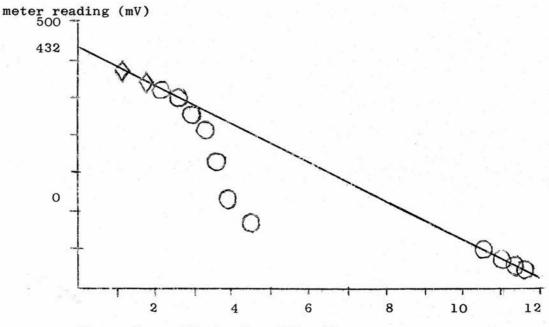


Figure 9. Electrode calibration curve.

As can be seen from figure 9 this plot is linear in the range $-\log h = 1.2$ to 3.0 and again from 10.0 to 11.6. The deviation from linearity in the region 3.0 to 10 is due to unbuffered solutions, and has been observed previously by Williams and Williams⁷⁹; a linear response was obtained in buffered solutions. E_j was assumed constant in the range $-\log h = 1.2$ to 11.6 due to the linearity of the plot in this region.

Formation constants of phenylalanine

As the accuracy of the subsequent metal-ligand complex formation study was to depend upon the accuracy of the pK's of the ligand the following procedure was adopted.

- (1) All titrations were performed at constant ligand
 concentration (i.e. A = constant)
 - (2) Each protonation was studied independently.
- (3) Only values of $\frac{1}{2}$ 0.25 either side of \overline{Z} = 0.5 or 1.5 were used for calculation of pK's 80 .

The formation curve (Figure 10) was constructed using a method, similar to that for $\bar{\mathbf{Z}}$ (Chapter III), as in the computer program in appendix 3. The formation curve can be seen to be independent of the ligand concentration and polynuclear species were therefore assumed absent.

The data was then analysed using SCOGS (appendix 2) and the results obtained were

$$pK_{a_1} = 9.6097 \pm 0.0018$$

 $pK_{a_2} = 2.7544 \pm 0.011$

s (in titre) = 0.196 (95 readings)

The effect of experimental error on the pK_a 's was investigated and the results summarized in Table VII.

Table VI

Experimental results for the protonation of phenylalanine

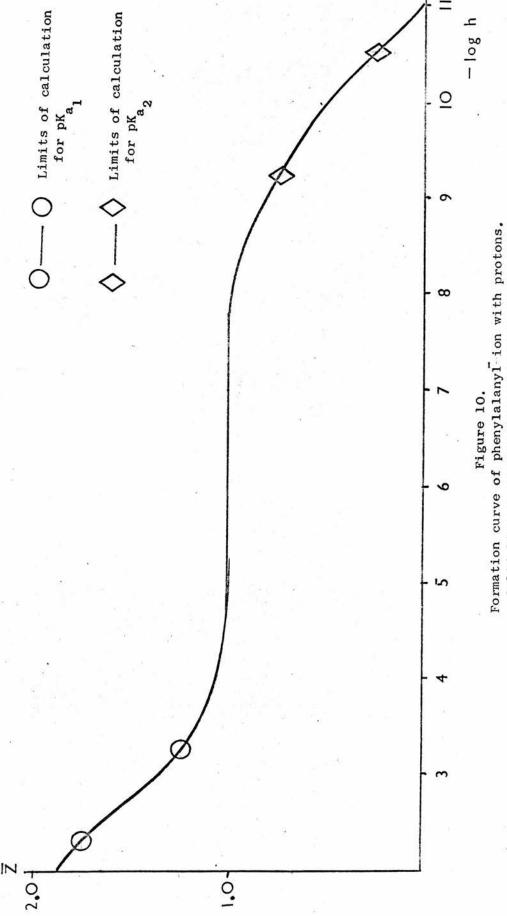
(a)

Titration		Titrate (S) Titrant (T) Volume molarity ml						E ^O mV
	A	н	A	н				
1	0.0500	-0.0100	0.0500	0.0500	14.98	433.7		
2	0.0500	0.0500	0.0500	0.0195	14.98	433.7		
3	0.0500	0.0500	0.0500	0.0195	15.00	444.6		
4	0.02498	0.02498	0.02498	0.01448	15.00	433.7		
5	0.02498	0.02498	0.02498	-0.00998	15.00	433.7		
6	0.00999	0.00999	0.00999	-0.01179	15.00	433.		
7	0.00999	-0.01179	0.00999	0.01149	15.00	444.		
8	0.00999	0.00999	0.00999	-0.01149	15.00	444.6		
9	0.00499	0.00499	0.00499	0.01047	15.00	433.		
10	0.00499	0.00499	0.00499	-0.01089	15.00	433.		

Table VI

(b)

	1		2	2	3		4	
W. 420km	titre (ml)	e,m,f, (mV)	titre (ml)	e.m.f.	titre (ml)	e.m.f.	titre (ml)	e.m.f. (mV)
	8.00	-168.4	1.50	243.6	1,50	254.1	1.00	248.9
	9.00	-163.2	2.00	253.0	2.00	263.4	1.50	263.0
	10.00	-159.4	3.00	267.3	3.00	277.5	2.00	273.7
	C. C. Landerson and C.	-155.9	4.00	278.6	4.00	288.6	3.00	290.6
	11.00	-150.0	5.00	288.7	5.00	298.2	4.00	303.5
	13.00 15.00	-145.4	6.00	296.6	6.00	306.9	5.00	313.6
	17.00	-141,3	7.00	304.3	7.00	314.6	7.00	327.1
	20.00	-136.2	8.00	310.9	8,00	321.3	1.00	001.11
	23.00	-130.2	0,00	310.3	9.00	327.2		
					3.00	321.2		
	26.00	-128.4						
	5		(6	7			
	titre	e.m.f.	titre	e.m.f.	titre	e,m,f,		
	(ml)	(mV)	(ml)	(mV)	(ml)	(mV)		
	1.00	-76.3	.75	-79.6	2.00	-125.7	1	
	1,50	-87.7	1.00	-87.5	2.20	-114.6		
	2.00	-95.1	1.50	-98.7	2.40	-103.0		
	3.00	-106.0	2.00	-107.1	2.60	-90.2	100	
	4.00	-114.0	3,00	-119.7	2.80	-73.0		
	5.00	-120.2	4.00	-129.5	3.60	244.0		
	6.00	-125,5	6.00	-145.5	3.80	258.2		
	8.00	-134.2	8.00	-159.9	4.00	267.9		
	10,00	-141.5		55.0 E	4.50	285.5		
	12,50	-149.3			5.00	298.1		
	15.00	-156.4			6.00	315.2		
	20.00	-170.2			7.00	326.4		
			Ta .		8,50	337.3		
					10.00	344.3		
	8	4	9)	1	.0		
	titre	e.m.f.	titre	e.m.f.	titre	e.m.f.		
	(m1)	(mV)	(m1)	(mV)	(ml)	(mV)		
	.40	250.5	.30	244.3	.50	-82,1		
	.50	257.8	.40	254.1	.75	-92.9		
	.70	269.6	.50	261.6	1.00	-100.8		
	.90	278.4	.75	275.7	1.50	-113. ọ		
	1.20	289.0	1.00	285.7	2.00	-122.3		
	1.50	297.5	1.60	301.7	3.00	-137.6		
	1.80	304.5	2.00	308.8	4.00	-150.9		
	1.00		100,000,000			104 0	1	
	2.30	313,8	3.00	320.9	5.00	-164.2	1	
		313.8 323.6	3.00 4.00	320.9 328.6	5.00	-164.2		



Solid line is the total experimental curve.

Table VII

The significance of various experimental errors.

variable	variation	pK _a obtained for + ve variation	change
Temperature	± 0.25°C	9.618	0.108
Eo	<u>+</u> 1 mV	9.627	0.016
Ligand concentration	± 1%	9.620	0.01
Initial volume	± 1%	9.607	0.003
Base concentration	± 1%	9,600	0.01
Each A analysed	0.05 M	9,611	0.001
independently	0.025 M	9,606	0.004
	0.010 M	9.580	0.03
	0.005 M	9.607	0.003

All the variations are within the range of the SCOGS-LETAGROP variation and are thus acceptable. Although the low value of pK_{a} , obtained from the 10 mM results, could be attributed to a systematic error, the computer output does not give substance to this theory. It can be seen that E^{O} is the most sensitive variable and, as such, care must be exercised in its determination.

Formation constants for copper (II) - phenylalanine complexes.

The hydrogen ion concentration in the vessel was varied by titrating with sodium hydroxide solution (0.100 M) whence precipitation heralded the end of the titration. A formation curve was constructed from the results in Table VIII.

 $\underline{ \mbox{Table VIII} }$ Experimental results for the Cu(II)-phenylalanine system.

(a)

Titration	Initia	Initial concentrations (M)				
	Metal	ligand	acid			
1	0.01896	0.04009	2 x 10 ⁻⁴	24.93		
2	0.00948	0.04010	1 x 10 ⁻⁴	24.92		
3	0,00473	0.04009	5 x 10 ⁻⁵	24.93		
4	0.01898	0.02004	2 x 10 ⁻⁴	24.91		
5	0.0955	0.02004	1 x 10 ⁻⁴	24.91		
6	0.0473	0.02004	5 x 10 ⁻⁵	24.91		
7	0.01894	0.00994	2 x 10 ⁻⁴	24.90		
8	0.00955	0.00994	1 x 10 ⁻⁴	24.91		
9	0.00474	0.00994	5 x 10 ⁻⁵	24.90		
10	0.01898	0.00497	2 x 10 ⁻⁴	24.90		
11	0.00955	0.00497	1 x 10 ⁻⁴	24,90		
12	0.00474	0.00497	5 x 10 ⁻⁵	24.90		

 $E^{O} = 444.6$ mV for all titrations

Table VIII

(b)

	1		2		4		5
titre	e.m.f.	titre	e.m.f.	titre	e.m.f.	titre	
(m1)	(mV)	(m1)	(mV)	(ml)	(mV)	(m1)	
0.0	266.4	0.0	245.6	0.0	000 F	0.0	053 0
0.50				0.0	266.5	0.0	251.6
		0.50	240.5	0.50	261.2	0.50	244.4
1.00		1.00	235.2	1.00	255.4	1.00	236.2
	255.6	1.50	229.1	1.50	249.0	1.50	226.9
	251.7	2.00	222.2	2.00	241.9	2,00	215.8
	251.7	2.50	214.3	2.50	234.0	2.50	203.8
	242.8	3.00	204.6	3.00	224.7	3.00	186,8
	238.0	3.50	192.6	3.50	213,5	3.50	166.6
	232.7	4.00	175.4	4.00	199.0	4.00	138.1
	227.0	4.50	141.8	4.50	177.4	4.50	86.8
	220.5		8	5,00	118,3		- At
	213.6				41.00	-	the many contract
	205.3	C	3		6		7
	196.7		e.m.f.		e.m.f.		e.m.f.
	186.4	(ml)	(mV)	(ml)	(mV)	(ml)	(mV)
	174.3		001 0				namana na
	159.2	0.0	231.8	0.0	238.5	0.0	265.4
	139.7	0.50	224.0	0.50	227,2	0.50	256.0
	110.2	1.00	213,7	1.00	212.8	1.00	244.9
9.50	18.8	1.50	199.5	1.55	190.7	1.50	230.7
		2.00	174.3	2.00	159.8	2.00	208.9
						2.50	137.6
						3.00	91.4
	8)	1	<u></u>	-	
titre	4		e.m.f.	1 titro	e.m.f.	1 1	
(m1)		(ml)	(mV)	(ml)	(mV)	(ml)	e,m.f.
					11.0	(
0.0	250.3	0.0	237.8	0.0	257.3	0.0	248.2
0.50	238.2	0.50	220.6	0.50	239.7	0.50	225.7
1.00	223,4	1.00	197.6	1.00	208.0	1.00	185.6
1.50	204.2	1.50	165.6				esusta en 2000 b
	175.1	2.00	112.4			100	
2.00							
2.00	78.4			1			
2,50							
2.50	2						
2,50	2 e.m.f.		Control of the Contro				
2.50 l titre (ml) 0.0	2 e.m.f.		.,				
2.50 	2 e.m.f. (mV)						

Total number of readings = 91

Figure 11 shows that the curves are not coincident as \bar{z} approaches 2.0. The experimental data was processed in SCOGS and an extensive survey of possible species was made with particular reference to hydrolysed species, which have been previously reported 1. For $(Phe^{-})_p Cu_q (II)_{r}$ species with the values pqr, 110, 210, 310, 111, 211, 212, 11-1, 11-2, and 22-2 were searched for; the species <math>101, 102 and 02-2 were assumed present and their formation constants kept constant 1.

The results were best described by three constants

$$\log \beta_{110} = 8.247 \pm 0.022$$

$$\log \beta_{210} = 15,549 \pm 0.022$$

$$\log \beta_{22-2} = 4.6 \pm 0.4$$

These constants gave a standard deviation in titre of 0.2174. For just β_{110} and β_{210} the same constants were obtained but the standard deviation was 0.2178. Additional data that had been obtained near precipitation, but had been rejected, was also processed and was best described by

$$\log \beta_{110} = 8.247 \pm 0.0211$$

 $\log \beta_{210} = 15.549 \pm 0.0211$
 $\log \beta_{22-2} = 3.55 \pm 0.2$
 $\sin (108 \text{ readings}) = 0.207$

The system can thus be described by the two complexes ${\rm Cu}^{\rm II}({\rm phe}^-)$ and ${\rm Cu}^{\rm II}({\rm phe}^-)_2$

$$\log \beta_{110} = 8.247$$

$$\log \beta_{210} = 15.549$$

but evidence is shown for the hydrolysis of Cu^{II}(phe⁻)₂ at high -log h giving a species Cu^{II}₂(OH)₂(phe⁻)₂ with a formation constant log $\beta_{22-2} \approx 4.0$.

Formation constants for nickel (II)-phenylalanine complexes.

Hydrogen ion concentration was varied by titration with sodium hydroxide (0.04999 M) using the same electrode pair ($E^{O} = 446.7 \text{ mV}$) for all the titrations. A formation curve (Figure 11) was constructed from the results given in table IX.

Table IX

Results for the nickel-phenylalanine system

(a)

Titration	Initial concer ligand	ntrations (M) metal	Initial volume (ml)
1	0.00994	0.00951	19,96
2	0.00995	0.00475	19,94
3	0.01170	0.00224	16.96
4	0.00497	0.00952	19.96
5	0.00497	0.00475	19,96
6	0.00450	0.00173	21.98
7	0.00234	0.01120	16.96
8	0.00234	0.00559	16.96
9	0.00209	0.00200	19.00

Table IX

(b)

3		2	4		
the second secon		Non-transfer out to the contract of the contract of		e.m.f.	titre
(mV)	(ml)	(mV)	(m1)	(mV)	(m1)
133,2	0.0	147.7	0.0	163.1	0.0
117.9	0.10	134.8	0.10	136.9	0.25
C. C			The second secon		0.40
				119.9	0.55
88,1		111.2	0.40	113,1	0.70
82.4		1775	0.50	101.3	1.00
		92.4	0.75	92.7	1,25
		81.5		84.7	1.50
				76.5	1.75
				68.9	2.00
			117		
7		3	(,	5
e.m.f.	titre	e.m.f.	titre	e.m.f.	titre
1 - 1 - 4 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6		(mV)	(ml)		(ml)
	5 7		25000 0000		1080 (20028)
137.3	0.0	106.6	0.0	132,2	0.0
115.7				117.5	0.10
102.0	0.20	80.5	0.20	107.3	0.20
89.6	0.30	70.5	0.30	99.5	0.30
75.2	0.40	61.6	0.40	92.5	0.40
63.6	0.50	54.1	0.50	85.8	0.50
47.5	0.60	48.1	0.60	80.1	0.60
	3			74.3	0.70
	-				0.80
i i		1			0.90
				60.2	1.00
(mV)	(m1)	(mV)	(m1)	1000	
97.2	0.0	120.8	0.0		
76.3	0.10	99.5	0.10		
60.1	0.20	86.4	0.20	1	
47.7	0.30	72.9	0.30	j	
32.5	0.40	58.7	0.40	Ì	
19.5	0.50	46.3	0.50		
2237 1227	- 0-	31.7	0.60		
3.7 -14.9	0.60	31.7	0.00		
	e.m.f. (mV) 133.2 117.9 106.5 96.9 88.1 82.4 7 e.m.f. (mV) 137.3 115.7 102.0 89.6 75.2 63.6 47.5 e.m.f. (mV)	0.0 133.2 117.9 0.20 106.5 0.30 96.9 0.40 88.1 0.50 82.4	e.m.f. (mV) (m1) (mV) 147.7	titre e.m.f. (ml) (mV) (ml) (mV) 0.0 147.7 0.0 133.2 0.10 117.9 0.20 125.6 0.20 106.5 0.30 117.9 0.30 96.9 0.40 111.2 0.40 88.1 0.50 105.2 0.50 82.4 0.75 92.4 1.00 81.5 70.20 80.5 0.20 102.0 0.30 70.5 0.30 89.6 0.40 61.6 0.40 75.2 0.50 54.1 0.50 63.6 0.60 48.1 0.60 47.5 8 0.20 80.4 0.60 47.5 8 0.20 80.4 0.60 47.5 0.20 80.4 0.60 47.5 0.60 47.5 0.20 80.4 0.60 47.5 0.60 47.5 0.20 80.4 0.60 47.5 0.60 47.5 0.20 80.4 0.60 47.5 0.60 47.5 0.20 80.4 0.60 47.5 0.60 47.5 0.20 80.4 0.60 47.5 0.60 47.5 0.20 80.4 0.60 47.5 0.60 47.5 0.20 80.4 0.20 60.1 0.30 72.9 0.30 47.7 0.40 58.7 0.40 32.5	e.m.f. (mV) (m1) (mV) (m1) (mV) (m1) (mV) 163.1

It can be seen from figure 11 that the formation curves are coincident, hence the system is described by simple stepwise species. The data was analysed using SCOGS and the following results were obtained

$$\log \beta_{110} = 5.353 \pm 0.026$$

 $\log \beta_{210} = 10.487 \pm 0.050$

s (84 readings) in titre = 0.063.

Evidence for a tris complex was not found as the 2:1 species was insoluble in the ionic medium used. The solid was filtered, washed with water, alcohol, and ether, air dried and subject to analysis. Ni^{II}(C₉H₁₀O₂N)₂.2H₂O C, 51.29; H, 5.99; N, 6.57 (calculated C, 51.09; H, 5.72; N, 6.62%). Similar compounds have been reported in the literature ⁸³. An attempt to remove the complexed water by heating in a vacuum oven to 150°C but a small percentage (~10%) of the water remained; NiA₂, C, 55.33; H, 5.41; N, 6.98 (calculated C, 55.85; H, 5.21; N, 7.24%). Infra-red spectra of the two complexes were run but conclusions could not be drawn from them.

Formation constants of the cobalt (II)-phenylalanine system.

Hydrogen ion concentration was varied by titration with sodium hydroxide (0.04999 M) using the same electrode pair (E^{O} = 446.7 mV) for all the titrations. A formation curve was constructed from the results given in table X.

 $\frac{\texttt{Table} \quad X}{\texttt{Results} \ \texttt{for the cobalt (II)-phenylalanine system}}$

(a)

Titrat	ion	Ini	tial cond ligand	centration meta		Init: volum (ml)	ne
1 2 3 4 5 6 7			0.00662 0.00993 0.00995 0.00397 0.00497 0.00663 0.00234	0.007 0.005 0.005 0.005 0.005 0.005	563 281 901 563 375	14.9 19.9 19.9 24.9 19.9 14.9	6 4 6 4
			(b)			
]			2		3		4
titre (ml)	e.m.f. (mV)	titre (ml)	e.m.f. (mV)	titre (ml)	e.m.f. (mV)	titre (ml)	e.m.f.
0.0 0.0 0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00 1.10	112.0 109.0 85.4 71.4 59.4 50.3 42.6 35.6 29.1 22.9 16.3 11.4 5.6 0.3	0.0 0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00 1.10 1.20 1.30	110.1 87.1 6.0 66.8 59.3 53.0 47.5 42.3 37.8 33.6 29.5 25.7 22.2 19.0	0.00 0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90	1.5 71.7 58.1 48.3 40.3 33.3 26.0 21.3 16.5	0.00 0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00 1.10 1.20 1.30	8.2 84.7 72.0 62.0 44.3 47.3 40.8 35.0 29.9 24.7 19.7 15.9 10.0 5.1
	5	-0000 - 001 - F-20	6		7	 	
titre (ml	e e.m.f. (mV)	titre (ml)	e.m.f. (mV)	titre (ml)	e.m.f. (mV)		######################################
0.0 0.10 0.20 0.30 0.40 0.50 0.60	94.6 73.2 59.9 49.9 41.3 33.3 27.5	0.0 0.10 0.20 0.30 0.40 0.50 0.60 0.70	86.9 60.3 46.7 35.9 27.5 18.3 13.0 6.0	0.0 0.10 0.20 0.30 0.40 0.50	85.7 53.8 37.0 23.9 12.7 1.3		
0.80 0.90 1.00 1.10	2014		Tota	1 number	of readin	ngs = 78	

It can be seen from figure 11 that the formation curves are coincident, hence the system is described by simple stepwise species. The data was analysed using SCOGS and the following results were obtained

$$\log \beta_{110} = 4.449 \pm 0.014$$

 $\log \beta_{210} = 8.439 \pm 0.037$

s (78 readings) in titre = 0.041

No evidence of a tris complex was obtained due to the formation terminating at \bar{z} = 0.8.

Formation constants of the iron (II)-phenylalanine system

hydroxide (0.04997 M) using the same electrode pair (E^O = 446.7 mV) for all the titrations. Particular care was exercised to exclude oxygen from the system as oxidation readily occured. On completion of each titration the solution in the vessel was tested for oxidation by the addition of potassium thiocyanate; half of the titrations were rejected because of oxidation. A formation curve was constructed from the results given in table XI.

Table XI
Results for the iron (II)-phenylalanine system

Titration	Initial conc ligand	entrations (M) metal	Initial volume (ml)
1	0.01013	0.01111	19.94
2	0.01065	0.00469	18.96
3	0.00675		29.92

Table XI

(b)

1		2		3	
titre e.m.f. (ml) (mV)	titre (ml)	e.m.f. (mV)	titre (ml)	e.m.f.	
20.20 72.6	8.20	52.4	20.10	71.6	
20.30 50.2	8,30	30.1	20.20	47.5	
20,40 36,6	8,40	17.6	20.30	33.0	
20.50 26.9	8.50	8,3	20.40	23.4	
20.60 19.2	8.60	1.2	20.50	15.2	
20.70 13.1	8.70	-4.5	20.60	9.3	
20.80 8.3	8.80	-9.3			
20.90 4.4	8.90	-13.6			
21.00 0.7	9.00	-17.2			
21.10 -2.5	9.10	-20.3			
	9.20	-23,3			

The results were analysed using SCOGS and the system was best described by three constants

$$\log \beta_{110} = 3.763 \pm 0.016$$

$$\log \beta_{210} = 6.882 \pm 0.244$$

$$\log \beta_{310} = 10.627 \pm 0.232$$

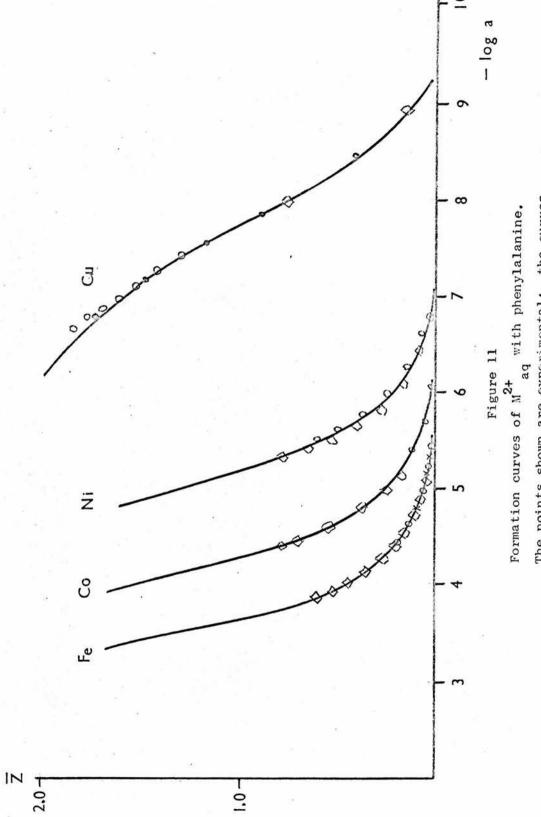
s (29 readings) in titre = 0.018

for only two constants the following was obtained

$$\log \beta_{110} = 3.736 \pm 0.009$$

$$\log \beta_{210} = 7.192 \pm 0.025$$

s (29 readings) in titre = 0.019



The points shown are experimental; the curves

are theoretical,

As \bar{z} did not exceed 0.6 the contribution made by β_{310} must be small and, hence, accounts for the large errors in $\log \beta_{210}$ and $\log \beta_{310}$. The values obtained by the convergence of two constants will be the "best" constants and the value obtained for $\log \beta_3$ a guide to the value of this constant i.e.

$$\log \beta_{110} = 3.736 \pm 0.009$$

 $\log \beta_{210} = 7.192 \pm 0.025$
 $\log \beta_{310} = 10.7 \pm 0.2$

s (29 readings) in titre = 0.02.

It will be difficult to obtain log β_{310} more accurately in this medium as oxidation occurs so readily at pH 7.

Formation constants of the iron (III)-phenylalanine system

Due to the formation of an insoluble precipitate during titrations with alkali⁹⁸ this investigation was carried out by titrating iron (III)-phe solutions with perchloric acid (0.0538 M) using the same electrode pair (E° = 446.7 mV).

Table XII

Results for the iron (III)-phenylalanine system

(a)

Titration	Initial	ations (M)	Initial volume	
TITTALION	ligand	metal	acid	(ml)
1	0.01483	0.00628	3 x 10 ⁻⁴	25.00
2	0.02060	0.00262	1×10^{-4}	23.98
3	0.01235	0.00786	3×10^{-4}	19.98
	i l			

Table XII

(b)

1			2		3
titre	e.m.f.	titre	e.m.f.	titre	e.m.f.
(ml)	(mV)	(ml)	(mV)	(ml)	(mV)
0.0	284,2	0.0	245.6	0.0	293.9
0,50	286.7	0.25	248.7	0.50	297.1
1.00	288.8	0.50	251.7	1.00	299.8
1.50	291.0	0.75	254.5	2.00	302.6
2.00	293.0	1.00	257.5	2.50	307.6
2.50	295.1	1.25	260.0	3.00	310.0
3.00	297.0	1.50	262.3	3.50	312,1
3.50	298.9	1.75	264.4	4.00	314.4
4.00	300.7	2,00	266.6		
4.50	302.6	2.50	270.5		
5.00	304.4	3.00	274.1		
5,50	306.1	3,50	277.4		
6.00	307.7	4.00	280.6		
7.00	310.9	4.50	283.6		
8.00	313.7	5.00	286.4		
-		5.50	289.2		
		6.00	292.0		
		6.51	294.6		
		7.00	297.0		
		7.50	299.4		
	1	8.00	301.6		

The aqueous iron (III) system is complicated by hydrolysis but this has been investigated by Hedström 98 for the 3.00 M (Na)ClO $_4$ medium and the constants he obtained have been used in the calculations for this system.

$$\log \beta_{O11} = -3.045$$
 $\log \beta_{O12} = -6.310$
 $\log \beta_{O22} = +2.914$

SCOGS was used to find the "best" constants that describe the experimental data. For the simple 1:1 and 2:1 species the following

was obtained

$$\log \beta_{110} = 10.412 + 0.04$$

 $\log \beta_{210} = 19.225 + 0.066$

s = 0.341 (44 readings)

Hydrolysis of these two species was also investigated and a constant for the following system was found

$$\log \beta_{110} = 10.388 \pm 0.04$$

 $\log \beta_{210} = 19.113 \pm 0.13$
 $\log \beta_{22-2} = 16.92 \pm 0.34$
 $s = 0.338 (44 \text{ readings})$

A search for the 3:1 complex was also made

$$\log \beta_{110} = 10.390 \pm 0.04$$

 $\log \beta_{210} = 19.087 \pm 0.18$
 $\log \beta_{310} = 26.13 \pm 1.77$
 $\log \beta_{22-2} = 16.95 \pm 0.37$
 $s = 0.342 (44 \text{ readings})$

The difference in the standard deviation is small for the three descriptions of the system, hence, the "best" constants can be a combination.

 $\log \beta_{110} = 10.39 + 0.04$

 $\log \beta_{210} = 19.11 + 0.10$

 $\log \beta_{310} \approx 26.0$

 $\log \beta_{22^{\circ}2} = 16.9 + 0.30$

s = 0.34 (44 readings).

The high errors in $\log \beta_{310}$ and $\log \beta_{22}$ can be attributed to the small degree of formation of the complexes in the present study. At the highest -log h value the degree of formation of the above complexes was 23%, 60%, 3% and 12% of the metal respectively.

Comparison with other workers results

The formation constants obtained in 3,00 (Na)ClO $_4$ are higher than those obtained at lower ionic strengths 99 and this has been found for all the systems studied when compared with published results (Tables XIII and XIV). Figure 12 shows the log β_2 s for Cu(II)-phe, obtained by other workers, plotted against $\sqrt{\Gamma}$. A smooth curve can be drawn, with a minimum at $\sqrt{\Gamma} \approx 0.7$, through most of the points, showing that this system is similar to those discussed in Chapter III, and that the present work is in good agreement with much of the previously published work. The comparisons for Ni(II)-phe and Co(II)-phe are similar to that for Cu(II)-phe but not as extensive. Previous work on the two main oxidation states of iron is scanty and the constants obtained are not well characterised.

Table XIII

Protonation of phenylalanine

pKa1	pK _{a2}	temp ^O C	method*	I	Reference
9,610	2.754	25	gl	3.00	This work
9,31	2.20	25	gl gl	->0	84
9,13	1.83	25	emf	0.06?	85
9,35	2.41	25	g1	0.37	96
9,18	2,21	20	g1	1,00	97
9,08	2.09	25	g1	0.05	9 8
9.02	-	25	g1	0.16	89

* gl = glass electrode

emf = electromotive force method

Table XIV

Metal phenylalanine complexes

a comparison of results

Metal	t°C	Method	I	10g β1	$\log \beta_2$	Ref.
Cu(II)	25	gl	3.00	8,247	15,549*	This work
FL (15)	25	gl	0.05	7,92	13.76	88
	25	gl	\rightarrow 0	8.18	15,18	88
	25	gl	0.16	7.51	14.25	89
	25	gl	→ 0	8.25	15,38	84
	20	gl	0.37	8.23	15.14	86
	25		1.00		14,92	92
	25	gl	0.01	7.38	14.24	93
	25	c	→ 0	7.87	14.77	90
10	25	c	0.027	7.44	14.64	90
	25	р	0.06		14.22	85
	20	gl	0.01	5. e - 1	14.90	91
Ni(II)	25	gl	3,00	5.353	10.487	This work
	25	gl	0.05	5,11	9,43	88
T ₁	25	gl) 0	5.46	9,99	88
	25	gl	→ 0	5.56	10.22	94
	20	gl	0.37	5,19	9,66	86
	25	gl	0.01	4.73	10.02	93

Table XIV continued

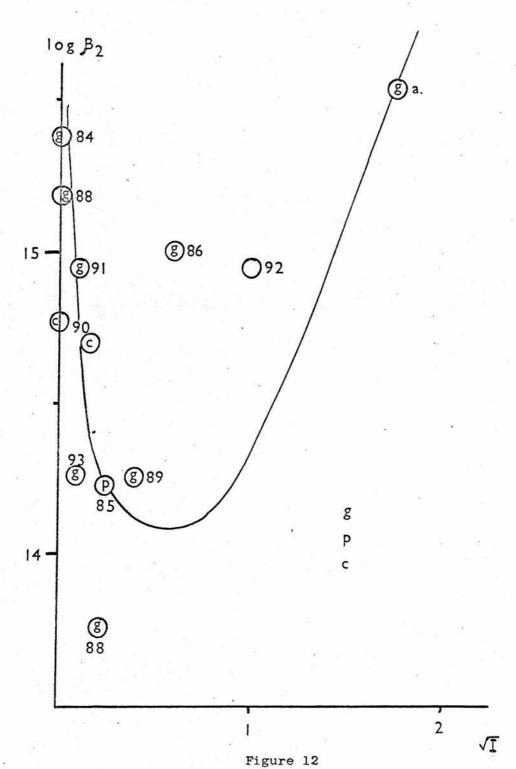
Co(II)	25	gl	3.00	4.449	8,439	This work
	25	gl	0.05	4.03	7.47	88
	25	g1	0.01	4.00	8.08	93
	20	g1	0.01		7.9	91
Fe(II)	25	g1	3.00	3.736	7.192*	This work
	20	gl	1.00	3.26		97
	20	g1	0.01	P-27 x3	6.3	91
Fe(III)	25	gl	3,00	10.39	19,11*	This work
	20	emf	1.00	8.9		87

gl - glass electrode

c - conductivity

p - polarography

* - system described by more than two constants



Published results for β_2 for Copper (II)-phenylalanine system

g = glass electrode

c = conductivity

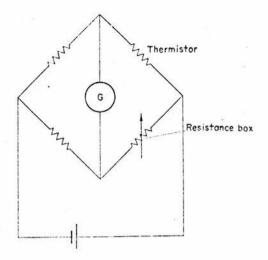
p = polarography

CHAPTER VI

CALORIMETRY

The calorimeter was of the Gerding, Leden and Sunner ⁹⁵ design, as shown in figure 13, and is similar to another calorimeter used in this laboratory ⁹⁶. The unit comprises of an inner reaction vessel of glass and an outer shielding vessel partially of glass and partially of copper. The two vessels are attached to the "lid" of the calorimeter; the reaction vessel by two springs and the outer vessel by an O-ring seal (O) to prevent leakage. The chimneys provide the means of introducing probes into the reaction vessel: (a) a burette tip, (b) a stirrer which also acts as a cooler, (c) a heat detector, (d) a heater, and (e) an electrode pair.

- (a) The burette, (B). The titrant was added through a glass burette tip protected from back diffusion by a polytetrafluoroethylene (PTFE) cap held on a gold spring. The titrant was prewarmed, to the temperature of the bath in a spiral of nylon tube (P) (Portex SFD Nylon C, 8 ml capacity) on top of the vessel, by immersion in the water of the bath. The free end of the nylon tube was then attached to a piston burette (Metrohm AG, E 274, 10 ml.).
- (b) The stirrer, (S). Vibro-stirring was used because it appears to have smaller heat of stirring corrections 96, but primarily it was used to minimise the effects of inefficient stirring and pressure upon the heat detecting system. The stirrer disc was a flat circular plate 1 mm thick PTFE (2.5 cm diameter) containing 10 holes of 1 mm diameter. This was screwed onto a hollow stainless steel tube held in nylon impregnated with molybdenum disulphide to reduce friction. The tube was connected directly to the vibro-motor (Chemap AP, El) using an L-shaped bar. Heat conduction from the



The Wheatstone bridge circuit for measuring thermistor resistance. G is a galvanometer.

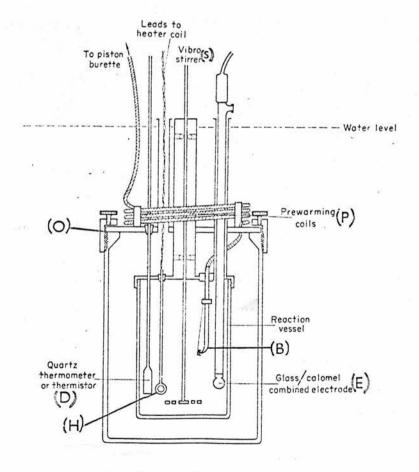


Figure 13.
The isothermal calorimeter.

motor to the calorimeter via the bar was prevented by wrapping the bar in asbestos tape at the connection to the motor. The stirrer tube was hollow to allow cooled nitrogen to be passed into it from a long hollow needle.

- (c) The heat detector, (D). The temperature change was measured by using a thermistor (Stantel F23), a conventional DC-Wheatstone bridge, a preamplifier (Pye, 11330) and a Scalamp galvanometer (Pye, 420). For a temperature rise of less than 0.1° C the temperature can be assumed to be inversely proportional to the resistance 95 (-60 Ω deg $^{-1}$ at 25°C).
- energy, a calibration experiment is required. This was done electrically by means of a heater coil of non-inductively wound resistance wire (20.83.\Omega) coated with a chemically resistant epoxy resin (Araldite). The voltage across the heater was measured on a digital voltmeter (Solartron LM 1420.2). The current flowing was passed through the heater resistor and also through a 10.000\Omega standard resistance; the voltage across this resistance was measured to give the current in the heater circuit. The time for which the heating current flowed was automatically recorded to within 0.02 s using a stopwatch (Jaquet 309 e).
- (e) Electrode pair, (E). Although there is provision for the use of a combination electrode (Activion TlN7DB/180) in the calorimeter it was not used in this work as more accurate results can be obtained by direct potentiometry.

The complete system was suspended in a thermostat bath controlled to $25.0000 \pm 0.0005^{\circ}$ C (LKB 7602 controller on 7603A bath) which was located in a thermostatted room (22° C \pm 0.5°C).

Experimental procedure.

For each titration the vessel was charged by either, directly pipetting the solutions into the reaction vessel or, making up the titrate in a siliconed (Beckman Desicote) flask and pouring the contents (99.57 ml) into the reaction vessel. The calorimeter was assembled and immersed in the water bath. After a minimum of eight hours, the stirring and electronic system were switched on and after two hours reached steady state conditions whence the titration could proceed.

For each point the following procedure was adopted.

- (1) 8 minute 'fore' period.
- (2) 6 minute reaction period in which 0.5 2 ml of titrant were added (or electrical energy for a calibration point).
- (3) 8 minute 'aft' period.
- (4) Nitrogen cooling and a 10 minute pause.
 This is shown in figure 14.

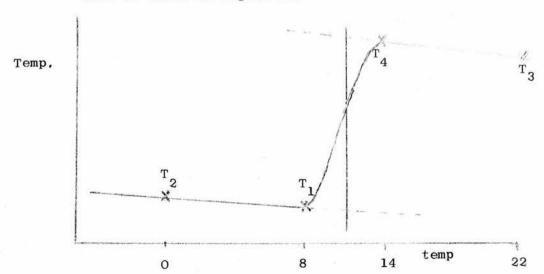


Figure 14. Temperature-Time plot for the reaction period of the calorimeter.

The heat corrections are calculated as follows

$$\triangle T = \frac{3(T_2^{-T_1})}{8} + \frac{3(T_4^{-T_3})}{8} + (T_4^{-T_1})$$

The values of 6, 8 and 10 minutes were arrived at by plots of resistance versus time and the above values were the times required to attain steady state. Each point would, thus, take 32 minutes making it possible to complete about 15 points per day.

Calibrations: These were performed during the course of titrations, and a body of data built up to construct a calibration curve. The electrical energy supplied to the system is calculated from

$$J = VIt$$

J in joules

I in amperes

t in seconds

The calibration constant is calculated

$$= \frac{J}{\triangle R}$$
 i.e. $J \Omega^{-1}$

and plotted against the total volume of solution in the reaction vessel.

The heat of ionisation of water, AH.

This was determined to assess the accuracy and reproducibility of the calorimeter. The conditions used in the calorimeter for these experiments were similar to those used in subsequent heat of formation determinations i.e. alkali was titrated into acid. The results obtained were for the formation of 2×10^{-4} moles of water and were as follows

(i)
$$-55.913 \text{ kJ mol}^{-1} \quad (-13.364 \text{ kcal mol}^{-1})$$

(ii)
$$-55.774 \text{ kJ mol}^{-1}$$
 (-13.330 kcal mol⁻¹)

(iii)
$$-55.879 \text{ kJ mol}^{-1}$$
 (-13.355 kcal mol⁻¹)
average $-55.522 \pm 0.024 \text{ kJ mol}^{-1}$ (-13.350 $\pm 0.008 \text{ kcal mol}^{-1}$)

This value agrees well with the literature values where the "best" calorimetric value is given as "close to -13.34 kcal mol-1,97

The heats of protonation of phenylalanine.

The following results were obtained by the titration of phenylalanine solutions with sodium hydroxide (0.100 M). Seven "runs" totalling 49 readings were completed.

Initial ligand,	0.02510	0.02510	0.02510	0.02521	0.02514	0.04820
Initial mineral acid,	0.01464	0.01464	0.000	0.000	0,000	0.000
Initial volume, ml	99.57	99,57	99,57	99.57	99.57	51,73
ml added		Heat	evolved	(Joules)		
2.0	9.788	9,282	0.368	1.125	1,384	
4.0	19,558	19,043	0.913	2.039	1,900	0.828
6.0	28,971	28,428	2,298	3,058	2.603	2,211
8.0	37,333	38,663	3,302	4,518	4,153	3,761
10.0	47,309	45,922	4,342	5,853	5.104	5.443
12.0	55,261		5.00	7.041	6.184	6.535
14.0			6.162	7.948	6.994	7,725
16.0			7,397	9,185	8.015	9,475
18.0			8,148	9,379	9,324	10,947
20.0				9.869	10.376	11,938

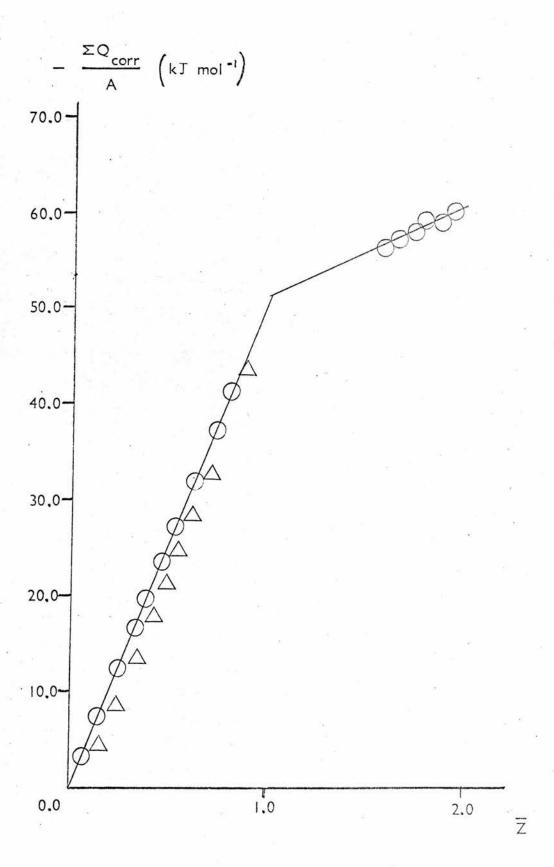


Fig. 15 Enthalpic Curve for Phe / H system.

An enthalpic curve was plotted (figure 15) but the values for the heats of protonation were obtained using the "least squares" method described in Chapter III (page 35). The results obtained were

$$\triangle H_1 = -50.405 \pm 0.13 \text{ kJ mol}^{-1}$$
 $\triangle H_2 = -60.14 \pm 0.5 \text{ kJ mol}^{-1}$

The heats of formation of Cu(II)-phe complexes

The results were obtained by the titration of Cu(II)-phe solutions with sodium hydroxide (0.100 M) solution. Six "runs" totalling 47 readings were completed.

nitial phe (M)	0.0397	0.0397	0.0201	0.0003	1	
nitial min,acid		AN IN STREET, SALES AND	3,0201	0.0201	0.0201	0.0200
/ /	0.000	0.000	0.000	0.000	0.000	0.0001
nitial volume (ml)	99.90	99.90	99,57	99.57	99,57	100.04
ml added		Н	eat evolv	ed (Joul	es)	411
2.0	8,389	8,389	6.784	6.402	5.693	
4.0	9.656	8.768	6.176	6.469	5.918	16,641
6.0	8.914	8.348	7.036	6.717	6.281	8,274
8.0	9.408	9.940	7.456	6.927	6,839	8.409
10.0	8.967	8.998	8.197	7.630	7.063	7.694
12.0	8.372	9.178	7.034	7.603	6.143	
14.0	9,141	8,834	6.355	7.087	7.492	15,246
16.0	8.701	8,728	6.371	7.076	3.783	10,473
18.0		7.802	5,192	5,861	72. 42. 5	9,417
20.0		10.222	5.635	4.947		
22.0		8.815				
24.0		6.139				

An enthalpic curve was plotted (figure 16) but the values of $\triangle_{\rm H_1}$ and $\triangle_{\rm H_2}$ were obtained by using the method described in chapter III. The results were: $\triangle_{\rm H_1} = -19.179 \pm 1.8 \; {\rm kJ} \; {\rm mol}^{-1}$ $\triangle_{\rm H_2} = -58.352 \pm 4.0 \; {\rm kJ} \; {\rm mol}^{-1}$

s (47 readings) = 1.17

Even though evidence for a hydrolysed species was found in the potentiometry, no account of it was taken during the above calculations due to the conditions employed in the experiments i.e. -log h was too low for $\operatorname{Cu}_2^{\mathrm{II}}(\operatorname{OH})_2(\operatorname{phe}^-)_2$ to be formed.

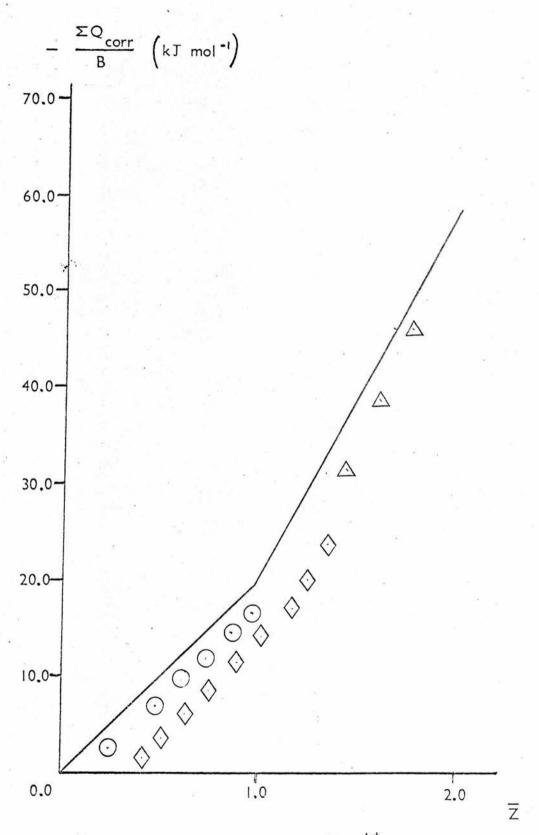


Fig. 16 - Enthalpic Curve for Phe /Cutt system.

The heats of formation of Ni(II)-phe complexes

The results were obtained by the titration of copper(II)-phenylalanine solutions with sodium hydroxide solutions. Five "runs" totalling thirty readings were completed.

Table XVII

Results for the heats of formation of Ni(II)-phe complexes.

Initial nic	kel(II)(mM	1)	a 1.90	3	9.514	5. 28 6	18.99	9.495
Initial phe	eny la l a nine	(mM)	2.02	4	10.120	8.996	29.82	9,900
Sodium hydr (Titrant)			49.97		49.97	49.97	100.00	100.00
Initial vol	ume (ml)		100.00)	100.00	90.00	99,90	99.90
ml adde	ed a		5		Не	eat evolved	しています。 (Toules)	1-
0.5	0.401							
1.0	1.425	1.5	87	1.	478		2.611	
1.5	1.679							
2.0	2.328	2.3	53	2.	182	4.726	3,835	
2,5	2.807							
3.0	2.995	2,5	78	3,	138		5,600	
4.0		3.3	32	4.0	029	8,185	7.557	
5.0		4.2	85	4.3	333			
6.0		5,8	25				9.847	
7.0		7.5	26					
8.0		9.0	60			18,251	11,880	19
10.0						23.721		i q

An enthalpic curve was plotted (figure 17) but the values of ΔH_1^0 and ΔH_2^0 quoted below were obtained using the method described in Chapter III.

These results were

$$\triangle H_1^0 = -9.815 \pm 0.6 \text{ kJ mol}^{-1}$$

$$\triangle H_2^0 = -24.537 \pm 1.2 \text{ kJ mol}^{-1}$$

$$s(30 \text{ readings}) = 0.6$$

Under the conditions of the experiment sufficient of the A_2^B complex was formed to be able to calculate a value of $\triangle H_2^0$ but nevertheless it was insufficient to be able to draw a complete enthalpic curve and line AB is an extrapolation. Measurements near the precipitation point were unreliable due to various heats of solution etc.

The heats of formation of Co(II)-phe complexes

The results were obtained by the titration of cobalt(II)-phenylalanine solutions with sodium hydroxide solutions (0.1 M). Four "runs" totaling 28 readings were completed.

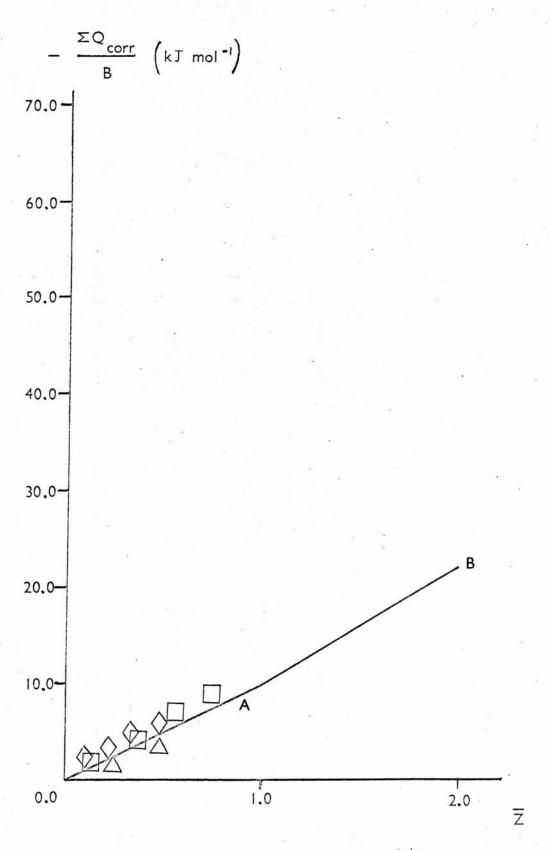


Fig. 17 Enthalpic Curve for Phe / Ni ++ system.

 $\frac{{\tt Table~XVIII}}{{\tt Results~for~the~heat~of~formation~of~Co(II)~complexes}}$

	1	2	3	4	
Initial cobalt(II) (mM)	7.880	7.880	2,253	2,253	
Initial phenylalanine (mM)	6,556	6,556	10.92	10.92	
Initial volume 'ml)	100.00	100.00	102.00	102.00	
ml added	h	eat evolved	(Joules)		
0.5			0.497	0.497	
1.0	0.691	0.691	0.300	0.273	
1.5			0.300	0.304	
2.0	0.512	0.534	0.298	0.292	
2.5			0.290	0.298	
3.0	0.522	0.504		G-111111111111111111111111111111111111	
3.5			0.581	0.578	
4.0	0.518	0.519	0.293	0.288	
4.5			0.297	0.301	
5.0	0.517	0.517			
6.0	0.549	0.540			

An enthalpic curve was plotted (figure 18) and the values of $\triangle {\rm H_1^o}$ and $\triangle {\rm H_2^o}$ were calculated by the method described in chapter III.

The results were

$$\triangle H_1^0 = -5.297 \pm 0.8 \text{ kJ mol}^{-1}$$

$$\triangle H_2^0 = -13.361 \pm 1.6 \text{ kJ mol}^{-1}$$
s (28 readings) = 0.8

The enthalpic curve shown is partly extrapolated for reasons identical to those mentioned for nickel in the previous section.

The heats of formation of Fe(II)-phe complexes

Values of $\triangle H^O$ were not obtained because of the oxidative instability of the system. The calorimeter described in Chapter VI was not designed to incorporate an inert atmosphere and so it was impossible to maintain anoxic conditions for sixteen hours in the present apparatus. However, I consider the study of iron(II)-amino acid systems to be sufficiently important to warrant a closer scrutiny of the experimental difficulties with a view to either adapting the present apparatus or to constructing a new calorimeter for determining the heats of formation of such complexes.

The heats of formation of Fe'III)-phe complexes

Although a reasonable amount of data was collected for this system, it was not possible to express it in terms of ΔH^0 values. Due to hydrolysis and subsequent precipitation in this system when titrated with alkali, the method used for all the previous systems had to be adapted. Solutions of iron(III) perchlorate and phenylalanyl were titrated with perchloric acid. This gave a pH range of 2.2 to 2.8 and unfortunately the concentration changes over this range are small. Thus, heat changes are correspondingly small and difficult to measure. Thermistor resistance is the experimental quantity that was actually measured and for the ferric system such measurements were only about twice the minimum measurable quantity and furthermore, except for the first few points, the reaction was endothermic and this renders the heat corrections excessive. Thus it was impossible to determine heats of formation of the iron(III)-phenylanine system.

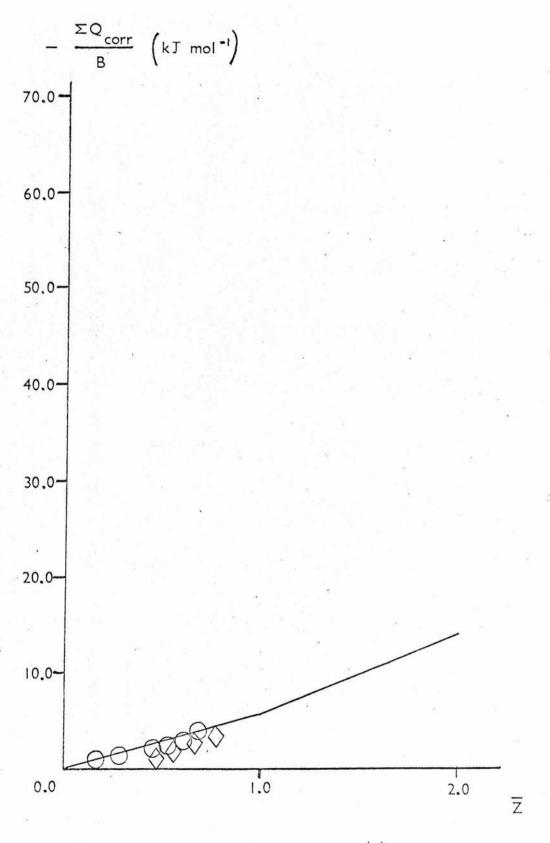


Fig. 18. Enthalpic Curve for Phe / Co + system.

Comparison with other workers' results

No direct comparisons may be made because of different background media, different methods of calculation and different types of calorimeter but, primarily, because the accuracy of some published work leaves something to be desired. Some comparative results are shown in table XIX. The ligand protonations and copper(II) systems have been well studied, but research into the cobalt(II) and nickel'II) systems is less extensive.

 $\begin{tabular}{ll} \hline \textbf{Table XIX} \\ \hline \textbf{Heats of formation of phenylalanyl complexes} \\ \hline \end{tabular}$

Metal	°c	Method	△H ₁ °	ÅH2	Ref.
н+	25	Cal	-50.405	-60.140	This work
	25	Cal	-44.601	_	84
	25	Temp.	-42,921	*	84
	25	Cal	-	-	88
	25	Cal	-43,138	-	89
Cu ⁺⁺		Cal	-19.18	-58,35	This work
		Cal	-19.7	-48.5	88
		Cal	-21.41	-45.55	89
		Cal	-22.16	-48.93	84
Ni ⁺⁺		Cal	-9.815	-24.537	This work
		Cal	-11.3	-19.3	88
		Cal	-13.38	-27,10	84
Co ²⁺		Cal	-5,297	-13.361	This work
		Cal	-6,28	-7.53	88

The accuracy of the results listed are naturally dependent upon the precision with which various experimental parameters can be measured. The error in analytical techniques was estimated as being $\langle 0.3\%$ but, by far the largest, and hence the governing, error was the observed temperature change. This was measured by recording the change in thermistor resistance $(\pm 0.01 \Omega)$. This gave maximum error of 8% in the derived enthalpies. Errors as high as this probably only occured for the cobalt system and were much smaller for the other systems because these evolved more heat.

CHAPTER VII

DISCUSSION

The results can be most efficiently discussed in three sections.

(a) the protonation of the phenylalanyl anion, (b) chelation trends occurring across the transition series, and (c) the individual complexing reactions of each metal ion.

(a) The Protonation of the Phenylalanyl anion.

Several workers have reported PKs for the phenylalanyl anion referring to a variety of temperatures and ionic strengths.

Activity coefficients can be calculated from a relationship suggested by \mathtt{Davis}^{40}

$$-f_{\pm} = \underbrace{A z_{+} z_{-}}_{1 + \sqrt{I}} - bI$$

where $\mathbf{z}_{\underline{+}}$ are the charges on the cation and anion and A and b are constants. For aqueous systems,

$$A = 1.825 \times 10^{6} (\xi T)^{-3/2}$$
$$= 0.509 \text{ at } 25^{\circ} C$$

(& is the dielectric constant of water).

Constant b encompasses corrections for the ionic strength variation of the dielectric constant of the medium and the effective sizes of the hydrated ions.

The activity coefficient can then be used to calculate the concentration pks over a range of ionic strengths and these values can then be compared with those obtained experimentally. This is illustrated in figure 19, where the value of b giving the "best" fit was chosen as 0.398.

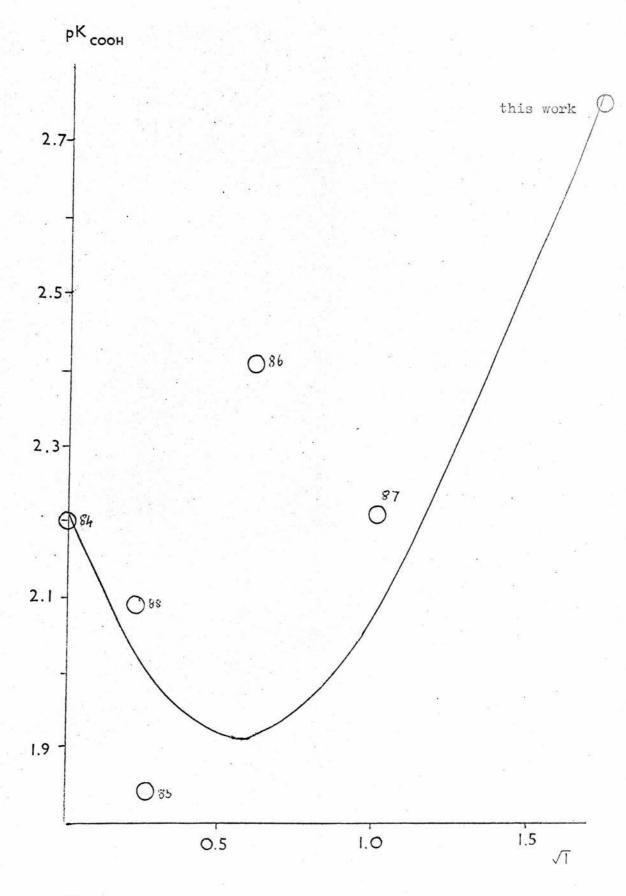


Fig. 19. Variation of pK with ionic strength.

Simon and Weber have noted their result as being high but have offered no explanation. The other five results, which included the present work, all lie near the curve and thus indicat that the results are consistent.

Table \overline{XX} Thermodynamic parameters for the protonation of the phenylalanyl anion in 3.00 M (Na)ClO4 at 25°C

	∠G ^O (kJ mol ⁻¹)	△H ^O (kJ mol ⁻¹)	△S ^O (J mol ⁻¹ K ⁻¹
-NH ₂	-54.87	-50.41	14.99
-coo	-15,73	-9.73	20.02
Overall values	-70.60	-60.14	35,01

The AHO-COO- value is somewhat higher than those reported for other amino acid carboxyl groups in this media. For example, consider:

I (histidyl) II (tryptophyl) III (phenylalanyl)

 ΔH_{-COO}^{0} -1.25 -9.64 (kJ mol⁻¹)

The governing factor appears to be the electron withdrawing power of the group attached to the β -carbon of the amino acid since no possibility exists for conjugation to occur over two saturated carbon atoms. An electron withdrawing group will have the effect of stabilising the negative charge on the carboxyl group and thus rendering the enthalpy of protonation less negative. The electron withdrawing power of the aromatic ring can be enhanced by more electron withdrawing groups or atoms, such as substituted nitro groups or a heterocyclic ring as in II. There are other factors which are also important, for example, the availability of the lone pairs on the nitrogen atoms. Hence a quantitative treatment must necessarily be very complex. The ratio of ΔH_{II}^{O} : ΔH_{III}^{O} : ΔH_{III}^{O} is 1:3:9 but considering the complexity of electron withdrawal this cannot really be simplified to claim that each additional nitrogen has an equivalent effect, i.e. the numerical ratio 1:3:9 is considered to be coincidental.

For $\triangle H_{-NH_2}^0$, I = -40.5; II = -38.4; III = -50.4 (kJ mol⁻¹) but no comparison can be made because of the added complication arising from protonating the imidazole ring of histidyl.

The entropy terms for phenylalanyl's two protonations are less positive than those for the other two amino-acids under discussion.

	Δs _{-NH2}	Δs ^o -coo-	√kJ mol ⁻¹
Histidyl	48.5	40.2	
Tryptophyl	61,1	41.4	
Phenylalanyl	15.0	20.4	

These values arise mainly from the decrease in the hydration sheaths

 κ^{-1}

upon protonation. The two related molecules, I and II have similar entropy changes whereas III is less polar and so has a smaller value.

(b) The Chelation of the Metal Ions

The increasing importance of the +II oxidation state as one crosses the first transition series is an important aspect of transition metal chemistry. This increased stability to the eventual exclusion of all other oxidation states at zinc arises because the 3d orbitals change from being diffuse excited orbitals into tightly-bound core orbitals. The +II state becomes most important from manganese onwards and, except for copper(1) and iron(III), the aqueous chemistry of these transition metals is wholly that of the +II state. Iron'(III) has great importance not only because of its aqueous chemistry but also because of its biological role and thus it merits special attention. This +III oxidation state for iron occurs against a trend of decreasing occurrence of oxidation states higher than +II because of the comparatively low third ionisation potential for iron which in turn arises from the metal's electronic configuration. A similar reason explains the stability of copper(I). These points will be dealt with more fully in a subsequent section.

The +II oxidation state occurs for the metals manganese through to zinc by ionisation of the two 4s electrons to produce an outer electronic configuration of $3d^n$ (n is 5 for Mn and 10 for Zn). All the ions form complexes and are hydrated in aqueous solution. Small ligands usually produce octahedral complexes and so the aquated ions are written $[B(H_2O)_6]^{2+}$. Copper deviates from this stereochemistry and gives Jahn-Teller distorted octahedral coordination, which in extreme cases becomes square planar. 102

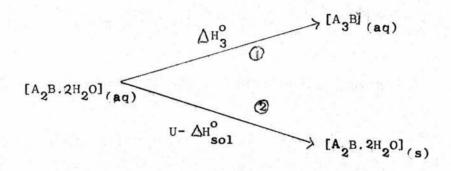
Complexes have been reported having up to three amino acids anions bound per divalent central metal ion 99 but in this study, this situation arose only for iron(II). Copper, as might be expected, formed ${\rm Cu}^{\rm II}{\rm phe}_2$ (where phe is the phenylalanyl anion) but not ${\rm Cu}^{\rm II}{\rm phe}_3$; Nickel and cobalt, however, could be expected to form ${\rm A_3B}$ complexes quite readily, but we found no evidence for these complexes because precipitation occurred at $\bar{\rm Z}=0.8$. This was due to the formation of an insoluble, aquated, 2:1 complex ${\rm A_2B.2H_2O}$. The nickel complex was identified by analysis and similar complexes have been studied by infra-red spectroscopy 83 . In fact both nickel- and cobalt-phenylalanine complexes had been reported previously and their insolubility had been commented upon 88 .

Table XXI

Thermodynamic parameters for metal-phenylalanyl complexes in 3.00 M (Na)ClO₄ at 25°C.

		△G° (kJ mol ⁻¹)	∆H ^o (kJ mol ⁻¹)	Δs ^o (π mol ⁻¹ κ ⁻¹)
Cu ²⁺	β ₁	-47.09	-19,18	93.60
	K ₂	-41.69	-39.17	8.48
	β2	-88.78	-58.35	1 02, 1 ,
Ni 2+	β	-30.57	-9,82	69.59
	K ₂	-29.26	-14.72	48.76
	β2	-59,83	-24.54	118.4
Co ²⁺	β_1	-25,40	-5.30	67.45
	K ₂	-22,78	-8,06	49,81
	β2	-48,19	-13.36	116, 85
[™] e ²⁺	β	-21,33		
	K ₂	-19.73		
	β2	-41.07		
Fe ³⁺		-59.33		
	β ₁ β ₂ β ₂ β ₂ β ₃ β ₄ β ₅ β ₄ β ₅ β ₄ β ₅	-49.79		
	β2	109.12		

The formation of the solid $A_2B.2H_2O$ in preference to the soluble complex A_3B is due to the high lattice energy of $A_2B.2H_2O$.



where ΔH_3^o is the heat of formation of A_3^B U is the lattice energy of $A_2^B.2H_2^O(s)$ ΔH_{sol}^o is the heat of solution of $A_2^B.2H_2^O(s)$

However, the reaction path followed is dependent upon the Gibbs free energy of each reaction and so the entropy terms ought also to be examined in addition to these enthalpy terms.

Complexes have a greater freedom of movement in solution compared to the solid state and so the entropy of precipitation ought to be negative.

The neutrality of the complex will minimise the hydration sheath which for most charged ions is large enough to make the entropy term positive and enhance precipitation.

The entropy term for forming A_3B is a small positive quantity and so even though the signs of the entropy changes are opposite this will produce only a small numerically difference compared to the large enthalpic differences.

 $\Delta_{(sol)}^{O}$ is small compared to the lattice energy and so the latter is the more important term in dictating the choice between paths (1) and (2).

$$U = -\frac{NA^{2}z^{2}}{r} \left(1 - \frac{1}{n}\right)^{103}$$

U is lattice energy (ergs)

N is Avogadro's number (6.024×10^{23})

A is Madelung constant

e is electronic charge $(4.802 \times 10^{-10} \text{ e.s.u.})$

r is ionic radius (cm.)

n is a constant for the system.

Thus, the lattice energy is dependent upon the two parameters r and n, (n has been experimentally determined from compressibility measurements and has values in the range $5-12^{103}$). Upon inspection, the B-O distance in $B'H_2O_6^{2+}$ when B = Fe²⁺ is different from when B = Ni²⁺ and Co²⁺.

Bond distances in B(H₂0)₆ 2+ "octahedra."100

	$H_2O - B(nm)$			B-O (nm) (oxide)
В	1 *	2 *	3 *	
Fe ²⁺	0.217	0.214	0.210	0.217
Co ²⁺	0.211	0.209	0.208	0.212
Ni 2+	0.209	0.208	0.204	0.208

Hence this difference in ionic radii quite probably explains $^{\text{Te}}$ ²⁺ following reaction scheme ① and Co²⁺ and Ni²⁺ following scheme ② since the lattice energies for the latter ions become larger more negative) then $\triangle \text{H}_2^{\text{O}}$ s.

For ions in the series from Mn²⁺ though to Zn²⁺, the general stability sequence for the replacement of water by more polarizable ligands is given

by the Irving-Williams series:

$$Mn^{2+} < Fe^{2+} < Co^{2+} < Ni^{2+} < Cu^{2+} > Zn^{2+}$$
.

This reflects the changes in heats of complex formation along the series 100 and as can be seen from table XXI, the results obtained in this study obey the Irving-Williams order.

Assuming that ionisation potential sums are a measure of the tendency of a metal ion to draw electrons to itself by the formation of covalent bonds, then some correlation between these sums and the stability of the complexes of the metal ions would be expected. Figure 20 shows this correlation for the four divalent metal ions studied complexing with phenylalanine.

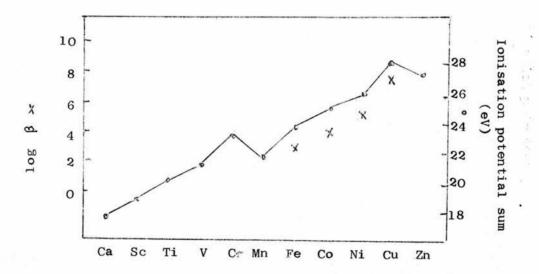


Figure 20

Log B₁ for phenylalanyl complexes compared to the ionisation energies of the meţal atoms giving the divalent cations.

From Table XXI it can be seen (i) that the enthalpy contribution to the Gibbs free energy makes this correlation an enthalpy effect and 'ii) that for all the metals studied $-\Delta H_1^0 < -\Delta H_{1,2}^0$, an effect that has been previously reported by Izath et al al and ascribed to the large difference in hydrational energies between B^{2+} and AB^{+} and AB^{+} and AB^{0} , however, is consistently larger than AS_2^0 and this is mainly due to statistical factors. Thus, the overall effect is $-\Delta G_1^0 > -\Delta G_{1,2}^0$ a fact uniformly true for all literature values of metal-amino acid interactions with just one exception (Sychev and Migal's 93 , phenylalanine work; their experimental approach has been questioned by Gergely et al 88).

The trends in ΔS^{0} show an interesting inversion in that ΔS^{0}_{1} decreases from Cu^{2+} to Ni^{2+} to Co^{2+} whereas $\Delta S^{0}_{1,2}$ increases along this series. This inversion can be ascribed to the number of water molecules released in the two reactions

$$B_{(aq)}^{2+} + A_{(aq)} \rightarrow BA_{(aq)}^{+}$$
and $BA_{(aq)}^{+} + A_{(aq)}^{-} \rightarrow BA_{2(aq)}^{+}$

Cu $^{2+}$ has the smallest ionic radius 1O2 and hence will have the largest hydrated radius (cf. the lanthanides 1O2) and similarly Ni $^{2+}$ \langle Co $^{2+}$. For BA $_2$, however, the size order will be reversed and so the overall entropy values will take the order Cu $^{2+}$ \rangle Ni $^{2+}$ \rangle Co $^{2+}$ (see table XXI). The trend in \triangle S $_{1,2}^{0}$ suggests that the number of water molecules released in the second reaction is Cu $^{2+}$ \langle Ni $^{2+}$ \langle Co $^{2+}$ and indicates that the size of the hydrated complex BA has the same order.

Metal-amino acid systems in solution have been studied by several schools 84,89,91,104,96 and the more recent publications have included

various protonated and hydrolysed species. Whilst the major complexes formed are the simple $^{A}_{P}$ B species, protonated, hydrolysed and polynuclear species have been found to exist 106,107 for ligands related to amino acids and for a few amino acids themselves. Perrin 105 obtained constants for the protonated species ABH and $^{A}_{2}$ BH involving a series of divalent metal ions and aliphatic amino acids. These complexes were said to be analogous to acetate complexes and hence the amine group was protonated and the metal-ligand bond utilises the carboxyl group. Jones and Williams 96 have reported the formation of protonated species with the lanthanide $^{3+}$ ions and histidyl but here the protonation is on the imidazole nitrogen. In this present study, we found no protonated species for the aromatic phenylalanine-metal system thus confirming the results of Izatt et al 34 and Curched 90 . Clearly, the formation of complexes such as

is dependent upon the type of R group and so for aliphatic groups that are electron repelling 'e.g. -CH₃) then the positive charge on the nitrogen will undoubtedly be stabilised whereas for electron withdrawing R groups 'e.g. aromatic rings) the charged nitrogen will be destabilised and hence protonation inhibited thus encouraging complex formation. This extra stability of aromatic amino acid complexes has been noted by other authors ^{88,84}

Although protonated complexes were not present, hydrolysis was detected in the copper(II) and iron(III) systems. Hydrolysis in these systems is well authenticated 105, although formation constants have not been reported for hydrolysis (leading to polynuclearity) amongst simple amino acid complexes.

(c) The Individual Complexing Reactions

(i) Copper(II)

The +II oxidation state is dominant in the aqueous solution chemistry of copper because of the elements low second ionisation potential and the high energy of hydration for the Cu²⁺ ion. Chelating agents also encourage the +II oxidation state; for example ethylenediamine (en) reacts with copper(I) chloride in potassium chloride solution to give

$$2CuCl + 2 en = [Cu(en)_{2}]^{2+} + 2Cl + Cu$$

Hence complications, from varying oxidation states are unlikely to arise in our interpretation of the results obtained for the copper-phenylalanine system.

The formation of only Cuphe and Cuphe $_2$ may be expected under our experimental conditions since ethylenediamine $(\log \beta_1 \approx 9)$ forms a 3:1 complex "only at extremely high concentrations of en." 102

The copper phenylalanyl complexes were deep blue indicating a shift in absorption from the far red to the middle of the red region because of the stronger ligand field produced by the nitrogen donors.

In the presence of oxygen donors, copper forms a series of polynuclear complexes, the simplest of which is the hydroxy complex reported by $\text{Biedermann}^{41}. \quad \text{This as a dimer of structure}$

Hence, the formation of Cu₂(phe)₂(OH)₂ is not surprising, ther analogous structures are found in the acetate and diazoaminobenzene complexes (both dimeric), and the formate and benzoate (both polymeric) complexes 102. Of

thinking in the teacher of the exercise

these the acetate is the nearest analogue and also the most studied.

The Cu-Cu distance is sufficiently short to permit some metal-metal interaction and this has been detected from magnetic studies of the solid complex.

Dimerisation has thus been recognised as an important feature of Cu'II) chemistry when copper is in an "oxygen environment" and, for this reason, the Cu₂(phe)₂(OH)₂ complex merits further study.

Figure 21 shows the distribution of complexes as a function of pH for blood plasma copper and ligand conditions. Values of these concentrations were obtained from "The Biochemist's Handbook". The predominent species at the pH of blood (7.38) are Cuphe and Cuphe₂ and the concentration of the dimeric hydroxy species is present as 2% of the total copper.

Interpretations of the biological role of copper and its compounds ought to take into account such hydrolysed species if we are to learn from the analogy of the importance of hydrolysed iron species in liver storage.

(ii) Nickel(fI)

Nickel forms, almost exclusively, divalent compounds in solution but these can have a variety of stereochemistries, of which the most important are the octahedral, tetrahedral and square planar configurations. In the solid state the formation of polymers through ligand sharing is important 102.

The 1:1 and 2:1 complexes with the phenylalanyl anion are formed by substituting the water of the hexaquo ion [Ni'H20)6]2+, by the chelating phenylalanyl ion to give octahedral complexes having four and two water ligands respectively.

The solid diaquobisphenylalinato-nickel'II) will, almost certainly, have a structure analogous to that of the glycine complex - a distorted

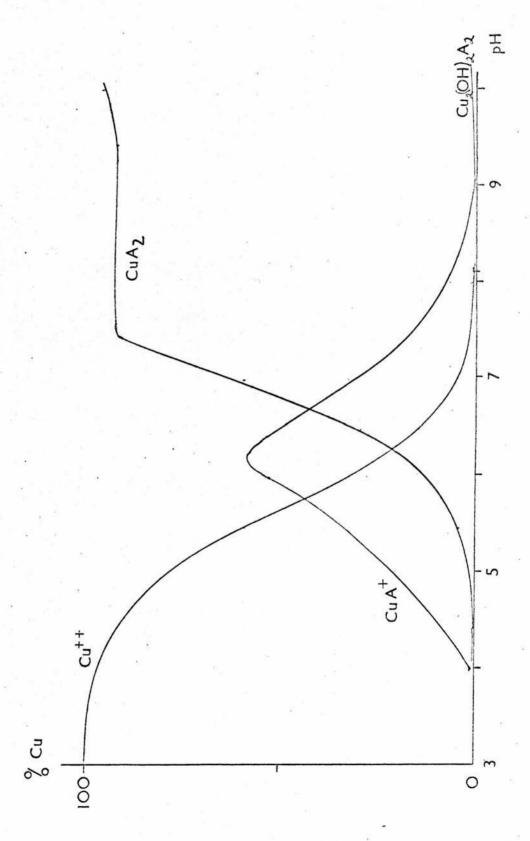


Fig. 21. Species distribution for the Cu +/Phe system in blood.

octahedra with two glycinate anions acting as chelating ligands in a plane and two water molecules occupying the <u>trans-axial positions</u> When heated in <u>vacuo</u>, this complex gives the anhydrous solid which is six-coordinate and contains terdentate ligands in which the carboxylate group is both bidendate and bridging There are other amino acids that behave in a like manner: α -alanine, β -alanine and α -amino-n-butyric acid. Hence, there is no apparent reason why phenylalanine ought not to be considered to form analogous compounds.

Although nickel is not an essential element for life in humans, iron, cobalt and nickel constitute group VIII of the first transition series and complexes of metals from this group are currently undergoing clinical trials as anticancer therapeuticals.

(iii) Cobalt(II)

Cobalt has two main oxidation states and, in the absence of complexing ligands, the +II is the most stable state in aqueous solution. Complexation particularly with nitrogen donor ligands, makes relatively easy

$$[\text{Co'NH}_3)_6]^{3+} + e^- \rightarrow [\text{Co(NH}_3)_6]^{2+} E^0 = 0.1 \text{ Y}$$

This stability of cobalt(III) complexes leads to an extensive solution chemistry and also, introduces the redox properties of the cobalt(II)/28 cobalt(III) couple, which biologically is very important.

The simple aqueous chemistry of cobalt(II), however, is similar to that of nickel. The major species exist as simple salts and in solution as $[\text{Co(H}_2\text{O)}_6]^{2+}.$ These mononuclear complexes are usually octahedral 102. The data obtained for the cobalt(II)-phenylalanine system was most similar to that for nickel, hence it is reasonable to assume that the insoluble complex

formed had the same composition and structure.

Several oxygen donor complexes of cobalt(II) are similar to those of nickel(II), the most striking examples being the polymeric nature of the acetylacetonates; the cobalt complex is tetrameric and the nickel complex trimeric 111.

The biological importance of cobalt has not been fully characterised and much more work, both <u>in vivo</u> and <u>in vitro</u>, is necessary before the full implications of the Co(II)/Co(III) couple, and the unusual stereochemistries of the complexes, are determined and understood.

(iv) Iron(II and III)

The iron'II) and iron'III) results are considered together since any discussion of either must necessarily account for the redox couple between them. Both ions form octahedral hexaquo ions in solution and simple octahedral complexes. The hexaquo iron'II) is unstable, with respect to iron(III), in the presence of an oxidising agent, for example atmospheric oxygen. The hydrolysis of iron'III) is a major feature of its aqueous chemistry.

Although the data that we obtained for the iron(II)-phenylalanine system is limited, it is more comprehensive than any comparable study published by other schools for the amino acid system. The iron'III) hydrolysed species is analogous to that of the copper complex and thus the following structure has been suggested for the dimer 102:

It is presumed that the Fe $_2^{III}$ (phe) $_2^{OH}$ will have a structure related to this hydroxy dimer and to the copper dimer discussed on page 96.

The Fe(II)/Fe(III) couple in 3.00 M (Na)ClO₄ was investigated but the oxidising power of the media was such that there was considerable potential drift rendering results unreliable. We intended to measure redox potentials for a range of complexes and thus describe the complete iron(II) iron(III)/phenylalanine system. This is a major project and would be the logical extension of the present work in addition to the calorimetric investigation of this iron system. The Fe(II)/Fe(III) couple has been extensively studied in the presence of a wide variety of ligands and most recently by Irving and Sharpe. The multitude of complexes that occur in these systems demand a computer and a specially designed program to calculate the results.

Conclusions and the Future

The human body is but 3% metals and yet life depends upon these elements far more than this figure suggests. For example, <u>in vivo</u> the transition metal ions usually occur in the active centres of enzymes which control the marshalling of amino acids into peptides. Chemical investigations of transition metal ion - amino acid interactions have been reported for over twenty years and there is still ample scope for further studies.

The present thesis presents thermodynamic parameters for the protonation and complex formation of phenylalanine, by in vivo standards a relatively simple ligand, and yet an intriguing range of polynuclear and hydrolysis species are soon encountered at biological pHs. Such complexes demand further investigation and especially the iron systems which compared to

their <u>in vivo</u> importance have received but occasional glances in this thesis. Knowledge of the <u>in vitro</u> chemistries of such systems does not always directly reveal <u>in vivo</u> mechanisms but it certainly helps!

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APPENDIX I

RWCALCOR --- Instruction sheets(2).
sample output
Program

Program

RWCALCOR

This program calculates the heat corrections for the formation of water, hydrolysed species and heats of protonation.

The heat corrections together with the change in concentrations of each complex are then solved to give the heats of formation of the complexes.

INPUT

The program is stored under the 44PS system in three versions:

- 1. gives normal output explained later.
- gives the normal output plus the heats of formation obtained from the experimental points for each experiment,
- gives normal output plus the heats of formation for the total job;

and is called as follows

DATA

/* /&

The experimental input is as follows:-

ITEM 1 (I2) No. of experiments (CARE: - can only deal with one SCOOS job at a time)

Item 2 (20A4) Title

Item 3 (512) No. of AH_r complexes, no. of BH_r (r-ve) complexes, no. of A_pB complexes, no. of A_pBH_r complexes. Integer for reference point i.e. M = 0 for every point refered back to first point (additive) M > 0 for point to point.

Item 3a (I2) Value of r in A_pBH_r complexes (omit of no A_pBH_r complexes)

Item 4 (7Ell.4) Heat of formation of water, heats of hydrolysis and
heats of protonation. (Secure out if not formed - no blanks)

Item 5 Output from SCOGS*. This consists of N (the no.
of points).

For two experiments items 2 to 6 are repeated $*$ The input for SCOGS must be in the same order as for Item 2

i.e. (i) Protonated species

(ii) Hydrolysed species

(iii) Complexes

OUTPUT

This is both printed and punched (Punched data for use in RWSOLV).

The punched data consists of (N-1) cards for each experiments, the first point being omitted as it is a reference point. Each card shows the corrected heat change and the change in concentration of each metalligand complex.

		ACLES	Z Z Z	MCLES MOLES	KC ES	MOLES FOLES	MOLES MOLES	* OLES	MOLES	MOLES
HEATS OF PROFCNATION 5.1469E C4 6.1000E C4 0.0	CHANGE IN CONCENTRATION	COMPLEX(1) = 8.38775-04 PCCMPLEX(2) = 1.06685-04 P	= 8.8496C-04 = 1.2732C-14	45-360-34 - 9.1908C-34	= 9.5081C-04	9.77948-04	20-34460.2 = 40-34460.3 = 40-34460.2 = 40-3600.2 = 40-3600.2 = 40-3600.2 = 40-3600.2 = 40-3600.2 = 40-3600.2 = 40-	= 1.01260-03 = 2.92040-04	CCMPLEX(1) = 1.0169C-U3 COMPLEX(2) = 3.4492D-04	COMPLEX(1) = 9.89420-04 CCMPLEX(2) = 4.88785-04
HEATS CF HYDRCLYSIS 0.0 0.0	Q-CCRRECTED	2.22850 00	5.8561D CO	9.C345D C0	1.28680 C1	1.64970 C1	1.58070, C1	2.4188D C1		3.67560 C1
HEATS	HYCROLYSIS	0.0-	0.0-	0.0-	0.0-	0.0-	0.0-	0.0-		0.01
	RECTONATION HYCROLYSIS	-5.2948D CO	-1.077CD C1	-1.64460 01	-2.22990 01	-2.8464D 01	-3.4870D C1	-4.16150 C1	-4.86880 CI	-6.39820 G1
2 = 0 5.5689E 04	MATER	1.11460 01	2,22956 01	3.34260 01	4.45270 01	5.56980 01	6.6828C 01			1.11425 02
NUMBER OF LIGAND COMPLEXES = 2 NUMBER OF HYDRCLYSED SPECIES = 0 HEAT OF FORMATION OF MATER = 5.56	C-MEASURED	8.07980 00	1.74210 01	2.66150 01	3.50960 01	4.37310 01	5.17650 01	6.05630 01	6.89140 01	8.41950 01
	VCLUME	101.5600	103.5000	105.9666	107.5000	109.5000	111.5000	113.5000	115.9000	119.5000
THE NUMBER OF THE HEAT OF	10	3.6976	3.1557	3.2173	3.2832	3,3536	3.4296	3.5122	3.6026	3.8130

END OF JCB

```
CHANGE IN CONCENTRATION FROM M TO I OF THE SPECIES.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             HEAT (IN JOULES) EVOLVED IN THE REACTION FROM M TOI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         UNDER INVESTIGATION. (HEATS OF PROTONATION FOR NCX
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       CORRECTION FOR THE PROTONATION OF THE LIGAND.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 HEAT EVOLVED (TAKE IN) BY THE REACTION OF SPECIES
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        CORRECTION FOR THE HYDROLYSIS OF THE METAL.
                      CALCULATION OF HEAT CORRECTIONS & CHANGE IN CONCENTRATIONS OF COMPLEXES
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                CORRECTION FOR THE FORMATION OF WATER.
                                                                                                                                                                                                                                                                                                                                         DOUBLE PRECISION SUMP%4<, SUMQ%4<, SUMR%4<, SUMS%4<, P%4<, Q%4<, R%4<,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    CALIBRATION FOR CALORIMETER AT POINT 'I'.
                                                                                                                                                    , QCORR%25) , CORPRO%25) , CCRH20%25)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            CHANGE IN TEMP (RESISTANCE) FROM I TO I+1
                                                                                                                                                                             ,VULF%25) , H%25) ,TITLE(20), HH(20)
                                                                                                                          , SIGMAC 25)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    CONC. OF PROTONATED SPECIES 1 TO NLC
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             CONC. OF METAL HYDROLYSED SPECIES
                                                                                                                                                                                                                                                                                                                                                                                     THE PH OF THE SYSTEM AT POINT 'I'
                                                                                                   ,HHYD(20),
                                                                                                                                                                                                                                                                               T%4<, A%50,5<, AD%50<, V%4<, SUMT%4<, QCALC%50<, PCENT%50<
                                                                                                                                                                                                                                                                                                                                                                                                                                                            CCNC. OF SPECIES(J =)1 TO NCX
                                                                                                                                                                                                                                                                                                       DOUBLE PRECISION C(4,4), AC(4,4), PP(4), CC(5,4), DSQRT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        METAL-LIGAND COMPLEX CONCS.
                                                                                                                            , DC%20,25) ,HYD(20,25)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         UNDER INVESTIGATION.
                                                                                                   QCQR(25) , DCI(25,25)
                                                                                                                                                                                                                                                                                                                                                                                                                                   CCNC. OF FREE ACID
                                                                                                                                                                                                                                                                                                                                                                                                            TOTAL VOLUME
                                                                                                                                                                                                                               ,NH(10)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    HEAT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              HEAT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       HEAT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           CALIB%25) , QMEAS%25)
                                                                                                                                                                             3 , CORHYD%25) , ZU(25)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        CORHYD(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              SIGMAC(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              CORH20(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       CORPRO(I)
                                                                                                                                                                                                                              DIMENSION NA(4), NB(4)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    CALIB(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  QCORR(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             QMEAS(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             HYD(J,I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      LIG(J,I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        XC(JJ,I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                             XC(J, I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 DC(3,1)
                                                                                                                                                                                                                                                                                                                                                                                                           VOLF(I)
                                                                                                                          XC %20,251
                                                                                                                                                                                                                                                                                                                                                                                    ZU(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                     (I)H
                                                                                                                                                                                                     REAL*8 LIG(20,25)
                                                                                                  DOUBLE PRECISION
                                                                                                                                                                                                                                                                                                                                                           PARAMETERS USED
\circ \circ \circ
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VALUE OF J IN XC(J,I) TO GIVE 2ND. HYDROLYSIS CX.
                                                                                                                                                                                                                                                                                                                                                                                MM IS AN OPTION. IF = 0 THEN ALL CALCULATIONS REFER TO POINT 1 AS BASE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   ), (HH(L), L = 1, NLC)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           (HH(L) \cdot L = 1 \cdot NLC)
                                                                                                                                                                                                                                                                                                                                                                                                       ALL OTHER VALUES GIVE "POINT BY POINT".
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              * INPUT -- IF ANY ABH SPECIES ONE CARD (ITEM 3A)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     NH(L), L = 1, NABH)
                                                                                                                                                                                                                                                                                                      WHYDR IS THE NUMBER OF HYDROLYSIS COMPLEXES.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      , NHYDR , NCX , NABH , MM
                                                                                                                                                                                                                                                                                                                                                                                                                                                         HW IS THE HEAT OF FORMATION OF WATER
                                                                                                                                                                                                                                                                              NLC IS THE NUMBER OF LIGAND COMPLEXES.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       * INPUT -- ONE CARD (ITEM 4)
READ(5,40)HW,(HHYD(L),L = 1, NHYDR
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             (ITEM 3)
(ITEM 1)
                                                                                                                          (ITEM 2)
                                                                                                                                                                                                                                                                                                                             NABH IS THE NUMBER OF ABH SPECIES
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          HEATS OF PROTONATION
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 HEATS OF HYDROLYSIS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      IF (NABH.GT.0)READ(5,30) (
* INPUT -- ONE CARD
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             INPUT -- CNE CARD
                                                                                                                         * INPUT -- CNE CARD
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              INTEGER - NHYD
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                IF (NHYDR.EQ.0)GU TO 41
                                                                                                  DO 1090 KKK= 1,KKKK
                                                                                                                                                   TITLE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      READ (5, 30) NLC
                        READ (5,10) KKKK
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            40 FORMAT (7E11.4)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         READ(5,40)HW,
                                                                                                                                                                                                     20 FORMAT (20A4)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  FORMAT (512)
                                                                                                                                                   READ(5,20)
                                                                       10 FORMAT(12)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              ***
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 HHYD(L)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           HH(L)()
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  30
```

99 FORMAT ('1')

NHYD = NHYDR+ NLC

INTEGER - NDP2 VALUE OF J IN XC(J,1) TO GIVE 1ST. HYDROLYSIS CX. BECOMES THE TOTAL NUMBER OF ALL SPECIES PRESENT INTEGER - NHYD2 VALUE OF J IN XC(J,I) TO GIVE 1ST. M-L CX. IF (NABH.GT.O) NCX = NCX + NABH NCX INTEGER -NCX = NCX + NHYD MHYD2 = NHYD + 1 NDP2 = NLC + 1***

** CUTPUT -- NEW PAGE AND TITLE OF EXPT. (ITEM 2 OF INPUT) WRITE(6,100) TITLE

WRITE(6,105) NLC ,NHYDR, HHYD(1) , HW , HHYD(2) ,HH(2),HH(3 4 45X, 1PE11.4, 15X, 1PE11.4, /1X, 'THE HEAT OF FORMATION OF WATER FORMAT ("I",43X,20A4,/43X,"*********************** 105 FORMAT(1X, THE NUMBER OF LIGAND COMPLEXES = 'II, 240X, 'HEATS OF HYDROLYSIS', 10X, 'HEATS OF PROTONATION'/, 1X, 5 = "IPE11.4,38X,IPE11.4,15X,IPE11.4/,108X,IPE11.4/, *THE NUMBER OF HYDROLYSED SPECIES = ", II, ** OUTPUT -- INPUT ITEMS 3 & 4 2), HH(4) 100

110 FORMAT(" '/6X, 'PH', 8X, 'VOLUME', 5X, "Q-MEASURED', 2X, ******** H 2 4X, "Q-CORRECTED", 6X, "CHANGE IN NO. OF MOLES", /43X, "WATER", 5X," LEAT CORRECTIONS ********* 3PROTONATION*, 4X, "HYDROLYSIS"/) WRITE (6,110)

6108X,1PE11.4//)

DATA AS DIRECTLY FROM SCOGS(3).

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(ITEM 5). (IF TOTAL NO. OF CXS.> 7 THEN'3N'CARD
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            POINT 'I' NOW MEANS THE CHANGE ASSOCIATED WITH THE REACTION FROM M TOI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 FOR LIGAND PROTUNATION HEATS CONTINUE BUT FOR M-L CXS. GC TO 2000
                                                                                                          M IS A VALUE ONE BEHIND I IN THE "DO" LCCP
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 2050 DC(JJ*I) = (VOLF(I)*LIG(J*I) - VOLF(M)*LIG(J*M))*0.001
                                                                                                                                                                                                                                                                                                                                                                                                                                         IF NO HYDROLYSED SPECIES GO TO STATEMENT 1030
   (ITEM 5)
                                                                                                                                                                                                                                                                                                                                                          READ (5,40) (XC(J,I), J=1,NCX)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           IF (NCX.NE.NHYD)GO TO 2000
                                                                                                                                                                                                                     * INPUT -- "ZN" CARDS
                                                                                                                                                                                                                                                READ (5,50) ZU(I), VOLF(I)
                                                                                                                                                                                                                                                                          H(I)=DEXP(-2.3026*ZU(I))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                     IF (NHYDR.EQ.0)GU TO 1030
* INPUT -- CNE CARD
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      GO TO(1020,1010),NHYDR
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  1010 HYD(2,1) =XC(NHYD,1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          1020 HYD(1,1) =XC(NDP2,1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            J = 1, NLC
                                                                                                          INTEGER -
                                                                                                                                                                                                                                                                                                                                                                                     DO 1000 J = 1,NLC
                                                                                                                                                                  IF (MM.EQ.0) M = 1
                                                                                                                                                                                                                                                                                                                                                                                                             1000 LIG(J,I) =XC(J,I)
                                                                                  DG 1060 I = 1,N
                                                                                                                                                                                                                                                                                                                                FORMAT (2E11.4)
                          READ (5,10)N
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     GO TO 1060
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     1030 CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            00 2050
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         2060 CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 0 = 66
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 2000
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FOR EITHER ACID INTO ACID OR BASE INTO BASE TITRATIONS, NO WATER IS FORMED.
HENCE, THE HEAT CORRECTION IS MISSED OUT. (GO TO 1071)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     1073 CORPRO(I) = CORPRO(I) + 0.001 * HH(L) *(VOLF(I) * LIG(L,I) - VOLF(
                                                                                                                          1050 DC( J_{\bullet}I) = (VOLF(I)*XC( J_{\bullet}I) - VOLF(M)*XC( J_{\bullet}M))*0.001
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           CURRECTIONS FOR WATER, HYDROLYSIS EPROTONATION
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            IF (MM. EQ. 0) QMEAS(I) = QMEAS(I) + QMEAS(I-1)
                                                                                                                                                                                                                                                                                                                 READ(5, 51)(SIGMAC(1), CALIB(1), I = 2,N)
                                                                                                                                                                                                                                                                                     INPUT -- 'N-1' CARDS (ITEM 6)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            IF (2U(I).LT.ZU(M)) GO TO 2072
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            GC TC 1071
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              .F(ZU(I).GT.ZU(M)) GO TO 2071
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           QMEAS(I)=SIGMAC(I)*CALIB(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        IF (NCX.EQ.NHYD)GD TO 2070
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             2070
                                                                                                                                                                                                                        READ CALCRIMETRY DATA IN,
DO 1040 J = NHYD2, NCX
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           IF (NHYD.GT.0)GO TO
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         DO 1073 L = 1,NLC
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          IF (ZU(I).LT.7.00)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             IF (MM. EQ. 0) M = 1
                                                         1040 XC(JJ,I) =XC(J,I)
                                                                                           DO 1050 J = 1,JJ
                                                                                                                                                                                                                                                                                                                                                                                                                                                DO 1070 I = 1,N
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    2M) * LIG(L,M))
                                                                                                                                                                                                                                                                                                                                                                                    FURMAT (2F10.3)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            GU TU 2070
                              + 17 = 17
                                                                                                                                                          1060 CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                   0
||
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OUTPUT -- VALUES OF GCORR(I), ZU(I), VOLF(I), QMEAS(I) & HEAT CORRECTIO
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  1072 CORH20(1) = CORH20(1) - NH(L) * (VOLF(I) * XC(L,I) - VOLF(M)*XC(L,M
                                                                        2070 CORH20(I) = -(0.001*(VOLF(I)*(LIG(1,I) + 2.0*LIG(2,I) + 3.0*LIG(3,
                                                                                                                                                       VCLF(M)*(LIG(1,M) + 2.0*LIG(2,M) + 3.0*LIG(3,
                                                                                                                                                                                                                                                                                                                                                   FITRATION , HENCE THE WATER PRODUCED IS THE REVERSE QUANTITY .I.E.
                                                                                                                                                                                                                                                                                                             THIS STATEMENT CALCULATES THE LOSS OF PROTONS FOR A BASE INTO ACID
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  NS FOR I = 2,N
119 WRITE(6,120) ZU(I) , VOLF(I) , QMEAS(I) , CORH2O(I) ,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     CORHZO(I) = CORHZO(I) - 0.001 * HHYD(L) * (VOLF(I) * HYD(L,I) -
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  1069 CORHYD(I) = CORHYD(I) + 0.001 * HHYD(L) * (VOLF(I) * HYD(L,I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               = QMEAS(I) - (CORPRO(I)+CORHZO(I)+ CORHYD(I))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        120 FORMAT (2(3X, F8.4), 4(3X, 1PE11.4), 6X, 1PE11.4)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                ** OUTPUT -- VALUES OF DC(J,I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     WRITE(6,130)(J,DC(J, I),J = 1,JJ)
                                                                                                                                                                                             4M) + 4.0%LIG(4,M) + H(M))) )*HW
                                     IF (ZU(I).GT.7.00) GO TO 1071
                                                                                                                2I) + 4.0*LIG(4,I) + H(I)) -
                                                                                                                                                                                                                                                                                                                                                                                                                                                                     IF (NABH. EQ. 0) GO TO 1071
2071 IF(NLC.GT.0)GD TD 2070
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       SO(1) = -DCOC10(H(1))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           2CORHYD(I) , QCORR(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     2 VOLF (M) * HYD (L,M))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  DO 1069 \ L = 1, NHYDR
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           DC 1072 L = 1,NABH
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  IF (H(I))119,119,118
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          100°0 % MH %
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          DG 1080 I = 2,N
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             2 VOLF (M) * HW
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             1071 CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               QCORR (I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          118
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130 FORMAT(101X, 'COMPLEX('II,') = 'IPE11.4, ' MOLES')
1080 CONTINUE
WRITE(6,150)
150 FORMAT(1X, ///40X,' END OF JOB')
1090 CONTINUE
STOP
END
```

APPENDIX II

RWSCOGSY --- Instruction sheets(3)
Program

RWZASCOG --- Instruction sheet Program

RWSCOGSY

This program is the version of $SCOGS^1$ used on the St. Andrews I.B.M. 360/44 computer. The program refines estimates of the Stability Constants for systems containing up to two metals and two ligands and can deal with protonated and mixed species. pK's are considered complexes of A and H^+ .

Several modifications have been made to the imput and output, so care ought to be exercised if this version is to be compared with the published program.

INPUT

The program is stored under the 44PS system and is called using the following cards:-

The experimental data is as follows

ITEM 1 (I2) Number of Jobs

ITEM 2 - (I2) Type of output required:-

- Ol Normal Iteration procedure
- 02 Normal Iteration procedure plus punched output
- 03 No iterations with punched output

NOTE: The punched output is for use in RWCALCR

ITEM 3 (12) The number of experiments to be refined together.

ITEM 4 (312) Total number of ligands, total number of metals and total number of complexes (including protonated Figands)

ITEM 5 (512,F8.4) For each complex a card carrying: No. of A_1 , no. of A_2 , no. of B_1 , no. of B_2 , no. of hydroxyl ions (-ve sign for protons), contained in the complex, the logarithm of the Formation Constant of the corresponding species (β_j) ITEM 6 (212) No. of dissociable protons on ligand 1, no. of protons on ligand 2, in the forms in which they were added to the solution (e.g.(1) histamine is zero but histamine dinitrate is two e.g.(2) phenylalanine is one)

ITEM 7 (20A4) Title of the experiment.

ITEM 8 (7F10.3) Initial concentrations of B_1 , B_2 , A_1 , A_2 , acid* and volume (Titrate (S))

ITEM 9 (7F10.3) Concentrations in titrate (T) of B₁, B₂, A₁, A₂, acid*, FO (in mV), FN (no. of mV/pH i.e. 59.162 at 25°)

ITEM 10 (2F10.3,4x,I1) One card for each experimental point bearing the titre in ml, Emf and Index (zero for all cards but the last)

ITEM 11 (2F8.4) -pK $_{\rm W}$ and activity coefficient

ITEM 12 (212) No. of cycles of refinement desired (about 5) and no. of constants to be varied.

ITEM 13 (I2,F10.3) One card for each constant to be varied carrying the no. of the constant (in order of listing in Item 4) and the amount by which it is to be varied each time (0.0004 is usually enough)

When two sets of experiments are refined together the sequence of cards is: ITEMS 1,2,3,4,5,6,7,8,9,10 (for lst expt.), 7,8,9,10 (for 2nd expt.), 11,12,13

(When two experiments are refined together it is considered as one job)..

For separate jobs, Items 2-13 are repeated for each job until the number in Item 1 is reached.

(* Acid is mineral acid)

OUTPUT

The output as far as the end of refinements should be self explanatory. Next there appears a long list of values of interest. These are calculated from the final formation constants, and are again self explanatory except for YH and YB. These are as defined in the Osterberg paper.

CARE: - All the output quantities have been calculated and are not the experimental (For experimental values use RWZASCOG (ZBAR) and RWYLOGH (YH and YB))

References

- 1. Sayce I.G., Talanta, 1968, 145, 1397.
- 2. Österberg R. and Sjöberg B., J. Biol. Chem., 1968, 3038.

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SCUGS WITH A GENERAL INPU JUNE 5TH 1970. THIS PROGRAM IS WRITTEN IN FORTRAN IV(E)	DOUBLE PRECISION CK(20), BC(20,20), CC(20,20), BTOT(2), CLTCT(2), 1Y1(2), Y2(2), Y3(2), Y4(2), E(20), B(20), EORIG(20), TX(2), VX(2), C(20), CLTCT(2), CLCTC(20), CLTCT(2), CLTCT(2), CLTCT(2), CLCTC(20), CLTCT(20), CLTCT	DIMENSION NORC(30) ,SIGMAM(2) ,SIGMAL(2) , ZBAR(2,2) ,YBB(2,2) 6,Y(2) ,AMN(20), VOLF(500) ,TLT(2) ,TMT(2) ,AML(2,20), AMM(2,20	DIMENSIBN TITLE(20), ML(2,20), MM(2,20), MN(20), AL(2,20), AM(2,20), LAN(20), NDP(2), ENDP(2), TM(2), TL(2), TITRE(60), ZU(60), ZB(2,60), ZZL(2,60), U(500), AC(500), BA(500), V(500), TITR(500), TEMP(20,20), 3BB(2,500), CL(2,500), IG(20), H(20), HORIG(20), UXS(500), NINCCH(500), 4ICH(20), DM(2), DMY(2), IFR(30)	COMMON C, YI, Y2, Y3, Y4, BTOT, CLTOT, TX, VX, HO, B, IML, MM, MN, AL, AM, AN, NL, NM, N, UX, F, CKW, NIT, NNCI, KJ	INTEGER TYPE	FORM/ FORM/ FORM/	FORMAT (FORMAT	FURMA FURMA		FURMA	1, F7.3/
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          285
                                                                                                                                                                                                      16
                                                                                                                                                                                                                                                                                                        234
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 283
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                (//2X, 'K', 3X, 'PH', 5X, 'TITRE', 5X, 'RESID', 6X, 'TM1', 8X, 'TM2', 8
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  12X, 'C1', 9X, 'C2', 9X, 'C3', 9X, 'C4', 9X, 'C5', 9X, 'C6', 9X, 'C7', 9
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  8X, C11', 8X, C12', 8X, C13', 8X, C14', 8X, C15', 8X, C16', 8X,
                                                                                                                                                                                                                                                                              OVERSHIFT, VARIABLE CONSTANT NO. ', 12, ' X(I)=', 1PE10.3)
                                                                                                                                                                                                                                                                                                   183 FORMAT (/' EXTREME OVERSHIFT, VARIABLE CONSTANT NO. ',12,' X(I)=',
                                                                                                                                                                                                                                                                                                                                                      196 FORMAT (/' THE STANDARD DEVIATION IN TITRE WITH THE INPUT CONSTANT
                                                                                                                                                      READINGS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        IX, 'TL1',8X, 'TL2',8X, 'FM1',8X, 'FM2',8X, 'FL1',8X, 'FL2',12X, 'YH'/,
                           F9.6,  E0 = 1, F7.2
    F9.6
                                                                                                                                                                                                                         (/' INCREMENT FOR VARIABLE CONSTANT ', 12, ' RAISEC')
                                                                                                                                                                                                                                                                                                                                                                                                      (/' THE STANDARD DEVIATION IN TITRE IS ', IPE11.4)
                                                                                                                                                 FORMAT (/' NUMBER OF PARAMETERS ', 12/' TOTAL NUMBER OF
   M2 = ",
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   ZIZ FORMAT (IX,13/4X,F6.3,2F11.6,8(1X,1PE10.3),2X, OPF7.4)
                                                                                                                                                                                                                                                     (/' INCREMENTS CHANGED FOR ', 13,' POINT(S)')
                                                                                                                                                                                                                                                                                                                                                                                                                                                                              (/ HALF SHIFTS APPLIED FOR NEXT CYCLE")
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          5C17',8X,'C18',8X,'C19',8X,'C20',12X,'ZBAR1,1'/)
   F9.6,
                                                                                                                                                                                                                                                                                                                                                                                                                                                      (1X,12,F12.4,F8.4,2X, 'SHIFT=',F7.4)
                         ACID = .
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          3X, 'C8', 9X, 'C9', 8X, 'C10', 12X, 'YB1, 1'/,
   M.1 =
                                                                                                                         (/' CKWL=',F7.3,5X,'F=',F5.2/)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        (/ CYCLES CALCULATED ', 12)
                      F9.6, ' L2 = ', F9.6,
                                                                        FURMAT ( ' , I3 , ' READINGS ) ' / )
, IIX, 'TITRANT
                                                                                                                                                                                                                                                                                                                                                                                                                              (/ XI NEGATIVE')
                                                 116 FORMAT (2F10.5,4X,11)
                                                                                                                                                                                                                                                                                                                                                                              1S IS ',1PE11.4/)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               READ(5,99) TYPE
                                                                                                 FORMAT (2F8.4)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             READ (5,99) NJ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             READS IN DATA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       WRITE (6,999)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           FORMAT (1H1)
                                                                                                                                                                                                                                                                          .
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     CALL CLEUND
                                                                                                                                                                                                                                                                                                                             11PE10.3)
                                                                                                                                                                           1,13/)
                                                                                                                                                                                                                                                                                                                                                                                                      197 FURMAT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  209 FORMAT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          FORMAT
                                                                                                                                                                                                    L26 FORMAT
                                                                                                                                                                                                                            FORMAT
                                                                                                                                                                                                                                                     FURMAT
                                                                                                                                                                                                                                                                                                                                                                                                                                FORMAT
                                                                                                                                                                                                                                                                                                                                                                                                                                                        FORMAT
                                                                                                                           FURMAT
                                                                                                                                                                                                                                                                              FURMAT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                FORMAT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               NJD=0
                                                                                                                                                                                                                                                                                                                                                                                                                                                        202
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19	20	23	25 26 27 27	30	32		43	45 46 48
						N P	,TMT(1),	
	,J),I=1,2),MN(J),E(J)				AL EXPERIMENT	ACID, VOL	,TL(2) ,ACID ,VOL	
INEXP NL,NM,N	(ML(I,J),I=1,2),(MM(I,J),I=1,2),MN(J),E(J) J)		(1, J) J) J) (NDP(I),I=1,2)		, INEXP ATION DATA FOR INDIVIDUAL	TLE (1),TM(2),TL(1),TL(2),ACID (1),TMT(2),TLT(1),T	,TM(2) ,TL(1) TLT(2) ,ACIDT ,E0	= 1 TRE(K), ZU(K), INDEX 115,117
READ (5,101) IN READ (5,105) NL DD 106 J=1,N	READ (5,107) DD 109 J=1,N EL(J) = 10.**E(-1-	AMM(I, J) = MM AL(I, J)=ML(I, AM(I, J)=MM(I, READ (5, 110)	ENDP(I)=ND ITN=0 DD 231 I=1 IFR(I)=0	EXP=1	READ (5,102) TIT WRITE (6,103) TI READ (5,113) TM(READ(5,113) TMT(BASF = -ACIDT	TE(6,114) (2) ,TLT = 0	IF(TYPE.EQ.3)KK K=K+1 READ (5,116) TI IF (INDEX) 117,
007	106		601	231	ادر	ر		115

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WRITE (6,108) J, (ML(I,J), I=1,2), (MM(I,J), I=1,2), MN(J), E(J) , EL(J)
                                                                                                                                         ZB(I,K) = (TM(I)*VOL + TMT(I)*TITRE(K))/VOL1
                                                                                                                                                           2L(I,K) = (TL(I)*VOL + TLT(I)*TITRE(K))/VOLI
                                                                                                                                                                                                                                                 COMBINES DATA FOR INDIVIDUAL EXPERIMENTS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    TURM(K)=CL(1,K)*ENDP(1)+CL(2,K)*ENDP(2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  [F(TYPE.NE.1) WRITE(7,99) NORC(1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    WRITE (6,111) (I,NDP(I),I=1,NL)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            (6,123) CKWL,F
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         READ (5,122) CKWL,F
                                                                                      ZU%K<#%E0-ZU%K<</FN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             (6,124) N,ITN
                                                                                                                                                                                                                                                                                                                                                                                           TITR(K)=TITRE(MIN)
                                                                                                        VOL1=VOL+TITRE(K)
                                                    WRITE (6,118) NOR
                                                                                                                                                                                                                                                                                                                                                                                                                            BB(1,K)=ZB(I,MTN)
                                                                                                                                                                                                                                                                                                                                                                                                                                               CL(I,K) = ZL(I,MTN)
                                                                                                                                                                                                                                                                                   DO 120 K=KTN,LIN
                                 NORC(KKK) = NOR
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   DG 1210 K=1,ITN
                                                                     OU 119 K=1,NOR
               KKK = KKK + 1
                                                                                                                                                                                             (FR(NEXP)=KIN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     WRITE (6,104)
                                                                                                                                                                                                                                                                                                                                                                                                            DO 120 I=1,2
                                                                                                                        DO 119 I=1,2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         J=1,N
                                                                                                                                                                                                                                                                                                                      J(K)=ZU(MTN)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                ITN=ITN+NOR
                                                                                                                                                                                                               LIN=IIN+NOR
                                                                                                                                                                                                                                                                                                                                       AC(K)=ACID
                                                                                                                                                                                                                                                                                                                                                        BA(K)=BASE
                                                                                                                                                                             KTN=ITN+1
                                                                                                                                                                                                                                                                                                     MIN=K-IIN
                                                                                                                                                                                                                                                                                                                                                                          V(K)=VOL
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        DU 301
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           WRITE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            MRITE
 NOR=K
117
                                                                                                                                                           119
                                                                                                                                                                            5003
                                                                                                                                                                                                                                                                                                                                                                                                                                               120
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IF(TYPE.EQ.3) WRITE(6,209)
READ (5,110) NCD,NCV
                                      READ (5,126) IG(I),H(I)
127 HORIG(I)=H(I)
                                                                             BEGINS REFINEMENT
                                                                                                                                                          UXS(K)=10.**U(K)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                              CLT0T(I)=CL(I,K)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                 BTCT(I)=BB(I,K)
                          DO 127 I=1,NCV
                                                                                                                                              00 129 K=1,1TN
                                                                                                                                                                                                                                                                             DO 131 K=1,1TN
                                                                                                                                                                                                                                                                                                                                                                                     00 133 J1=1,20
                                                                                                                                                                       30 1290 I=1,2
                                                                                                                                 CKW=10.**CKWL
                                                                                                                                                                                                                                                                                                                     EDRIG(J)=E(J)
                                                                                                                                                                                                                                                                                                                                 00 133 J=1,20
                                                                                                                                                                                                                                                                                                        DO 132 J=1,N
                                                                                                                                                                                                                                                                                                                                                                                                                                                     00 136 I=1,2
                                                                                                                                                                                                                                                                                                                                                                                                  CC (1,1)1)=0.0
                                                                                                                                                                                                                                                                                          NINCCH(K)=0
                                                                                                                                                                                                                                                                                                                                               C(3) = 0.0
                                                                                                                                                                                   TX(I) = 0.0
                                                                                                                                                                                                                                                                                                                                                                         CK(1)=0.0
                                                                                                                                                                                                1290 VX(I)=0,0
                                                                                                                                                                                                             NCC=NCC+1
                                                                                                                                                                                                                                                                                                                                                            0=(r)H)]
                                                                                                                                                                                                                                                    SQRD=0.0
                                                                                                                                                                                                                                                                 INCCH=0
                                                                                                                                                                                                                                        SQR=0.0
                                                                                                                                                                                                                           NNCI=0
                                                                                                                                                                                                                                                                                                                                                                                                                                         NE XP=1
                                                                                                                   1CC=0
                                                                                                      0=33N
                                                                                                                                                                                                                                                                                                                                                                                                                0=7
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	NTRATI					AND
	CONCENTRATI					LIGAND,
	LIGAND					FREE LI
	FREE					TAL,
	AND					FREE ME M(K)+HO
	METAL					INE FOR CALCULATION OF ALL FREE MENTRATIONS 150,215,215 URM(K)+AC(K)-HD)/(BA(K)-TURM(K)+HD
	FREE					N OF 1
	E FOR	45				LAT 101
01 001	STIMATE 40		147	8,146 MN(J1		INE FOR CALCULATION NTRATIONS 150,215,215 URM(K)+AC(K)-HD)/(B
*0.0000001)*0.0000001	IAL ES 140,14	142,	.146.	M 146,148,146 J1)*UX**MN(J1 +DM(I)	(D) ×4	INE FOR CAL NTRATIONS 150,215,215 URM(K)+AC(K
* 0	INITI 139,1	140,	N N N N N N N N N N N N N N N N N N N	*NM (1)) 1 (E(J1) (1)+DM	NL (1)/0	
(S (K) 38 I=1,2 =BTOT (I	RMINES ICC-1)	-IFR (N T-99)	BIOT (BIOT (I=1,0 J=1.0	8 KI=1 N(KI,J) NUE 10.**	1UE 5 I=1, 6 CLTOT 0 I=1, 0,**E	SUBROUT S CONCEI GGSNR ICI-30)
J=0 M=0 UX=UXS DB 138 Y1(1)= Y3(1)=	DETERN IF (IC	IF (K-	1 DU 144 1=1,NM 4 VX(I)=BTOT(I) DO 146 I=1,NL DMY(I)=1,0 DO 146 J1=1,N IF (ML(I,J1))146,146,147	DO 148 IF (MA CONTIN DM(I)=	CONTIN DU 145 TX(I)= DU 149 B(I)=1 KJ=K	
138		142	J J	147	146 145 140 149	720
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152 153 154 155 156 158 160 161 163	164 165 165 166 167 168 170 171 173	177 178 179 180 181
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		DIFFERENTIATION
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221	DIFFERENTIAT (J) (J)	USED H(J))
20,220,22 2,153 16,216 ,157),M	11 FFE	*
220,220, 52,153 216,216	I I	R EMENT
	(ICAL (IS)+ (IS)- (IS)	
TR(K) DTII 1001 152, 154, 154, 314, 31	51NS NUMERIC 34-1 15)=E0RIG(19 15)=E0RIG(19 2=CCTITR 15)=E0RIG(19 170 140 18)=E0RIG(19 18)=E0RIG(19	S INC)*5.0
17R = 11 11 - 11 1 - 13 1 - 13	(J) (CC+ (CC+ (LT) (T) (T) (T) (T) (T) (T)	ASE. H(J)=1 H(K) H(K)=(C)=(C)
CT=CTITR DTITR=TITR(K) R=CTITR-DTITR IF (NIT-100) 2 R=0.0 IF (KK) 152,15 IF (L-1) 154,2 M=M+1 GO TO (155,156 SQRO=SQRO+R*R CTI=CTITR		INCREASES INC SMALL H(J)=H(J)*5.0 INCCH=1 ICH(J)=1 NINCCH(K)=1 GO TO 160 DE(J)=(CT2-CT
	BE 15 15 15 15 15 15 15 15 15 15 15 15 15	
222 222 15 15 15	5 7 7 7	158
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213
                                                                                                                                                                                                                                                                                                                               CALLS MATRIX INVERSION SUBROUTINE, AND SOLVES FOR SHIFTS
                                                                                                                                      CC(II, JJ)=CC(II, JJ)+DE(II)*DE(JJ)
                                                                                                                                                                                                                                  IF (ICH(I)) 171,171,172
                                                                                                                 CK(II)=CK(II)-RD*DE(II)
                                                                                                                                                                                                             IF (INCCH) 169,169,170
          IF (J-NCV) 161,162,162
                                                                                                                                                                     IF (K-ITN)135,135,167
                                                   E(15) = EORIG(15) +H(J)
                                                                                                                                                                                                                                                                                      NICH=NICH+NINCCH(I)
                                                                                                                                                                                                                                                                                                                                                   CALL SUB760(BC,NCV)
                                                                                                                                                                                                                                                                                                          WRITE (6,175) NICH
                                                                                                                            DO 163 JJ=1,NCV
                                                                                                       DO 163 II=1,NCV
                                                                                                                                                                                                                                             WRITE (6,173) I
                                                                                                                                                                                                   BC(1,1)=CC(1,1)
                                                                                                                                                                              DO 168 I=1,NCV
                                                                                                                                                                                         JO 168 J=1,NCV
                                                                                                                                                                                                                        DO 171 I=1,NCV
                                                                                                                                                                                                                                                                            DO 174 I=1, ITN
                                                                                   SETS UP MATRIX
                                                                                                                                                                                                                                                                                                                                                                         DO 176 I=1,NCV
176 X(I)=0.0
H(J)=HORIG(J)
                                                                                                                                                                                                                                                                                                 NINCCH(I)=0
                                                             GD TO 140
                                                                                                                                                                                                                                                       CONTINUE
                                         15=16(J)
                                                                                                                                                                                                                                                                  VICH=0
                    J=J+1
                                                                                                                                                          1CC=0
                                                                                                                                                 K=K+1
                               M=1
                                                                                                                                                                                                                                                                                                                                                     169
                                                                                                       162
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, J. *C.	- X -	*18 8*1		2 7,	6.8.3	190,191 V AT(ITN-NCV V S)+X(I) 4,194,195
*	H 1/2	1,180 1,17	×		7	190,19 V V V S)+X(I
255	OF SH SHIFT SHIFT	179) 18 2) I	3) I	84,1 NCV) 18	183	*0-00 HO
=1, +8, (×(ANY	~ a a	8 4 18		95 0	19 19 19 11, 11,
77 77 = X (= 0 0 0 A B	KS S CES			Se si	184 186 187 187 187 187 187 187 187 187 187 187	C C C C C C C C C C
DO 1 X(1) X(1) 1EOS 1OS= DO 1 XAB=	CHEC 0.5. REDU	F (F (BIT	E OS RIT	NO TO TO		N X (1) N X
7.		180	179	78	187 189 186 (184 191 192 190 193

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+AMM(I,J)*C(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                          = SIGMAL(I) +AML(I,J)*C(J)
                                                                                                                                                                                                                                                                  IF (K.EQ.NORS) WRITE (7,99) NORC (KKK+1)
                                                                                                                                                                                                                                                                                                                                                                              +AMN(J)*C(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       IF(BB(II,K), EQ.0.0)GU TO 5998
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      IF(CL(II,K).EQ.0.0)60 TD 5998
                                                                                                                                                                                                                                                                                                                                                                                                          IF (AMM(1, J))5989,5989,5988
                                                                                                                                                                                                                                                                                                                                                                                                                          IF (AMM(2, J))5999,5999,5988
                                                                                                          WRITE(7,778) U(K), VOLF(K)
                                                                                                                                                                                                                                                   IF (NORS, EQ.ITN)GO TO 6000
                                                                                                                                                                                     WRITE(7,778)(C(J),J=1,N)
                                                                                          VOLF(K) = V(K) + TITR(K)
                                                                            IF (TYPE, EQ. 1) 60 TO 6000
                                                                                                                                                                                                                                    VORS # NORS & NORC%KKK<
                                                                                                                                                                                                                                                                                                                                                                                             = SIGMAM(I)
                                                                                                                                                                                                                                                                                                                                                                              = SIGMAN
                                                                                                                                                                                                                    30 6011 KKK = 1,30
                                                                                                                                                                                                                                                                                                                                                              = 1,N
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         30 5998 II =1,2
                                                                                                                                                                                                                                                                                                                                0 =
                                                                                                                                                                                                                                                                                                                 0 =
                                                                                                                                                                                                                                                                                                  1 =1,2
                                                                                                                        FORMAT (7E11.4)
               DU 230 I=1,20
                                             WRITE (6,209)
                                                                                                                                                       = f 1019 DO
                                                                                                                                                                       C(1) = 0.0
                                                                                                                                         II = N + I
                                                                                                                                                                                                                                                                                                                                                                                                                                         SIGMAL(I)
                                                            50 TO 134
                                                                                                                                                                                                                                                                                                                                                              00 5999 J
                                                                                                                                                                                                                                                                                                                                                                                            SIGMAM(I)
                              0.0=(1)3
                                                                                                                                                                                                                                                                                                                 SIGMAL(I)
                                                                                                                                                                                                                                                                                                                               SIGMAM(I)
                                                                                                                                                                                                     VORS # 0
                                                                                                                                                                                                                                                                                                                                                                                                                                                         CONTINUE
                                                                                                                                                                                                                                                                                  CONTINUE
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                                                                                                                                                                                                                                                                                                                                               SIGMAN
                                                                                                                                                                                                                                                                                                                                                                             SIGMAN
KK=1
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                               230
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                                                                                                                301
                                                                                                                                                                                                                                                                                                                                                                                                                                                          12,2 =1, F7.4
                                                                                                                                                                                                                                                                                                                                             , (ZBAR(2,1), I=1,2) , YBB(1,2) , (YBB(2,1),1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                DOUBLE PRECISION TERM(20), TERN(20), C(20), Y1(2), Y2(2), Y3(2), Y4(2),
                                                                                   WRITE (6,212) K, U(K), TITR(K), R, BB(1,K), BB(2,K), CL(1,K), CL(2,K),
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          18TOT(2), CLTOT(2), TX(2), VX(2), BO(2), ALO(2), SEM(20, 20), SEI(20, 20),
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    DIMENSION ML(2,20), MM(2,20), MN(20), AL(2,20), AM(2,20), AN(20)
                                                                                                                                                                                                                                                                                                                                                                                                                             334 FORMAT (' ', 5X, 'ZBAR1, 2 = ', F7.4, 2X, '2, 1 = ', F7.4, 2X,
                                                                                                                                                                                                                                                                                                                                                                                                                                                          F7.4,2X,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       ML, MM, MN, AL, AM, AN, NL, NM, N, UX, F, CKW, NIT, NNCI, KJ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            COMMON C, Y1, Y2, Y3, Y4, BTOT, CLTOT, TX, VX, H0, B,
                                                                                                                                                                                                                                                                                                                                                                                                                                                        2F7,4, **** YB1,2 =", F7.4, 2X, '2,1 =",
                                                                                                                                                                    WRITE (6,214) (C(J), J=11,20) ,ZBAR(1,1)
                                                                                                                                         WRITE (6,213) (C(J), J=1,10) ,YBB(1,1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           FURMAT (5X,10(1X,1PE10.3), 5X,0PF7.3)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              213 FORMAT (8X,10(1X,1PE10.3),4X,0PF7.3)
YBB(I, II) = SIGMAM(I) /CL(II, K)
                                                                                                              VX(1), VX(2), TX(1), TX(2), Y(1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       SEV(20), SHFT (20), B (20), HO
                            Y(II) = SIGMAN /CL(II,K)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           IF (NJD-NJ) 1,1000,1000
                                                                                                                                                                                                                                                                                                                                         WRITE(6,334) ZBAR(1,2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        IF (K-ITN) 135,135,215
                                                                                                                                                                                                                             IF(ML(2,J))331,331,332
                                                                                                                                                                                                                                                         IF (MM(2, J) )333,333,332
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     3, 2X, "Y2 =", F7.4)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               SUBROUTINE COGSNR
                                                                                                                                                                                                 N_1 = 1.0
                                                                                                                                                                                                                                                                                                                                                                      2=1,2), Y(2)
                                                                                                                                                                                                                                                                                                                GD TO 335
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                I+drN=drN
                                                        CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   CONTINUE
                                                                                                                                                                                                                                                                                   CUNTINUE
                                                                                                                                                                                                                                                                                                                                                                                                   335 K=K+1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        STCP
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                                                        5998
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ZBAR(I,II) = SIGMAL(I) / BB(II,K)

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	998 FORMA	FORMAT (* ITERATI	ERATION DID NOT C	CONVERGE,	POINT	NUMBER	. (81.	***		351
ی در	CALCU	CALCULATES CONCEN	ONCENTRATION OF E	EACH SPECIES	IES				•	
)	NIT=0									
	00 1	K=1, N								353
	1 TERM	K)=B(K)*UX**	MN(K)							354
	2 DO 3	K=1,N								352
	3 TERN	K)=TERM(K)						9		356
	1F (N	1F (NM) 42,42,41								
	5 00 4	J=I,NM								358
	4 TERN(K)=TERN(K)*V	X (C) WW * * (C) X	C						
	45 D0 5	K=1,N								
	IF (N	11 5,5,50								
	9 00 09	J=I , NL								
	6 TERN(K)=TERN(K)*T	X(7) **WL(7) X							
	5 C(K)=	TEKN(K)								373
	100 NIT=N	IIT+1.								374
رى	CALCULATE	LATES EACH TOTAL	OTAL METAL A	AND TOTAL LIGAND CONCENTRATION	LIGAND	CONCE	NTRATION			
)	7 00	I=1,NM								375
	80(1)	=VX(I)							3	376
	DO 8									377
	8 BU(1)	I w	I,K)*C(K)							378
		Ξ	-BTOT(I))							379
	y 00	I=I •NL								380
	ALG(1									186
)=ALO(I)+AL()+AL(I,K)*C(K)							383
	9 74(1)	Y4(I)=DABS(ALO(I)	LO(1)-CLTOT(1))							384
į,	IF (N	11	,11,999							385
ے د	CHECKS	DEGREE OF	COMVERGENCE							
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                                                                                                                                                             IF CONVERGENCE INSUFFICIENT SETS UP, AND SOLVES, MATRIX FOR IMP-ROVED VALUES OF EACH FREE METAL AND FREE LIGAND CONCENTRATION
                                                                                                                                                                                                                                                                                                                                                                                                                                         SEM(I, J) = SEM(I, J) - C(K) * AM(J, K) * AL(IMNM, K)
                                                                                                                                                                                                                                                                                                                                                               SEM(I, J) = SEM(I, J) - C(K) * AM(I, K) * AM(J, K)
          IF (Y1(1)-Y2(1)) 14,12,12
                                               IF (Y3(I)-Y4(I)) 14,13,13
                                                                                                                                                                                                                                                                                                               SEN(I,I)=-TX(IMNM)
                                                                                                             HD=HD-AN(J)*C(J)
                                                                         HD=1./UX-CKW*UX
                                                                                                                                                                                                                                                                                       DO 1003 I=M1,M2
                                                                                                                                                                                                                                                                                                                                                                           DO 1005 I=M1,M2
                                                                                                                                                                                                                                                                          SEM(I,I) = -VX(I)
                                                                                                                                                                                                                                                                                                                           00 1004 I=1,NM
                                                                                                                                                                                                                                      DO 1001 J=1,M2
                                                                                                                                                                                                                                                              30 1002 I=1,NM
                                                                                                                                                                                                                                                                                                                                       DO 1004 J=1,NM
                                                                                                                                                                                                                                                                                                                                                                                       DU 1005 J=1,NM
                                                                                                                                                                                                                                                                                                                                                                                                                                                    NO 1006 I=1,NM
                                                                                                                                                                                                                          DO 1001 I=1,M2
                                                                                                                                                                                                                                                                                                                                                   DO 1004 K=1,N
                                                                                                                                                                                                                                                                                                                                                                                                  DO 1005 K=1,N
                                                                                                 DU 2001 J=1,N
                                                                                                                                                                                                                                                  SEM(I, J)=0.0
DO 12 I=1,NM
                                   00 13 I=1,NL
                                                                                                                                                                                                                                                                                                    MN-I-MNWI
                                                                                                                                                                                                                                                                                                                                                                                                                NN-I-WNWI
                                                                                                                                                                                                                                                                                                                                                                                                                             MNM=I-NM
                                                                                                                         IPT=IPT+1
                        CONTINUE
                                                            CONTINUE
                                                                                                                                                                                                              M2=NM+NL
                                                                                     40 = HD / F
                                                                                                                                                                                                  I +WN= TW
                                                                                                                                    RETURN
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                                                                                                                                                                                                                                                                                                                                                                                                                                                              644
                                                                                                                     SEM(I, J) = SEM(I, J) - C(K) * AL(IMNM, K) * AL(JMNM, K)
                                       SEM(I, J) = SEM(I, J) - C(K) * AM(I, K) * AL(JMNM, K)
                                                                                                                                                                                                                                                                                                                                                                                           (SHFT(I)+0.9999) 1014,1013,1013
                                                                                                                                                                                                                                                        CALLS MATRIX INVERSION SUBROUTINE
                                                                                                                                                                                                                                                                                                                                                                 SHFT(1)=SHFT(1)+SEI(1,J)*SEV(J)
                                                                                                                                                                                       SEV(I) =-CLTOT (IMNM) + ALO (IMNM)
                                                                                                                                                                                                                                                                                                                                                                                                                                               VX(I) = VX(I) + VX(I) * SHFT(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       TX(K) = TX(K) + TX(K) * SHFT(I)
                                                                                                                                                SEV(1) = -BTOT(1) + BO(1)
                                                                                                                                                                                                                                                                                   CALL SUB760(SEI,M2)
                                                                                                                                                                                                                              SEI(I, J) = SEM(I, J)
DO 1006 J=M1,M2
                                                    DO 1007 I=M1,M2
                                                                                                                                                             DO 1009 I=M1,M2
                                                                                                                                                                                                                                                                                                                                                                                                                                                             DO 1016 I=M1,M2
                                                                  DO 1007 J=M1,M2
                                                                                                                                                                                                                                                                                                                                                                                                        SHFT(I)=-0.9999
                                                                                                                                   DO 1008 I=1,NM
                                                                                                                                                                                                  DO 1010 I=1,M2
                                                                                                                                                                                                                DO 1010 J=1,M2
                                                                                                                                                                                                                                                                                                                                                                             00 1013 1=1,M2
                                                                                                                                                                                                                                                                                                                                                                                                                                  DO 1015 I=1,NM
                                                                                                                                                                                                                                                                                                                                     DG 1012 I=1,M2
                                                                                                                                                                                                                                                                                                             DO 1011 I=1,M2
                                                                                                                                                                                                                                                                                                                                                    DO 1012 J=1,M2
             DO 1006 K=1,N
                                                                              DO 1007 K=1,N
                                                                                                                                                                                                                                                                                                                          SHFT(1)=0.0
                         UMNM=U-NM
                                                                                                                                                                          MNHIHMNWI
                                                                                           MN-I-WNWI
                                                                                                        MN-C=MNWC
                                                                                                                                                                                                                                                                                                                                                                                                                     CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         K=I-NM
                                                                                                                                                                                                                                                                                                                                                                                          Li-
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       9101
                                                                                                                                                                                                                                                                                                                                                                                                                                               1015
                                                                                                                      1007
                                                                                                                                                                                                                                                                                                                                                                1012
                                                                                                                                                1008
                                                                                                                                                                                                                               0101
                                                                                                                                                                                                                                                                                                                                                                                                        1014
                                                                                                                                                                                                                                                                                                                                                                                                                     1013
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									19												
		*																			
		60																_			
																		760			
																		,J760)=A760(1760,J760)-CM760*A760(K760,J760)	-		
																100		760			
		CONVERGENCE AFTER 100 ITERATIONS	c															0 (K			
		ATI																476			
		ER.											00					*0			
		Ξ											M76					M76			
		100									2		1/0)-C			
		ER ER					_						091					091			
		FT					09,	20					٦,					٦,			
		ш					SUBROUTINE SUB760(A760,N760)	20,					760	- 5	79			760			
		S					760	09		(0) (K	,	, (O			1)0			
		ERG.					(A	AZ	00	476	0.1	0,0	176	00	92	0.0	00	176			
		N	Z.				196	S	Z	1.0	= (NZ	/=(ZZ S	0.0)=(N76	/=(
							SUE	ISI	=1,	K76	760	=1,	760	11	01.0 176	760	=1,	760			
		2	966	-	1		빌	REC	760	09	0,K	160	0,1	760	0 (O (0,K	760	0,1			
2		Ħ	(9)	J.V	2		Ξ	Q .	*	= A7	923	7	913		- A7	176	3	16	S	7	
01 09		EXITS	표.	- Î	UR.		ROI	18	164	.09	10	76	10	767	1.09	0	16	0	IL	UR	0N
09		Щ.	WRITE(6,998)	1PT=1	RETURN	END	SUE	DOUBLE PRECISION A760(20,20)	DO 764 K760=1,N760	CM760=A760(K760,K760	A76	00	A760(K760, J760) = A760(K760, J760)/CM760	00	IF (1160-K/60) (62, (64, 162 CM760=A760 (1760, K760)	A760(1760,K760)=0.0	DO 763 J760=1,N760	A7,60(1760	CONTINUE	RETURN	Ш
			666						3				165		162			763	764		
	()	ں ں	6				1.5	L.	5				7		7			7	7		
		-					hard	None													

Program

RWZASCOG

This program is used for calculating formation curves of metal-ligand interactions from experimental results that have been prepared as data for input into RWSCOGSY.

INPUT

The program is stored under the 44PS system on the St. Andrews I.B.M. 360/44 computer and is called using the following cards

Card 2. //bEXECbRWZASCOG

DATA

/*

The experimental DATA is identical to the input of RWSCOGSY + a few blank cards as item 14 of data.

OUTPUT

This is self explanatory. A formation curve is a plot of ZEAR versus pA.

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RWZASCOG
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```
DIMENSION TITLE (20,30), BS (30), ASI (30), HSI (30), VINIT (30), HTI (30), ED
                                                          3AA(30,40), PH(30,40), BB(30,40), FLIG(30,40), ZBAR(30,40), PA(30,40), ZD
                                       , VADD (30,40), E(30,40), AT(30), BT(30), V(30,40), TH(30,40),
                                                                                                                                                                                                                                                                                                                                                                                                                                                                          , FN(J)
                                                                               3NA(30,40),H(30,40),B(5),BETA(5),Z(5),FN(30),NUM(30)
                                                                                                                                                                                                                                                                                                                                                                                                                                  (C) LINI A
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              10X,3(F10.3))
                                                                                                                                                                                                                                                                                                                                                                                                                                  , HSI(J),
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          • INDEX
                                                                                                                                                                                                                                                                                                                                                                                                                                                     -URMAT (F10.3,10X,F10.3,10X,2(F10.3))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         , HTI(J)
                                                                                                                                                                                                                                                                                                                                                                                                             READ(5,5001)(TITLE(1,J),I = 1,20)
 DLOG
                                                                                                                                                                                                                                                                                                                                                                                                                                 , ASI(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        READ(5,40) VADD(J,I), E(J,I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         , AT(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             FURMAT (F10.3,10X, F10.3,
DOUBLE PRECISION DEXP,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         [F(INDEX.EQ.0)60 TO 15
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            FORMAT (2 (F10.3), 4X, 11)
                                                                                                                                                                                                                                                                 READ(5,2001) BETA(II)
                                                                                                                                                                                                                                               30 2098 II = 1,NLXS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         READ(5,5100) BT(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                  READ(5,2003) BS(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                + (C)WON = (C)WON
                                                                                                                                                                                                         NLXS
                                                                                                                        DO 144 MMM = 1, MM
                                                                                                                                                                                                                                                                                     FURMAT (10X, F10.0)
                                                                                                                                                                                                                                                                                                                             READ %5,65) NDP
                                                                                                   READ (5,65) MM
                                                                                                                                                                                                                          FORMAT (4X, 12)
                                                                                                                                                                                                      READ (5,2099)
                                                                                                                                                                                                                                                                                                                                                                                        FURMAT (2044)
                                                                                                                                           READ (5,2000)
                                                                                                                                                                                   FORMAT (2012)
                                                                                                                                                                                                                                                                                                                                                                      M.1=C 41 00
                                                                                                                                                               READ (5,65) N
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  NUM(J) = 0
                                                                                                                                                                                                                                                                                                                                                   DPN = NDP
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      1 + I =
                                                                                                                                                                                                                                                                                                           CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          15
                                                                                                                                                                                    2000
                                                                                                                                                                                                                                                                                       2001
                                                                                                                                                                                                                                                                                                           2098
                                                                                                                                                                                                                           2099
                                                                                                                                                                                                                                                                                                                                                                                           5001
                                                                                                                                                                                                                                                                                                                                                                                                                                                       2003
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              5100
```

UU UU

```
2BT(J) ,AT(J) ,EC(J) , B(2) , B(3)
30 FORMAT('', 5X, 'INITIAL SOLUTIONS .... ACID =',F9.6,3X,'METAL ='
                                                                                                                                                                                                                                                                                                                                                                                                                                                                            .... ACID = ", OPF9.6, 3X, "METAL = ", F9.6, 3X
                                                                                                                                                                                                                                                                                                                                                                                                                             ,5X, 'BETAI ='
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      ,5X, 'BETA2 ="
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             FLIG(J,I) = (TH(J,I) - H(J,I) + WK/H(J,I)) / (B(1)*H(J,I) + 2.0*B(
                                                                                                                                                                                                                                                                                                                                                       B(1) , HTI(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   TH(J,I) = ((HSI(J)*VINIT(J))/V(J,I)) +(HII(J)*VADD(J,I)/V(J,I))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         60 FORMAT(19X, 'VADD'6X, 1HE, 7X, 2HPH, 7X, 4HZBAR, 6X, 2HPA, 7X, 4HFLIG,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       + BT(J) * VADD(J,I))/ V(J,I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           AA(J,I) = (ASI(J)*VINIT(J)/V(J,I))+(AT(J)*VADD(J,I)/V(J,I)
                                                                                                                                                                                                                                                                                                                                                  , ASI(J) , VINIT(J),
                                                                                                                                                                                                                                                                                                                                                                                                                          * VOLUME = *, F7.2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      =', F7.2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            106X, 'BETA3 = 'IPE11.4/)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       + 3.048(3) *H(J,I)**3.0)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 , F9.6,3X, 'ED
                                                                                                                                                                                                                                                                                               WRITE(6,2009) (TITLE(I,J), I= 1,20)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  HSI(J) = HSI(J) + ASI(J) * DPN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   PH(J_1) = (EO(J) - E(J_1))/FN(J)
                                                                                                                                                                                                                                                                                                                                                                                                                       2,F9.6,3X,'LIGAND =',F9.6,3X,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              + VACD(J,I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            H(J,I) = EXP(-2.3026*PH(J,I))
                                                                                                                                                                       READ(5,2002)(2(1), 1=1,NBETA
                                                                                                                                                                                                                                                                                                                                               WRITE(6,30) HSI(J) ,8S(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    BB(J,I) = (BS(J)*VINIT(J)
                                                                                                                                                                                                                                                                                                                      FURMAT("1" ,40X ,20A4//<
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           HTI(J) = HTI(J) + AT(J)
                                                                                                                                                                                                                                                B(II) = 10.0**BETA(II)
                                                                                                                                               NBETA = NLXS - NBETA
                                                                                                                                                                                                                        DO 2097 1I = 1,NBETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           V(J_1) = VINIT(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                "LIGAND ="
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   DO 144 I = 1, NUMJ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         4 , 6X, 'TITRATING
                                                                                               READ(5,64) NBETA
                                                                                                                                                                                              FURMAT ( F10.0 )
                      READ (5,2004) WK
                                                                                                                                                                                                                                                                        00 144 J = 1, M
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     22)*H(J,I)**2.0
                                                                       WK = 10.0**WK
                                                                                                                     FORMAT (2X,12)
                                            FURMAT (F10.3)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            (C) WON = FWON
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    18X,4HZONA//)
                                                                                                                                                                                                                                                                                                                                                                                                                                                   , IPE11,4 /
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   WRITE (6,60)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         ,1PE11.4
14 CONTINUE
                                               2004
                                                                                                                                                                                                                                                                                                                         2009
                                                                                                                                                                                                                                                2097
                                                                                                                                                                                                2002
```

```
ZBAR(J,I) =(AA(J,I) - FLIG(J,I)*(1.0 + B(I)*H(J,I) + B(2)*H(J,I)**
22.0 + B(3) *H(J,I)**3.0))/BB(J,I)
                                                                                                                                                      144 WRITE(6,50) VADD(J,I) ,E(J,I) ,PH(J,I) ,ZBAR(J,I) ,PA(J,I)
                                                                                                                                                                                   2LIG(J,I) ,ZONA(J,I)
50 FORMAT(' '15X,F6.2,3X,F6.1,3H F7.4,3H
13H F7.4,3H E11.4,3H E11.4/)
                                                                                          142 PA(J,I) = -ALOGIO(FLIG(J,I))
143 ZONA(J,I) = ZBAR(J,I)/FLIG(J,I)
                                                              IF(FLIG(J,I))143,143,142
                                                                                                                                                                                                                                                                                       65 FORMAT(I2)
```

APPENDIX III

RWSOLV

```
SUMP%4<, SUMQ%4<, SUMR%4<, SUMS%4<, P%4<, Q%4<, R%4<,
                              1T%4<, A%90,5<, AU%90<, V%4<, SUMT%4<, QCALC%90<, PCENT%90<
                                                 C(5,4)
                                             DOUBLE PRECISION CC(4,4) ,AC(4,4) ,PP(4),
                                                                                                                                             READ%5,30< A%I,NY< , %A%I,J<,J#I,NX<
NA(4), NB(4),
                                                                                                                                                                                                                                             C%J,K<#C%J,K<6A%I,K<*A%I,J<
                                                                                                                                                                                                                                                                                                                                             MINV (AC, 4, DEL, NA, NB)
                                                                                                                                                               E11.4)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             S#SECC%1,K<*AC%K,J<
DOUBLE PRECISION
                                                                                              READ 25,20< N, NX
                                                                                                                                                              FORMAT (E11.4, 6
                                                                                                                                                                                                                                                                                                                                                              FURMAT %6E15.8<
                                                                                                                                                                                                                                                                                              CC%I, J<#C%I, J<
                                                                                                                                                                                                                                                                                                              AC%I, J<#C%I, J<
                                                                                                                                                                                                                                                                                                                              PP%I<#C%NY,I<
                                                                                                                                                                             DO. 11 J#1,NY
                                                                                                                                                                                             DO 11 K#1,NX
                                                                                                                                                                                                                                                            DO 12 I#1,NX
                                                                                                                                                                                                                                                                              30 13 J#1,NX
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               DO 31 K#1,NX
                                                                                                                                                                                                                                                                                                                                                                                                                                            DO 32 I#1,NX
                                                                                                                                                                                                                                                                                                                                                                                                                                                            DO 32 J#1,NX
                                                               KEAD %5,20<
                                                                              DO 28 L#1,M
                                                                                                                              N. 1#1 71 DO
                                                                                                                                                                                                                               DO 11 I#1,N
                                                                                                                                                                                                                                                                                                                                                                                                             SWIN#XN-0.5
                                                                                                                                                                                                                                                                                                                                                                                             XMAX#XNE0.5
                                                                                                                                                                                                              C%J,K<#0.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              SUM#SUMES
                                                                                                                                                                                                                                                                                                                                                                                                                               SUM#0.0
                                                                                                               NY#NXE1
                                                                                                                                                                                                                                                                                                                                                                                XN#NX
                                                                                                                                                                                                                                                                                                                                               CALL
                                                                                                                                                                                                                                                                                                                                                                                                                                                                              S#0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               31
                                                                                                                                               30
```

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30
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         NIN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         NIN.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        NIN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          VNIN.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       MINV
                                                                                                                                        FORMAT('1',10X,'H1 = ',1PE11.4,10X,'H2 = ',1PE11.4,10X,'H3 = ',1PE
                                                                                                                                                                                          16X, COEFFICIENTS 1,
                                                                                                                                                                                                                                                                                                                                  (A(I,1), J=1,NX)
                             FORMAT('1', 'COEFFICIENTS MATRIX SINGULAR', 2(E16.8)///)
                                                                                                                                                                                                                                                                                                                                               4(6X,1PE11.4)//)
                                                                                                                                                                                                                                                                                                                                                                                                         FORMAT(' ',30X, 'THE STANDARD DEVIATION IS' , F7.4)
                                                                                                                                                                                     60 FORMAT( ',9X, 'QEXPT',11X, 'QCALC',
                                                                                                                                                                                                    SIGMA = SQRT(SQ/(G - (4.0 - XN))
                                                                                                                                                                                                                                                                                                                             WRITE(6,80) A(1,NY), QCALC(I)
                                                                                                                                                       211.4,10X, "H4 = ',1PE11.4////
                                                                                                                         WRITE%6,100< %V%I<,I#1,NX<
                                                                                                                                                                                                                                                                                                SQ = SQ + (S - A(I,NY)) **2
                                                                                                                                                                                                                                                                                                                                            FORMAT(" ',2(6X,1PE11.4),
                                                                                                                                                                                                                                                                                                                                                                                            SIGMA
IF %SUM-XMIN<40,40,50
               WRITE(6,45) SUM ,DEL
                                                                                           CX#CX&AC%I,J<*PP%J<
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      SUBROUTINE MINV
                                                                                                                                                                                                                                                                                 S#SEA%I,J<*V%J<
                                            DO 52 I#1,NX
                                                                            DO 51 J#1,NX
                                                                                                                                                                                                                                                                 DO 54 J#1,NX
                                                                                                                                                                      WRITE $6,60<
                                                                                                                                                                                                                                    DO 27 I#1,N
                                                                                                                                                                                                                                                                                                                                                                                           WRITE %6,70<
                                                                                                                                                                                                                                                                                                                                                                                                                          FORMAT%212)
                                                                                                                                                                                                                                                                                                              QCALC%I<#S
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   PURPOSE
                                                                                                                                                                                                                     SQ = 0.0
                                                                                                                                                                                                     22,3 6 4
                                                                                                          V%I<#CX
                                                             CX#0.0
                                                                                                                                                                                                                                                   S#0.
                                                                                                                                                                                                                                                                                                                                                                                                                                         STOP
                                                                                                                                                                                                                                                                                                                                                             C#N
                                                                                                                                                                                                                                                                                                                                                                                                                                                         END
                               45
                                                                                                                                         100
                                                                                                                                                                                                                                                                                 54
                                             20
                                                                                            51
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IF %SUM-XMAX<35,40,40

INVERT A MATRIX	N I N	70
	> NIN	80
USAGE	VIN.	96
CALL MINV(A,N,D,L,M)	NIN'	100
	>NIN	110
	> N I N	120
	> Z I Z	130
RES	NIN.	140
	NIN N	150
D - RESULTANT DETERMINANT	NIN.	160
IR OF	NI N	170
1	>NIN	180
	VIN.	190
	NIN.	200
MATRIX A MUST BE A GENERAL MATRIX	MINV	210
	NIN'	220
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	>ZIV	230
NONE	NIN	240
	MINV	250
	MIN	260
	NIN'	270
ILSO CALCULATED. A DETERMINANT OF ZERO	NIN.	280
THE MATRIX IS SINGULAR.	VIN.	290
	VIN.	300
	NIN.	310
	NIN.	320
UBROUTINE MINV(A, N, D, L, M)	MIN	330